

# The Onset of Buoyancy and Surface Tension Driven Convection in a Ferrofluid Layer by Influence of General Boundary Conditions

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## Abstract

This paper investigated the buoyancy and surface tension-driven ferro-thermal-convection (FTC) in a ferrofluid (FF) layer due to influence of general boundary conditions. The lower surface is rigid with insulating to temperature perturbations, while the upper surface is stress-free and subjected to general thermal boundary condition. The numerically Galerkin technique (GT) and analytically regular perturbation technique (RPT) are applied for solving the problem of eigenvalue. It is analyzed that increasing Biot number, decreases the magnetic and Marangoni number is to postponement the onset. Additionally, magnetization nonlinearity parameter has no effect on FTC in the non-existence of Biot number. The results under the limiting cases are found to be in good agreement with those available in the literature.

## Keywords

Marangoni Number, Ferrothermal Convection, Insulating, Regular Perturbation Technique, Galerkin Technique

## 1. Introduction

Until recently, there were liquids which could be magnetized to be comparable with the magnetization of magnetic nanoparticles. They have developed colloidal suspensions containing magnetic nanoparticles with a carrier liquid like water, hydrocarbon such as mineral oil or kerosene, or fluorocarbon referred as ferrofluids (FFs). Hence, FFs subjects have obtained much attention among the scientific communities [1] [2] [3] [4]. The magnetization of FFs depends on its magnetic field, temperature and density. Whereas when a horizontal FF layer is pre-

sent with a magnetic field, it is heated from below and convective motions might take place which is called as FTC [5].

Thereby, FTC can also be induced by providing surface-tension and later with the function of temperature. Qin and Kaloni [6] have investigated both linear and non-linear stability of combined effects of buoyancy and surface tension forces in a FF layer. Hennenberg *et al.* [7] have examined the coupling effects on Marangoni and Rosensweig instabilities by considering two semi-infinite immiscible and incompressible viscous fluids. The results of different basic temperature gradients on FTC which is driven by buoyancy and surface tension forces discussed by Shivakumara *et al.* [8] with an plan following indulgent control of FTC concept. Shivakumara and Nanjundappa [9] have also examined the initiation of Marangoni FTC with differing initial temperature gradients. A very less number of researches address the effects of Bouyancy and surface tension forces on FTC (see [10] [11]) with viscosity variations ([12] [13] [14] [15]), heat source strength ([16] [17]) and Coriolis force ([18] [19]) in a FF layer. Later, Shivakumara *et al.* [20] studied the onset of FTC in a horizontal FF layer with temperature dependent viscosity in exponentially. In many natural phenomena, the study of penetrative FTC in a saturated porous layer is studied by Nanjundappa *et al.* [21] with the internal heating source and applied Brinkman extended Darcy model in the momentum equation. Nanjundappa and co-workers ([22] [23] [24]) analyzed the internal heat generation effect on the onset of FTC in a FF saturated porous layer. Recently, Savitha *et al.* [25] investigated the penetrative FTC in a FF-saturated high porosity anisotropic porous layer via uniform internal heating.

The intent of the present work is to investigate Bénard-Marangoni FTC in a FF layer due to influence of general boundary conditions. The numerically Galerkin technique (GT) and analytically regular perturbation technique (RPT) are applied for solving the problem of eigenvalue when both the surfaces insulated to temperature perturbations.

## 2. Formulation of the Problem

Consider an incompressible FF horizontal layer of thickness  $d$  with temperatures  $-k_1 \partial T / \partial z = q_0$  ( $z = 0$ ) and  $k_1 \partial T / \partial z = h_1 (T - T_\infty)$  ( $z = d$ ). Where  $T$  is the temperature,  $q_0$  is the conductive thermal flux,  $k_1$  the overall thermal conductivity,  $h_1$  the heat transfer coefficient and  $T_\infty$  the temperature in the bulk of the environment.

Cartesian coordinates  $(x, y, z)$  system are chosen (see **Figure 1**). Gravity acts vertically downwards and is given by  $\vec{g} = -g\hat{k}$ , where  $\hat{k}$  is the unit vector in the  $z$ -direction. The layer is bounded below by a rigid surface and above by a non-deformable free surface. At the upper free surface, the surface tension  $\sigma$  is assumed to vary linearly with temperature in the form

