

Phase Portraits and Traveling Wave Solutions of a Fractional Generalized Reaction Duffing Equation

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Abstract

In this paper, we study the traveling wave solutions of the fractional generalized reaction Duffing equation, which contains several nonlinear conformable time fractional wave equations. By the dynamic system method, the phase portraits of the fractional generalized reaction Duffing equation are given, and all possible exact traveling wave solutions of the equation are obtained.

Keywords

Fractional Duffing Equation, Dynamic System Method, Traveling Wave Solution

1. Introduction

Some famous nonlinear fractional wave equations, such as the fractional Klein-Gordon equation, Landau-Ginzburg-Higgs equation, the fractional φ^4 equation, the fractional Duffing equation and the fractional Sine-Gordon equation, can be summarized as the fractional generalized reaction Duffing model. A lot of authors have done a lot of research on the exact solutions of this equation. By using the new ansatz method, the solitary wave solutions and periodic solutions of gRDM were obtained in [1]. Furthermore, the exact soliton solutions of gRDM have been obtained by using the generalized hyperbolic function method, the Bäcklund transformation obtained by the homogeneous balance method, the first integration method of the fractional derivative in the sense of the improved Riemann-Liouville derivative, and the compatible fractional complex transformation method, respectively in [2] [3] [4] [5]. Based on an extended first-type elliptic sub-equation method and its algorithm, the new bell-shaped and kink-shaped solitary wave solutions, triangular periodic wave solutions and singular solutions

of gRDM were solved in [6]. The accurate soliton solutions were obtained by using Bäcklund transformation of fractional Riccati equation, function variable method, and general projective Riccati equation [7] [8] [9]. In addition, other authors have used auxiliary function methods, Hermite transformation and Riccati equations, fractional sub-equations and other methods to study the exact solutions of gRDM in [10] [11] [12]. Recently, some new traveling wave solutions of the (2+1)-dimensional time-fractional Zoomeron equation and the superfield gardner equation have been obtained in [13] [14]. The fractional derivatives and fractional derivative equations have been deeply studied in [15] [16] [17] [18]. In this paper, we consider the following fractional order generalized reaction Duffing equation

$$D_t^{2\alpha} u + pu_{xx} + qu + ru^2 + su^3 = 0, \quad (1)$$

where p, q, r and s are all real constants, $0 < \alpha \leq 1$, and $D_t^{2\alpha} = D_t^\alpha D_t^\alpha$ is defined in Section 2. The following equations are special cases of Equation (1), for example

1) Fractional Klein-Gordon equation

$$D_t^{2\alpha} u - u_{xx} - au - bu^3 = 0, t > 0, 0 < \alpha \leq 1.$$

2) Fractional Landau-Ginzburg-Higgs equation

$$D_t^{2\alpha} u - u_{xx} - m^2 u + gu^3 = 0, t > 0, 0 < \alpha \leq 1.$$

3) Fractional φ^4 equation

$$D_t^{2\alpha} u - u_{xx} + u - u^3 = 0, t > 0, 0 < \alpha \leq 1.$$

4) Fractional Duffing equation

$$D_t^{2\alpha} u + au + bu^3 = 0, t > 0, 0 < \alpha \leq 1.$$

5) Fractional Sine-Gordon equation

$$D_t^{2\alpha} u + au + bu^3 = 0, t > 0, 0 < \alpha \leq 1.$$

In this paper, we use the dynamic system approach [19] [20] to study the phase portraits and traveling wave solutions of the Equation (1), and try to construct all possible exact traveling wave solutions of this equation.

The rest of this paper is organized as follows. In Section 2, we introduce some basic definitions and important properties of the fractional derivative. In Section 3, by applying the dynamic system approach [19] [20], we give the phase portraits of the Equation (1). In Section 4, we give all possible exact traveling wave solutions of the Equation (1) under different parameters. In Section 5, we state the main conclusions of this paper.