$$\sigma = \sigma_0 - \sigma_T (T - T_0) \quad (1)$$

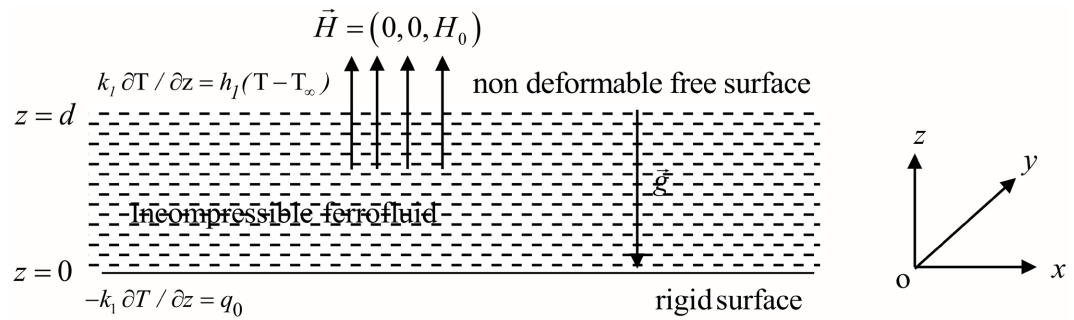


Figure 1. Physical configuration.

where  $\sigma_0$  is the unperturbed value and  $-\sigma_T$  is the rate of change of surface tension with temperature  $T$ . The fluid density  $\rho$  is assume to vary linearly with temperature in the form

$$\rho = \rho_0 [1 - \alpha_t (T - T_0)] \tag{2}$$

where  $\alpha_t$  is the thermal expansion coefficient and  $\rho_0$  is the density at  $T = T_0$ . The governing equations for the flow of an incompressible fluid are

$$\nabla \cdot \vec{q} = 0 \tag{3}$$

where  $\vec{q} = (u, v, w)$  is the velocity vector.

$$\rho_0 \left[ \frac{\partial \vec{q}}{\partial t} + (\vec{q} \cdot \nabla) \vec{q} \right] = -\nabla p + \rho \vec{g} + \mu \nabla^2 \vec{q} + \mu_0 (\vec{M} \cdot \nabla) \vec{H} \tag{4}$$

where  $p$  is the pressure,  $t$  is the time and  $\mu_0$  the magnetic permeability of vacuum.

$$\left[ \rho_0 C_{v,H} - \mu_0 \vec{H} \cdot \left( \frac{\partial \vec{M}}{\partial T} \right)_{v,H} \right] \frac{DT}{Dt} + \mu_0 T \left( \frac{\partial \vec{M}}{\partial T} \right)_{v,H} \cdot \frac{D\vec{H}}{Dt} = k_t \nabla^2 T \tag{5}$$

where  $C$  is the specific heat,  $C_{v,H}$  is the specific heat at constant volume and magnetic field, and  $\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}$  is the Laplacian operator.

The magnetic field ( $\vec{H}$ ) in magnetic fluid obeys the Maxwell equations in the absence electric field and current are

$$\nabla \cdot \vec{B} = 0, \quad \nabla \times \vec{H} = 0 \quad \text{or} \quad \vec{H} = \nabla \phi \tag{6a,b}$$

where  $\vec{B}$  is the magnetic induction and  $\phi$  is the magnetic potential.

$$\vec{B} = \mu_0 (\vec{M} + \vec{H}) \tag{7}$$

Since the magnetization ( $\vec{M}$ ) depends on the magnitude of magnetic field and temperature, we have

$$\vec{M} = \frac{\vec{H}}{H} M(H, T). \tag{8}$$

The linearized equation of magnetic state about  $H_0$  and  $T_0$  is

$$M = M_0 + \chi (H - H_0) - K (T - T_0) \tag{9}$$

where  $\chi = (\partial M / \partial H)_{H_0, T_0}$  is the magnetic susceptibility,  $K = -(\partial M / \partial T)_{H_0, T_0}$  is

the pyromagnetic co-efficient and  $M_0 = M(H_0, T_0)$ .

It is clear that there exists the following solution for the basic state:

$$\bar{q}_b = 0, \quad p_b(z) = p_0 - \rho_0 g z - \frac{1}{2} \rho_0 \alpha_t g \beta z^2 - \frac{\mu_0 M_0 \kappa \beta}{1 + \chi} z - \frac{\mu_0 \kappa^2 \beta^2}{2(1 + \chi)^2} z^2$$

$$T_b(z) = T_0 - \beta z, \quad \bar{H}_b(z) = \left[ H_0 - \frac{K \beta z}{1 + \chi} \right] \hat{k}, \quad \bar{M}_b(z) = \left[ M_0 + \frac{K \beta z}{1 + \chi} \right] \hat{k} \quad (10)$$

where  $\beta = \Delta T/d$  is the temperature gradient and the subscript  $b$  denotes the basic state.

To study the stability of the system, we perturb all the variables in the form

$$\bar{q} = \bar{q}', \quad p = p_b(z) + p', \quad T = T_b(z) + T', \quad \bar{H} = \bar{H}_b(z) + \bar{H}', \quad \bar{M} = \bar{M}_b(z) + \bar{M}' \quad (11)$$

where  $\bar{q}'$ ,  $p'$ ,  $T'$ ,  $\bar{H}'$  and  $\bar{M}'$  are perturbed variables and are assumed to be small.

Substituting Equation (11) into Equations (8) and (9), and using Equation (7), we obtain (after dropping the primes)

$$\begin{aligned} H_x + M_x &= (1 + M_0/H_0) H_x, \\ H_y + M_y &= (1 + M_0/H_0) H_y, \\ H_z + M_z &= (1 + \chi) H_z - K T. \end{aligned} \quad (12)$$

Again substituting Equation (11) into momentum Equation (4), linearizing, eliminating the pressure term by operating curl twice and using Equation (12) the z-component of the resulting equation can be obtained as (after dropping the primes):

$$\left( \rho_0 \frac{\partial}{\partial t} - \mu \nabla^2 \right) \nabla^2 w = -\mu_0 K \beta \frac{\partial}{\partial z} (\nabla_h^2 \varphi) + \frac{\mu_0 K^2 \beta}{1 + \chi} \nabla_h^2 T + \rho_0 \alpha_t g \nabla_h^2 T \quad (13)$$

where  $\nabla_h^2 = \partial^2/\partial x^2 + \partial^2/\partial y^2$  is the horizontal Laplacian operator. The temperature Equation (5), after using Equation (11) and linearizing, takes the form (after dropping the primes):

$$\frac{\partial T}{\partial t} - \mu_0 T_0 K \frac{\partial}{\partial t} \left( \frac{\partial \varphi}{\partial z} \right) = k_1 \nabla^2 T + \left[ \rho_0 C_0 - \frac{\mu_0 T_0 K^2}{1 + \chi} \right] w \beta \quad (14)$$

where  $\rho_0 C_0 = \rho_0 C_{v,H} + \mu_0 H_0 K$ . Equations 6(a, b), after substituting Equation (11) and using Equation (12), may be written as (after dropping the primes)

$$\left( 1 + \frac{M_0}{H_0} \right) \nabla_h^2 \varphi + (1 + \chi) \frac{\partial^2 \varphi}{\partial z^2} - K \frac{\partial T}{\partial z} = 0. \quad (15)$$

The normal mode expansion of the dependent variables is assumed in the form

$$\{w, T, \varphi\} = \{W(z), \Theta(z), \Phi(z)\} \exp[i(\omega t + \ell x + m y)] \quad (16)$$

where  $\ell$  and  $m$  are wave numbers in the  $x$  and  $y$  directions, respectively, and  $\omega$  is the growth rate with is complex. On substituting Equation (16) into Equations (13)-(15) and non-dimensionalizing the variables by setting

$$z^* = \frac{z}{d}, w^* = \frac{d}{\nu} w, t^* = \frac{\nu}{d^2} t, \Theta^* = \frac{\kappa}{\beta \nu d} \Theta, \Phi^* = \frac{(1+\chi)\kappa}{K\beta \nu d^2} \Phi \quad (17)$$

where  $\nu = \mu/\rho_0$  is the kinematic viscosity and  $\kappa = k_1/\rho_0 C_0$  is the effective thermal diffusivity, we obtain (after dropping the asterisks for simplicity)

$$\left[ D^2 - a^2 - \omega \right] (D^2 - a^2) W + a^2 [Ra_m D\Phi - (Ra + Ra_m)\Theta] = 0. \quad (18)$$

$$(D^2 - a^2 - \omega Pr)\Theta + W = 0. \quad (19)$$

$$(D^2 - M_3 a^2)\Phi - D\Theta = 0. \quad (20)$$

Here,  $W, \Theta, \Phi$  are respectively the z-component perturbed amplitudes of velocity, temperature and magnetization term. In addition  $D \equiv d/dz$  differential operator,  $a = \sqrt{l^2 + m^2}$  wave number,  $Ra = \alpha_i g \beta d^4$  thermal Rayleigh number,  $M_1 = \mu_0 K^2 \beta / (1 + \chi) \alpha_i \rho_0 C$  magnetic number,  $Ra_m = Ra M_1 = \mu_0 K^2 \beta^2 d^4 / (1 + \chi) \mu \kappa$  magnetic thermal Rayleigh number,  $M_2 = \mu_0 T_0 K^2 / (1 + \chi) \rho_0 C$  magnetic parameter,  $M_3 = (1 + M_0 / H_0) / (1 + \chi)$  magnetization nonlinearity parameter and  $Pr = \nu / \kappa$  Prandtl number.