2. Definition and Properties of the Fractional Derivative

The idea of fractional derivatives originated from the semi-derivative discussed by Leibniz and Lospida in 1695. Subsequently, many authors studied fractional derivatives and formed several different definitions, such as Riemann-Liouville, Caputo and other fractional derivatives. In this section, we introduce the com-

mon fractional derivatives proposed by Khalil *et al.* [21]. Let $f : (0, +\infty) \rightarrow \mathbf{R}$. Then, the conformal fractional derivative of f of order α is defined as

$$D_t^\alpha f(t) = \lim_{\varepsilon \rightarrow 0} \frac{f(t + \varepsilon t^{1-\alpha}) - f(t)}{\varepsilon}, \quad (2)$$

for all $t > 0$, $\alpha \in (0, 1]$. And the conformal fractional derivative has the following properties. Let $\alpha \in (0, 1]$, and f, g be α -differentiable at a point $t > 0$. Then

$$\begin{aligned} D_t^\alpha t^s &= s t^{s-\alpha}, s \in \mathbf{R}, \\ D_t^\alpha [f(t)g(t)] &= g(t)D_t^\alpha f(t) + f(t)D_t^\alpha g(t). \end{aligned} \quad (3)$$

In addition, if f is differentiable, then

$$D_t^\alpha f(t) = t^{1-\alpha} \frac{df(t)}{dt}. \quad (4)$$

3. Phase Portraits of Equation (1)

Inspired by [22], we introduce the following fractional transformation

$$\xi = kx - \frac{n}{\alpha} t^\alpha, U(\xi) = u(t, x), \quad (5)$$

where k, n are all arbitrary constants. According to (3)-(4), it infers

$$D_t^\alpha D_t^\alpha u(t) = D_t^\alpha \left(t^{1-\alpha} \frac{dU(\xi)}{d\xi} \cdot \frac{d\xi}{dt} \right) = D_t^\alpha \left(-n \frac{dU(\xi)}{d\xi} \right) = n^2 \frac{d^2 U(\xi)}{d\xi^2}. \quad (6)$$

By (6), substituting Equation (5) into Equation (1), we get

$$(n^2 + pk^2)U'' + qU + rU^2 + sU^3 = 0, \quad (7)$$

where ' is the derivative with respect to ξ . Furthermore, it follows from [20] [23] that (7) is equivalent to the plane Hamiltonian system

$$\begin{aligned} \frac{dU}{d\xi} &= V, \\ \frac{dV}{d\xi} &= AU^3 + BU^2 + PU, \end{aligned} \quad (8)$$

with the Hamiltonian

$$H(U, V) = \frac{1}{2}V^2 - \frac{A}{4}U^4 - \frac{B}{3}U^3 - \frac{P}{2}U^2 = h,$$

where $A = -\frac{s}{n^2 + pk^2}$, $B = -\frac{r}{n^2 + pk^2}$, $P = -\frac{q}{n^2 + pk^2}$.

In order to study the phase pictures of the system (8), it is necessary to study the equilibrium points of the system (8). Let $\Delta = B^2 - 4AP$. When $\Delta = 0$, the system (8) has two equilibrium points $E_0(0, 0), E_1(-B/2A, 0)$. When $\Delta > 0$, the system has three equilibrium points $E_0(0, 0), E_2\left(\frac{-B + \sqrt{\Delta}}{2A}\right)$ and

$E_3\left(\frac{-B - \sqrt{\Delta}}{2A}, 0\right)$. When $\Delta < 0$, the system has only one equilibrium point

$E_0(0,0)$. Let $M(U_e, V_e)$ be the coefficient matrix of the linearized system of the system (8) at an equilibrium point $E_j (j = 0, 1, 2, 3)$. Let $J = \det(M(U_e, V_e))$. We have

$$\begin{aligned} J(E_0) &= -P, \\ J(E_1) &= 0, \\ J(E_2) &= \frac{B\sqrt{\Delta} - \Delta}{2A}, \\ J(E_3) &= -\frac{B\sqrt{\Delta} + \Delta}{2A}, \\ \text{Trace}(M(E_j)) &= 0, (j = 0, 1, 2, 3). \end{aligned}$$

By the planar dynamical theory [20], the above analysis and Maple, we obtain the following results and the phase portraits.

Case 1. $\Delta = 0$.

When $P > 0$, $E_0(0,0)$ is a saddle point and $E_1\left(-\frac{B}{2A}, 0\right)$ is a cusp point.

When $P < 0$, $E_0(0,0)$ is a center point and $E_1\left(-\frac{B}{2A}, 0\right)$ is a cusp point.

The corresponding phase portraits of the system (8) are shown in **Figure 1**.

Case 2. $\Delta > 0$.