We impose the boundary conditions (see Ref. [5] [12] [26]):

$$W = DW = 0, D\Theta = 0, \Phi = 0 \text{ at } z = 0 \quad (21)$$

$$W = D^2 W + a^2 Ma \Theta = 0, D\Theta + Bi \Theta = 0, D\Phi = 0 \text{ at } z = 1 \quad (22)$$

or

$$W = D^2 W + Ma a^2 \Theta = 0, D\Theta + Bi \Theta = 0, D\Phi - \Theta = 0 \text{ at } z = 1 \quad (23)$$

where,  $Ma = \sigma_r \Delta T d / \mu \kappa$  the Marangoni number and  $Bi = h_c d / k_1$  the Biot number.

### 3. Numerical Solution

The Galerkin method is applied to solve the problem of eigenvalue constituted by Equations (18)-(20) subject to Equations (21)-(23) and accordingly the expanded unknown variables are

$$\{W, \Theta, \Phi\}(z) = \sum_{m=1}^n \{A_m W_m, B_m \Theta_m, C_m \Phi_m\}(z) \quad (24)$$

where  $A_m, B_m, C_m$  are constants and basis functions  $W_m, \Theta_m, \Phi_m$  are trial chosen usually satisfying the considered boundary conditions as follows

$$W_m = (z^3 - 5z^2/2 + 3z/2)z^m, \Theta_m = z(1 - z/2)z^m, \Phi_m = z^2(1 - z/3)z^m. \quad (25)$$

By introducing Equation (25) into Equations (18)-(20), multiplying the resulting equations respectively by  $W_m, \Theta_m$  and  $\Phi_m$ , integrating between  $z = 0$  and  $z = 1$  and using Equations (21)-(23) yields

$$C_{nm} A_m + M_{nm} B_m + F_{nm} C_m = 0. \quad (26)$$

$$G_{nm} A_m + H_{nm} C_m = 0. \quad (27)$$

$$I_{nm} C_m + J_{nm} D_m = 0. \quad (28)$$

where

$$\begin{aligned}
C_{mn} &= \langle D^2 W_m D^2 W_n \rangle + 2a^2 \langle DW_m DW_n \rangle + a^4 \langle W_m W_n \rangle, \\
M_{mn} &= -a^2 Ra(1 + M_1) \langle W_m \Theta_n \rangle + a^2 Ma DW_m(1) \Theta_n(1) \\
F_{mn} &= a^2 Ra M_1 \langle W_m D \Phi_n \rangle \\
G_{mn} &= -\langle \Theta_m W_n \rangle, \\
H_{mn} &= \langle a^2 \Theta_m \Theta_n + D \Theta_m D \Theta_n \rangle + Bi D \Phi_m(1) \Theta_n(1) \\
I_{mn} &= -\langle D \Phi_m \Theta_n \rangle \\
J_{mn} &= \langle a^2 M_3 \Phi_m \Phi_n + D \Phi_m D \Phi_n \rangle
\end{aligned}$$

with  $\langle \dots \rangle = \int_0^1 (\dots) dz$

Equations (26)-(28) may have a solution of non-trivial solution if

$$\begin{vmatrix} C_{nm} & D_{nm} & E_{nm} \\ F_{nm} & G_{nm} & 0 \\ 0 & H_{nm} & I_{nm} \end{vmatrix} = 0. \quad (29)$$

It would be informative to seem at the results for  $m = n = 1$  as it gives adequate physical insight into the problem with minimum mathematical computations. For this order, Equation (29) in terms of  $Ma$  gives the following characteristic equation (after omitting the subscript 1)

$$Ma = \frac{\eta_1 + \Omega \eta_2}{1260a^2 \langle W \Theta \rangle} \left[ \frac{70Bi}{\eta_3} + (a^2 + \Omega Pr) \right] + \frac{140R_m \langle WD \varphi \rangle}{\eta_3} - 2(R_a + R_m) \langle W \Theta \rangle \quad (30)$$

where  $\eta_1 = 4536 + 432a^2 + 541a^4$ ,  $\eta_2 = 216 + 541a^2$  and  $\eta_3 = 56 + 11M_3 a^2$ .

To stability of the system is examined by taking  $\Omega = i\omega$  in Equation (30) and the complex quantities have to be clearly yields

$$\begin{aligned}
Ma &= \frac{1}{1260a^2 \langle W \Theta \rangle} \left[ \eta_1 \left( \frac{70Bi}{\eta_3} + a^2 \right) - Pr \eta_2 \omega^2 \right] \\
&\quad + \frac{140R_m \langle WD \varphi \rangle}{\eta_3} - 2(R_a + R_m) \langle W \Theta \rangle
\end{aligned} \quad (31)$$

where

$$N = \frac{1}{1260a^2 \langle W \Theta \rangle} \left[ Pr \eta_1 + \eta_2 \left( \frac{70Bi}{\eta_3} + a^2 \right) \right].$$

The steady onset (*i.e.*, direct bifurcation) is governed by  $\omega = 0$  and it occurs at  $Ma = Ma^s$ , where

$$Ma = \frac{1}{1260a^2 \langle W \Theta \rangle} \left[ \eta_1 \left( \frac{70Bi}{\eta_3} + a^2 \right) \right] + \frac{140R_m \langle WD \varphi \rangle}{\eta_3} - 2(R_m + R_a) \langle W \Theta \rangle \quad (32)$$

#### 4. Numerical Results and Discussion

Equation (29) leads to characteristic equation

$$f(Ra, Ma, Bi, M_1, M_3, a) = 0. \tag{33}$$

Here we note that the minimum of  $Ra$  corresponding to  $a_c$  is to be found that for various physical parameters  $Ma, Bi, M_1$  and  $M_3$ . Mathematica 12.0 symbolic algebraic package is applied to compute numerically by Galerkin method for fixing the other parameters with three sets of boundary combinations. The value of  $(Ra_c, a_c)$  obtained here are compared with Sparrow *et al.* [27]. The results established are in admirable agreement and thus validate the exactness of the numerical technique utilized (see **Table 1**).

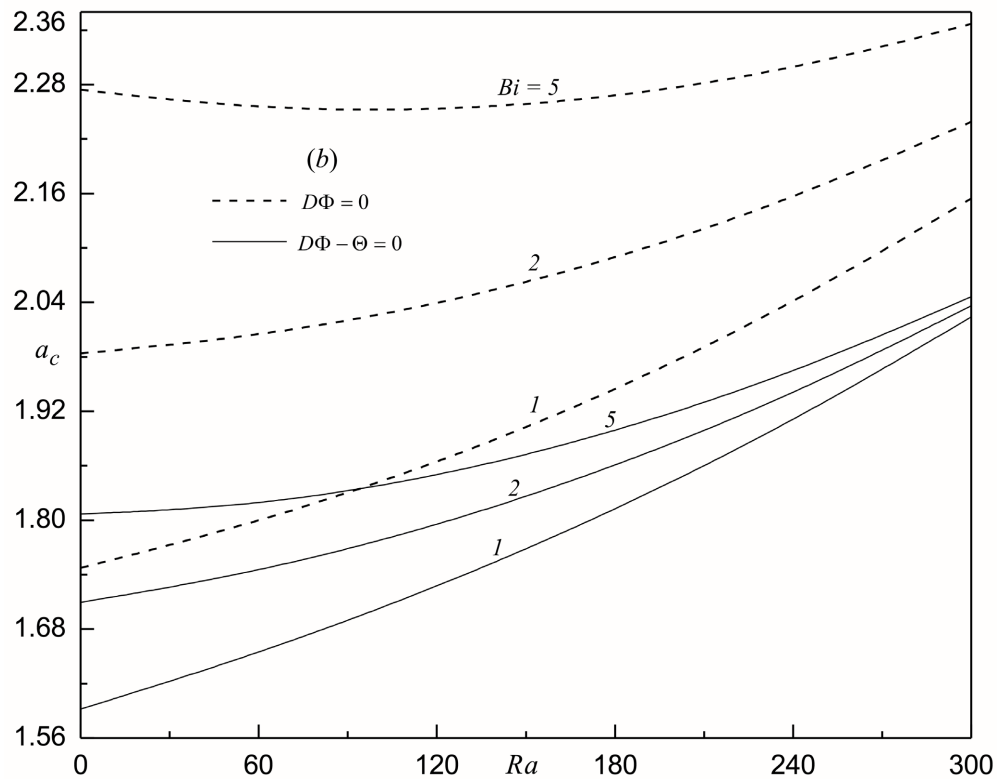
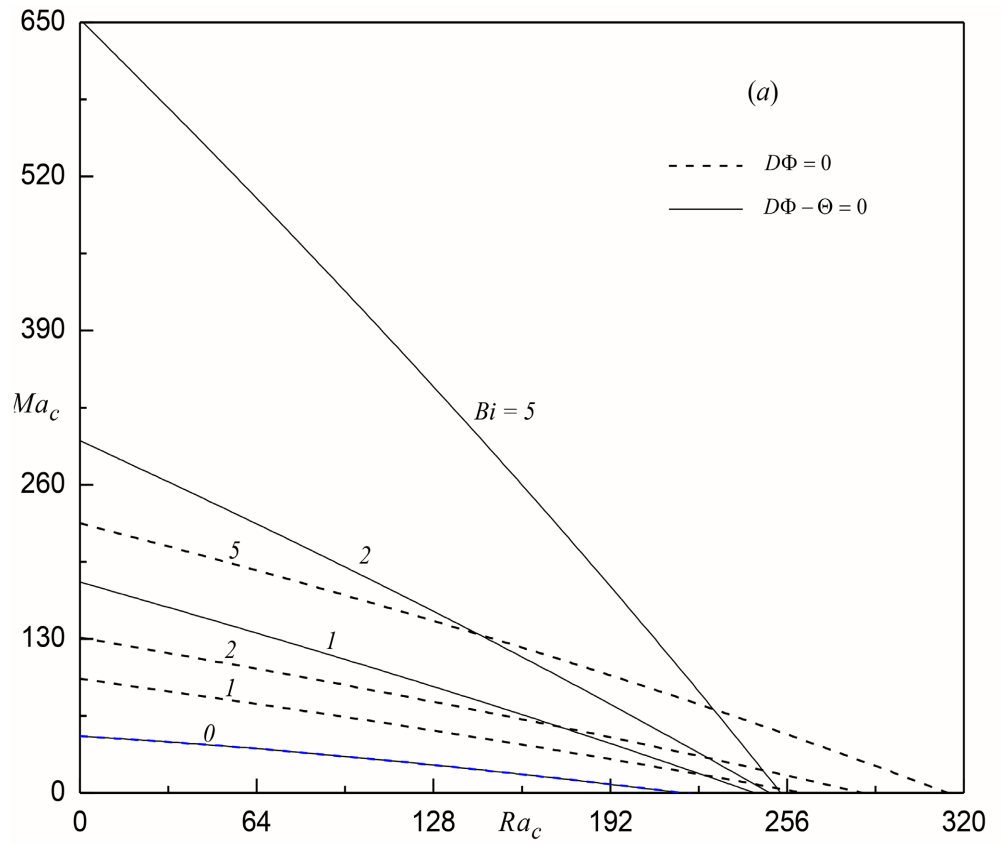
The loci of  $Ma_c$  and  $Ra_c$  with  $Bi, M_1$  and  $M_3$  are shown in **Figures 2(a)-4(a)** respectively as well as different magnetic boundaries at the upper surfaces like  $D\Phi - \Theta = 0$  and  $D\Phi = 0$  at  $z = 1$ . It is noticeable that, curves are slightly convex and there is a strong coupling between  $Ma_c$  and  $Ra_c$ . If the magnetic force is leading, then the surface tension becomes insignificant and vice-versa. A review of **Figure 2(a)**, further reveals that with increase in  $Bi$  it delays the FTC. This may be attributed to fact that with increasing  $Bi$ , the free surface gets deviated from good conductor of heat and there is an increase in  $Ma_c$  and  $Ra_c$ . Also  $D\Phi - \Theta = 0$  surfaces offer more stabilizing effect compared to  $D\Phi = 0$  against FTC. **Figure 2(b)** illustrates that increasing in  $a_c$  as  $Bi$  increases, hence its effect is to diminish the size of convection cells.