When $P > 0$, $A > 0$ and $B < 0$, $E_0(0,0)$ and $E_2\left(\frac{-B + \sqrt{\Delta}}{2A}, 0\right)$ are saddle points and $E_3\left(-\frac{B + \sqrt{\Delta}}{2A}, 0\right)$ is a center point.

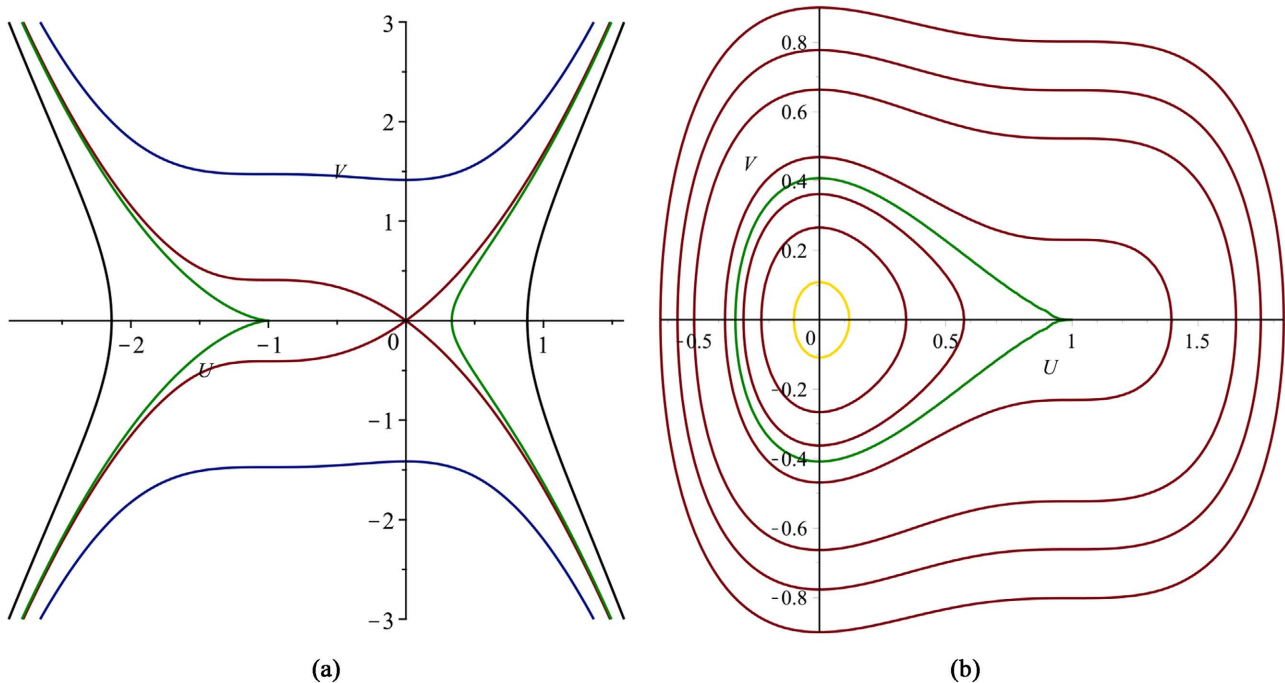


Figure 1. The phase portraits of the system (8). (a) $\Delta = 0, P > 0$; (b) $\Delta = 0, P < 0$.

When $P > 0$, $A > 0$ and $B > 0$, $E_0(0,0)$ and $E_3\left(-\frac{B+\sqrt{\Delta}}{2A}, 0\right)$ are saddle points and $E_2\left(\frac{-B+\sqrt{\Delta}}{2A}\right)$ is a center point.

When $P > 0$, $A < 0$, $E_0(0,0)$ is a saddle point, and $E_2\left(\frac{-B+\sqrt{\Delta}}{2A}\right)$ and $E_3\left(-\frac{B+\sqrt{\Delta}}{2A}, 0\right)$ are center points.

When $P < 0$, $A > 0$, $E_0(0,0)$ is a center point, and $E_2\left(\frac{-B+\sqrt{\Delta}}{2A}\right)$ and $E_3\left(-\frac{B+\sqrt{\Delta}}{2A}, 0\right)$ are saddle points.

When $P < 0$, $A < 0$ and $B > 0$, $E_0(0,0)$ and $E_3\left(-\frac{B+\sqrt{\Delta}}{2A}, 0\right)$ are center points and $E_2\left(\frac{-B+\sqrt{\Delta}}{2A}\right)$ is a saddle point.

When $C < 0$, $A < 0$ and $B < 0$, $E_0(0,0)$ and $E_2\left(\frac{-B+\sqrt{\Delta}}{2A}\right)$ are center points and $E_3\left(-\frac{B+\sqrt{\Delta}}{2A}, 0\right)$ is a saddle point.

When $C = 0$ and $A > 0$, $E_0(0,0)$ and $E_2(0,0)$ are cusp points and $E_3\left(-\frac{B+\sqrt{\Delta}}{2A}, 0\right)$ is a saddle point.

When $C = 0$ and $A < 0$, $E_0(0,0)$ and $E_2(0,0)$ are cusp points and $E_3\left(-\frac{B+\sqrt{\Delta}}{2A}, 0\right)$ is a center point.

The corresponding phase portraits of the system (8) are shown in **Figures 2-6**.

Case 3. $\Delta < 0$

When $P > 0$, $E_0(0,0)$ is a saddle point.

When $P < 0$, $E_0(0,0)$ is a center point.

The corresponding phase portraits of the system (8) are shown in **Figure 7**.

4. Exact Solutions of Equation (1)

We use the elliptic integral theory and direct integration method to give all possible explicit parameter representations of the traveling wave solution of Equation (1). We first denote

$$h_0 = H(0,0) = 0,$$

$$h_1 = H\left(-\frac{B}{2A}, 0\right) = \frac{5B^4}{192A^3} - \frac{PB^2}{8A^2},$$

$$\begin{aligned}
 h_2 &= H\left(\frac{-B+\sqrt{\Delta}}{2A}, 0\right) = -\frac{3W_1^4+8BW_1^3}{192A^3} - \frac{PW_1^2}{8A^2}, \\
 h_3 &= H\left(\frac{B+\sqrt{\Delta}}{2A}, 0\right) = -\frac{3W_2^4+8BW_2^3}{192A^3} - \frac{PW_2^2}{8A^2},
 \end{aligned}
 \tag{9}$$

where $W_1 = -B + \sqrt{\Delta}$, $W_2 = B + \sqrt{\Delta}$.