In **Figure 3(a)**,  $Ra_c$  and  $Ma_c$  presented with  $M_1$  when  $M_3 = 1$  and  $Bi = 2$ . This is expected that an increase in  $M_1$  is to decrease  $Ma_c$  and  $Ra_c$ , thus leads to a more unstable system due to an increase in magnetic force. Moreover, it is remarkable  $Ma_c$  and  $Ra_c$  are diminishes as  $M_1$  increases. From **Figure 3(b)**, increase  $M_1$  is to increase  $a_c$ , thus leading to diminish the convection cell size..

The effect of increase in  $M_3$  is shown in **Figure 4(a)** for  $Bi = M_1 = 2$  and it is

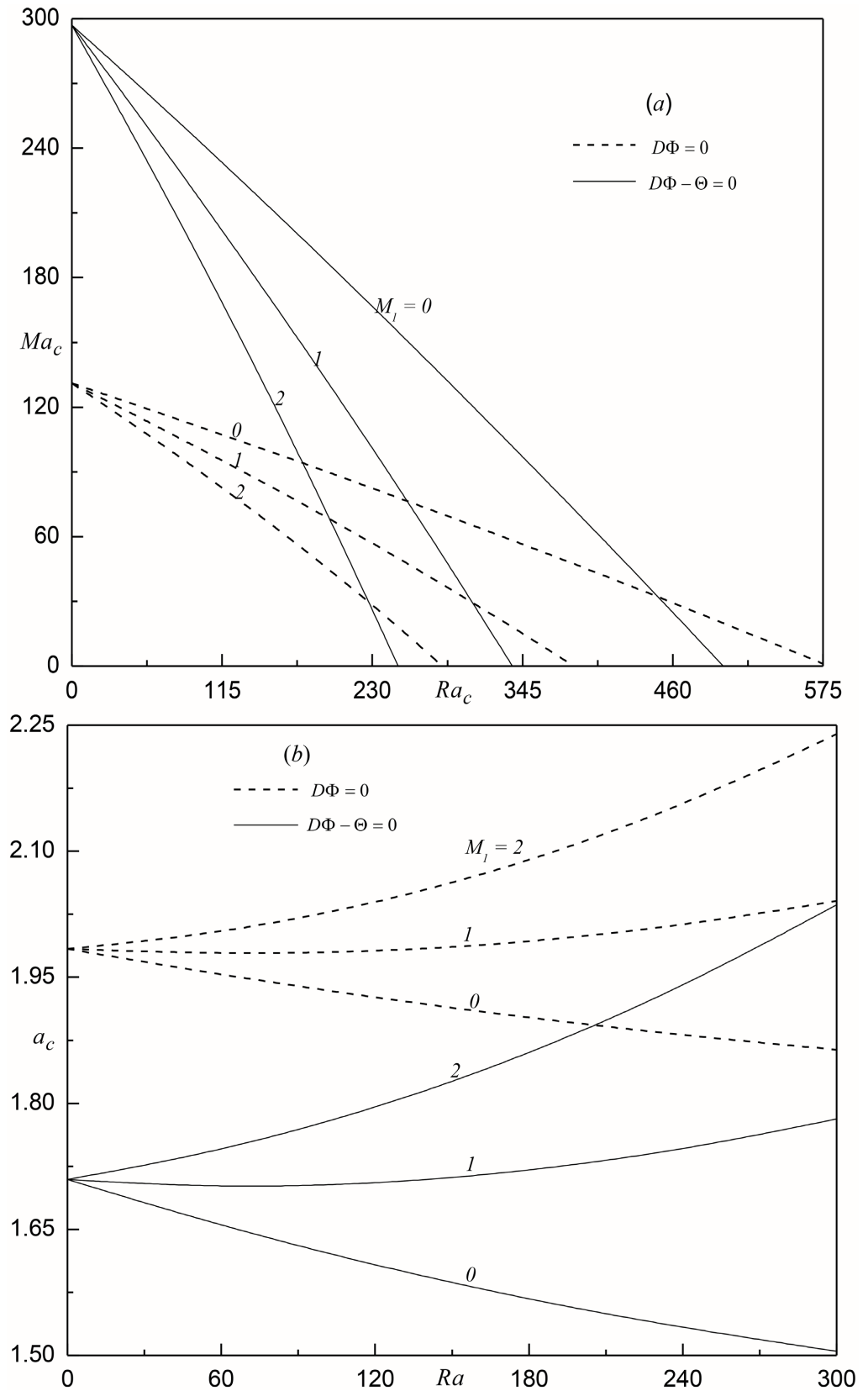
**Table 1.** Comparison of  $(Ra_c, a_c)$  with  $Bi$  for  $Ma = M_1 = 0$ .

$Bi$	Sparrow <i>et al.</i> [27]		Present study	
	$Ra_c$	$a_c$	$Ra_c$	$a_c$
0	320.000	0.00	320.000	$-2.641 \times 10^{-9}$
0.01	338.905	0.58	338.904	0.5831
0.03	353.176	0.76	353.158	0.7624
0.1	381.665	1.015	381.665	1.0151
0.3	428.290	1.03	428.290	1.2992
1	513.792	1.64	513.790	1.6438
3	619.666	1.92	619.666	1.9211
30	780.240	2.18	780.237	2.1760
100	804.973	2.20	804.972	2.2029
$\infty$	816.748	2.21	816.744	2.2147