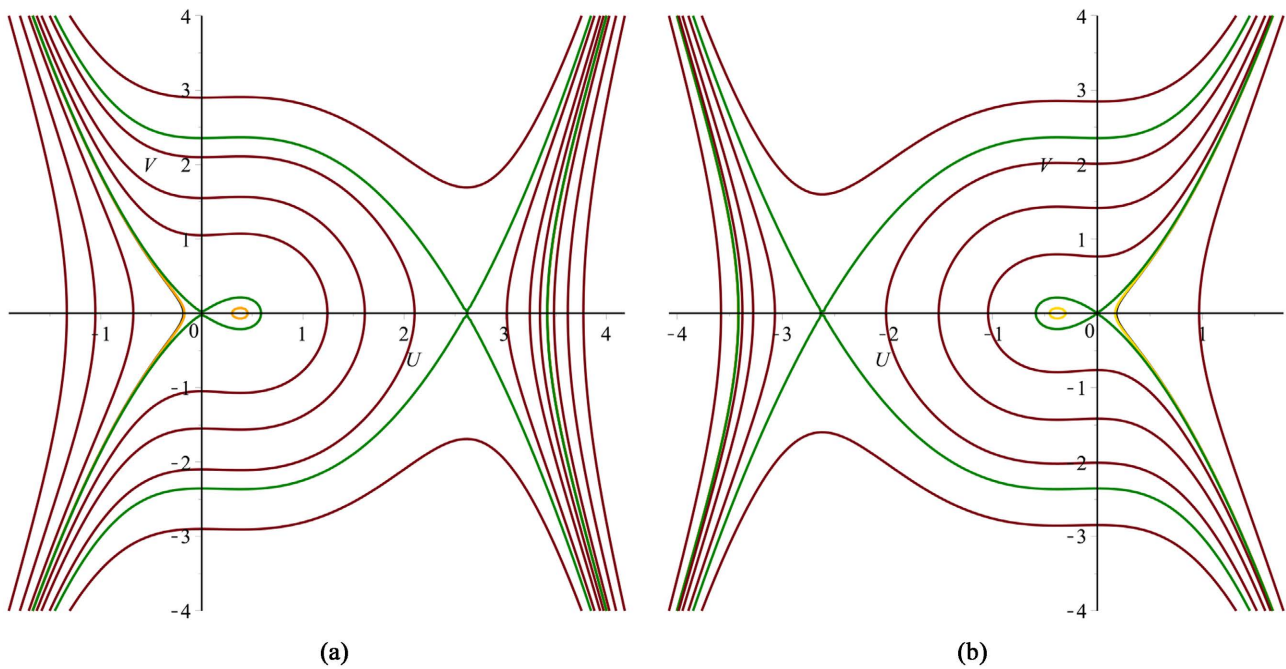


Figure 2. The phase portraits of the system (8). (a) $\Delta > 0, A > 0, B < 0, P > 0$; (b) $\Delta > 0, A > 0, B > 0, P > 0$.

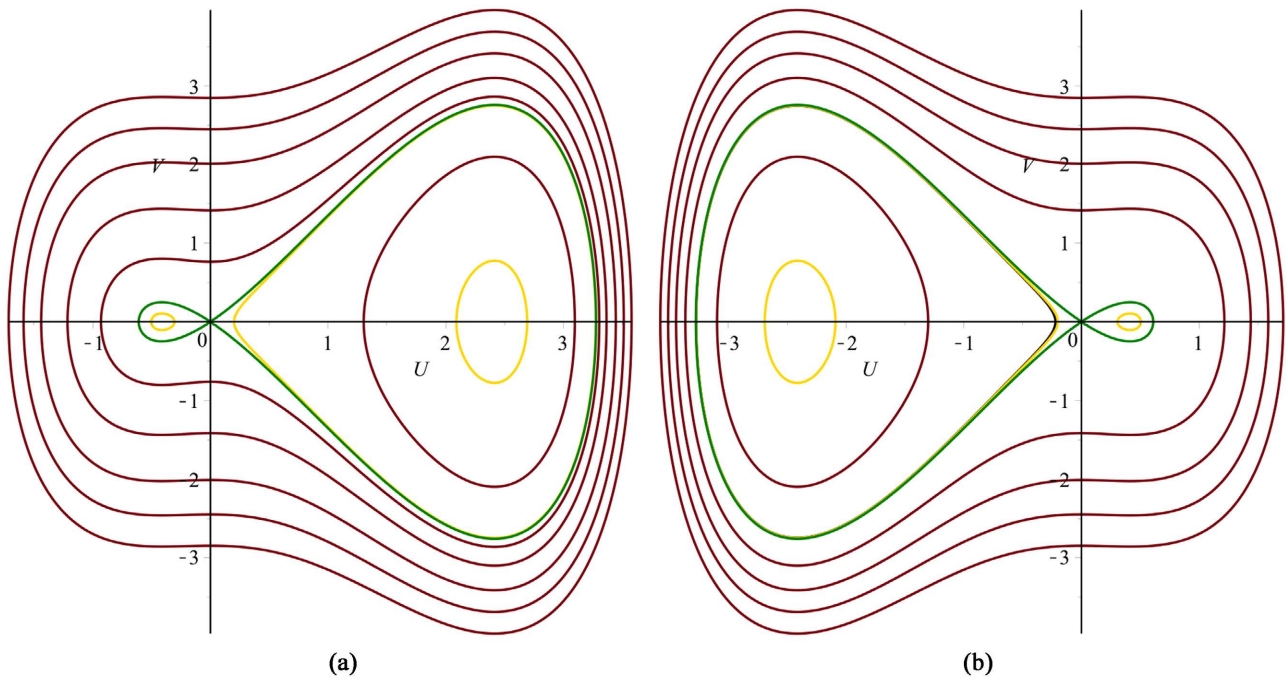


Figure 3. The phase portraits of the system (8). (a) $\Delta > 0, A < 0, B > 0, P > 0$; (b) $\Delta > 0, A < 0, B < 0, P > 0$.

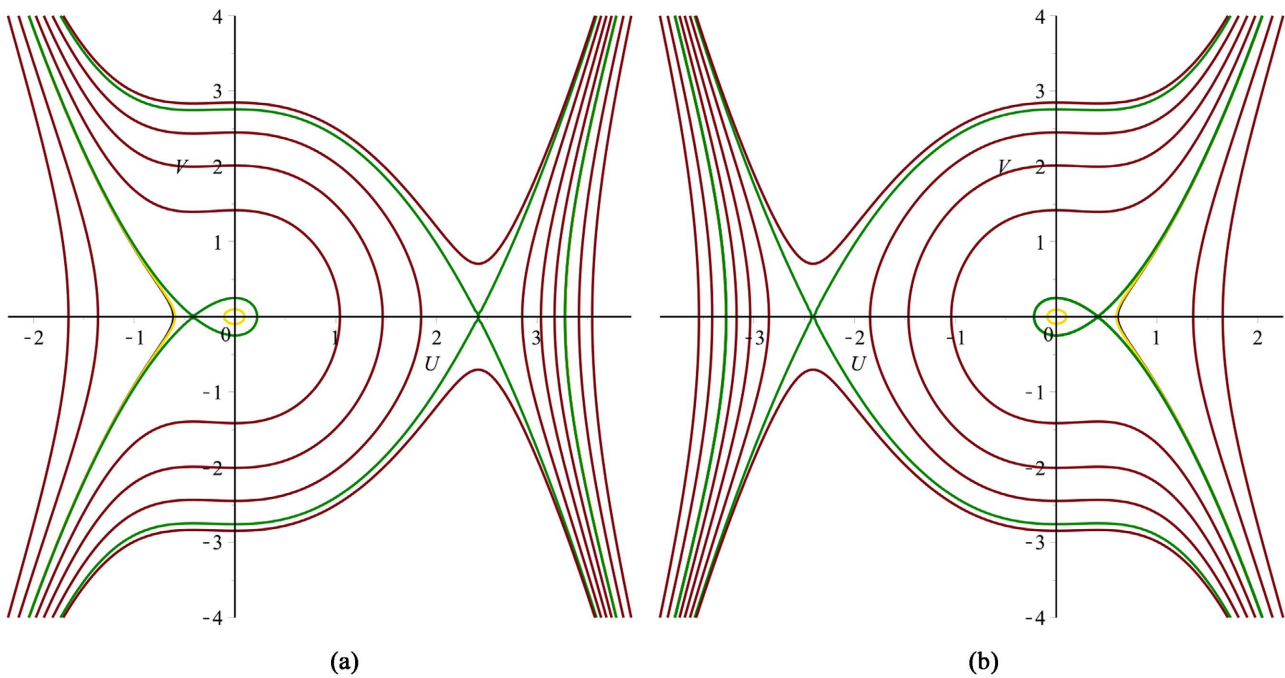


Figure 4. The phase portraits of the system (8). (a) $\Delta > 0, A > 0, B < 0, P < 0$; (b) $\Delta > 0, A > 0, B > 0, P < 0$.