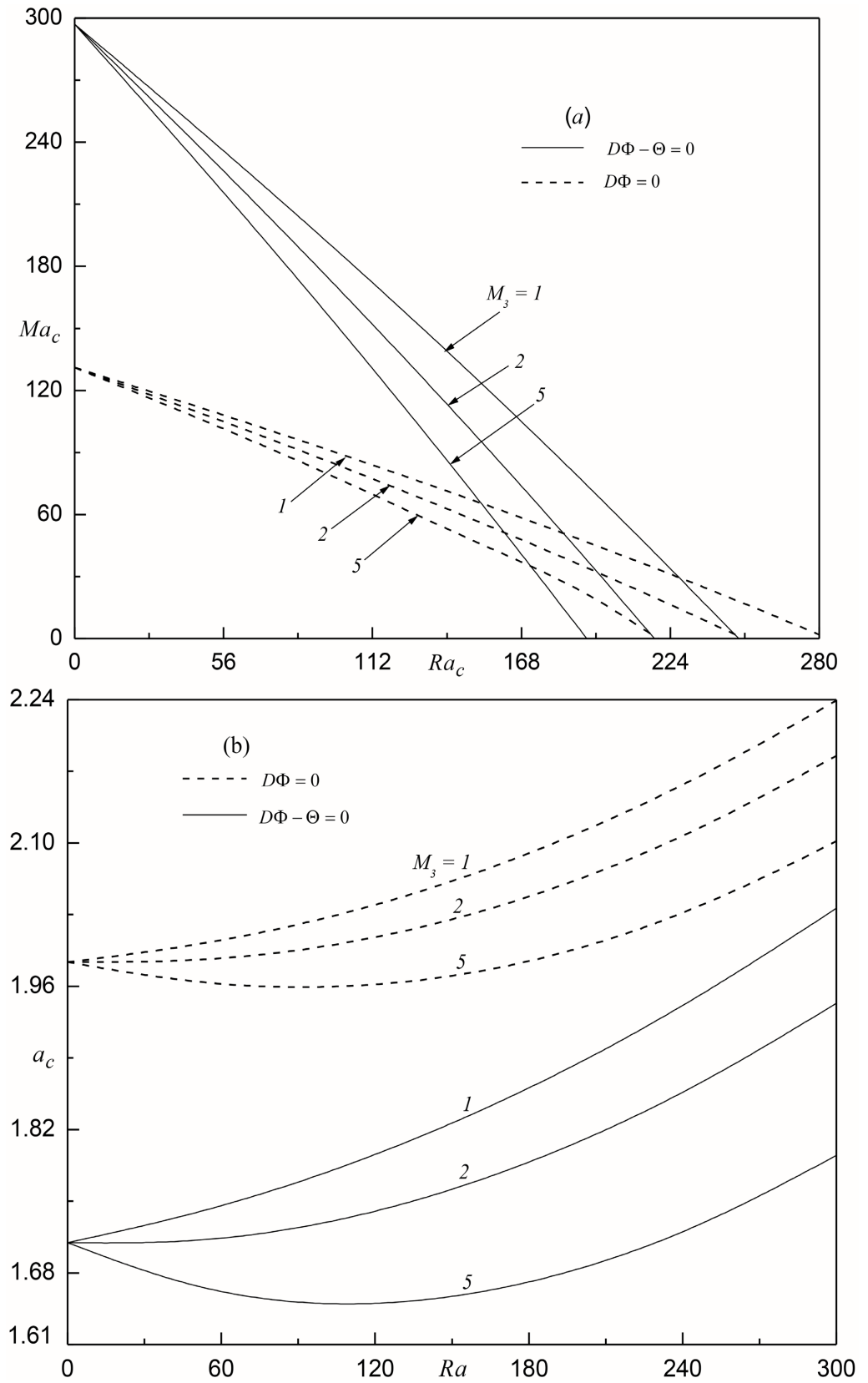


**Figure 2.** (a)  $Ma_c$  versus  $Ra_c$  with  $Bi$  when  $M_3=1$  and  $M_1=2$ ; (b)  $a_c$  versus  $Ra_c$  with  $Bi$  when  $M_3=1$  and  $M_1=2$ .





**Figure 3.** (a)  $Ma_c$  versus  $Ra_c$  with  $M_1$  when  $M_3 = 1$  and  $Bi = 2$ ; (b)  $a_c$  versus  $Ra$  with  $M_1$  when  $M_3 = 1$  and  $Bi = 2$ .



**Figure 4.** (a)  $Ma_c$  versus  $Ra_c$  with  $M_3$  when  $M_1=2$  and  $Bi=2$ ; (b)  $a_c$  versus  $Ra_c$  with  $M_3$  when  $M_1=2$  and  $Bi=2$ .

observed the stability parameters  $Ra_c$  and  $Ma_c$  decreases as increasing  $M_3$ , thus the mechanism of magnetization non-linearity parameter has a destabilizing effect on the system. Nonetheless,  $Ra_c$  and  $Ma_c$  are found to be independent of  $M_3$  for  $Bi = 0$ . While the value of  $a_c$  decreases as increasing in  $M_3$  and thus the effect is to enlarge size of convection cells.

## 5. Conclusions

The influence of general boundary conditions on buoyancy and surface tension-driven FTC in a FF layer is investigated numerically Galrkin technique based on weighted residual technique. The following conclusions were resulting:

- The initiation of FTC is inhibited with increasing Biot number  $Bi$ .
- The magnetic parameter  $M_1$  and fluid magnetization non-linearity parameter  $M_3$  hasten the FTC.
- The magnetic bounding surfaces  $D\Phi - \Theta$  offer more stabilizing while  $D\Phi$  surfaces offer least stable effects against FTC. *i.e.*  $(Ra_c \text{ or } Ma_c)_{D\Phi} < (Ra_c \text{ or } Ma_c)_{D\Phi - \Theta}$ .
- The critical value ( $a_c$ ) for  $D\Phi - \Theta$  is always higher than those of remaining boundaries. *i.e.*  $(a_c)_{D\Phi - \Theta} < (a_c)_{D\Phi}$ .

## Conflicts of Interest

The authors declare no conflicts of interest regarding the publication of this paper.

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