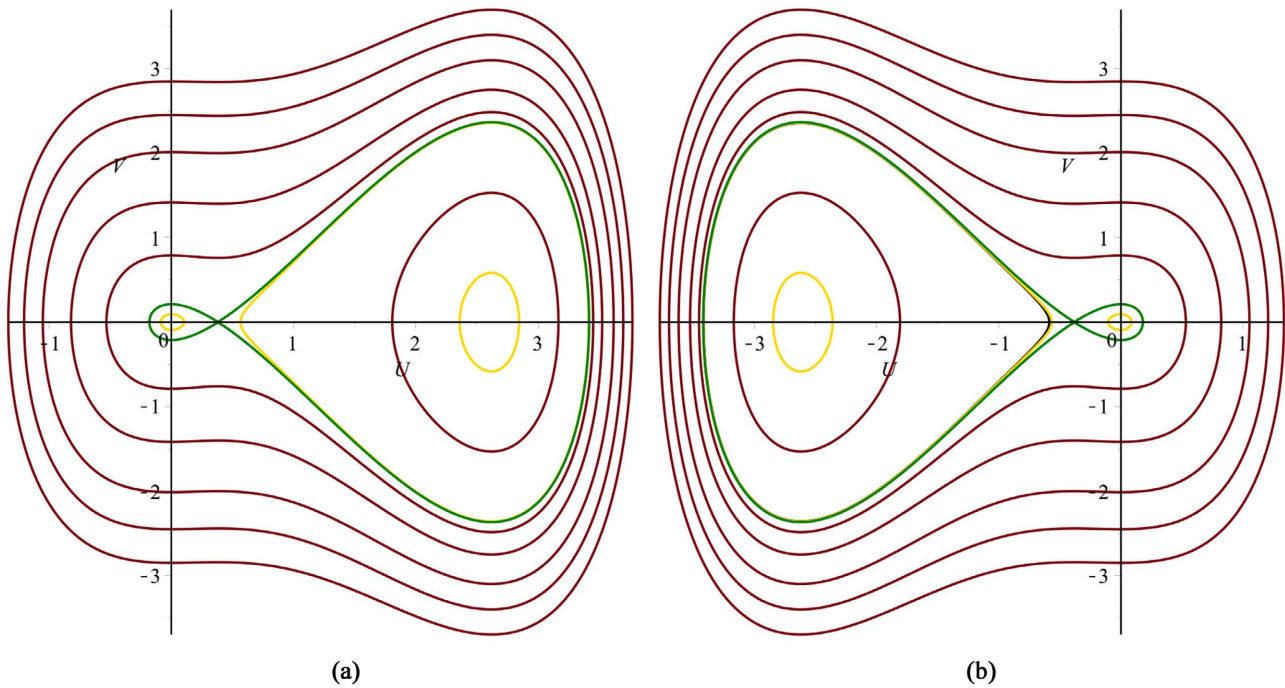


Figure 5. The phase portraits of the system (8). (a) $\Delta > 0, A < 0, B > 0, P < 0$; (b) $\Delta > 0, A < 0, B < 0, P < 0$.

4.1. Consider Case 1 in Section 3

By $\Delta = 0$, it obtains $PA > 0$.

(1) If $P > 0, A > 0$, corresponding to the homoclinic orbit $E_0(0,0)$ defined by $H(U,V) = h_0$ from (9), the Equation (1) has a solution of shown in **Figure 1(a)**. By $H(U,V) = h_0 = 0$, it gets

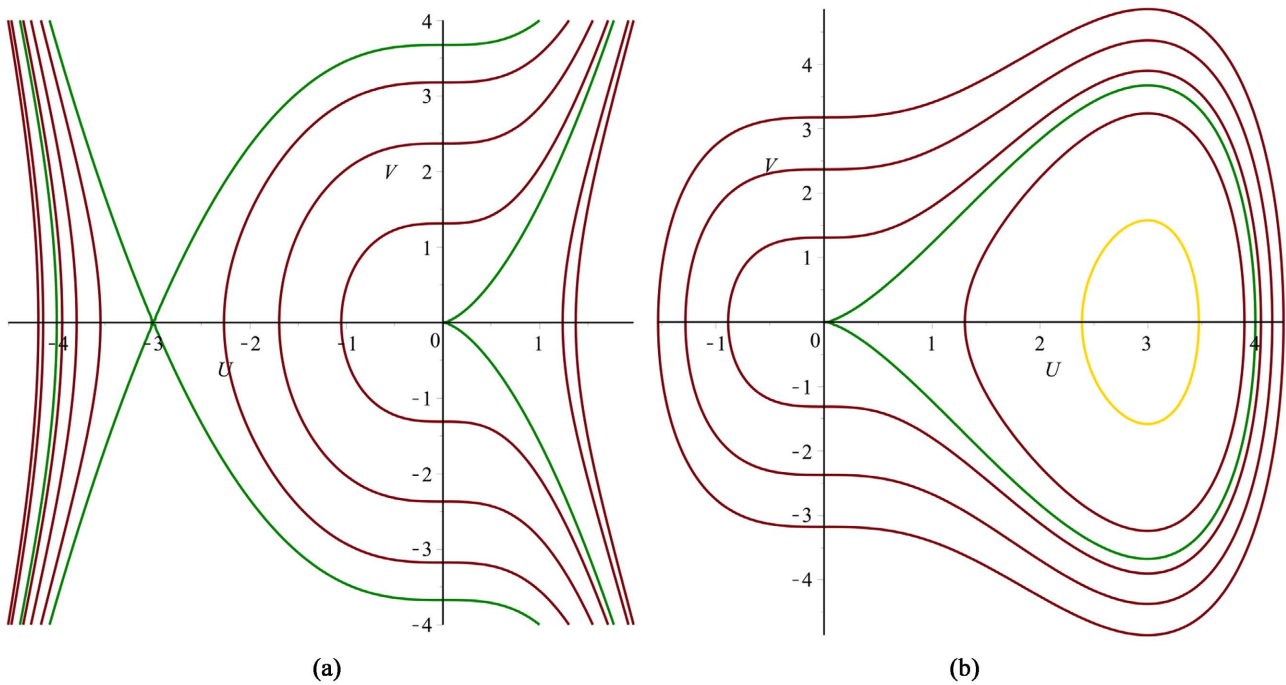


Figure 6. The phase portraits of the system (8). (a) $\Delta > 0, A > 0, P = 0$; (b) $\Delta > 0, A < 0, P = 0$.

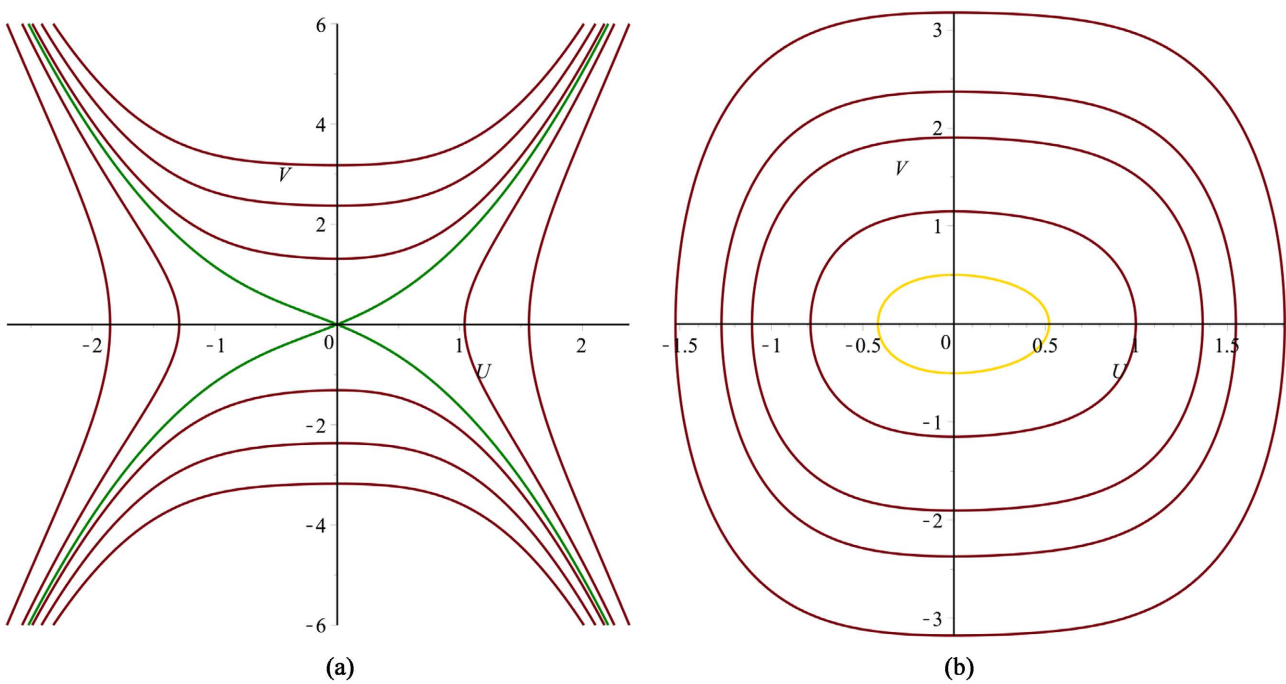


Figure 7. The phase portraits of the system (8). (a) $\Delta < 0, A > 0, P > 0$; (b) $\Delta < 0, A < 0, P < 0$.

$$V = \pm U \sqrt{\frac{A}{2}} \sqrt{\left(U + \frac{2B}{3A}\right)^2 + \frac{2PA}{9A^2}}. \tag{10}$$

Using the first equation of system (8) and equation (10), we get the following parameter expression

$$u(t, x) = \pm \frac{8A^2 M_1 e^{-\frac{1}{3}\xi\sqrt{AM_1}}}{e^{\frac{2}{3}\xi\sqrt{AM_1}} A^2 - 72A^2 M_1 - 24ABe^{-\frac{1}{3}\xi\sqrt{AM_1}} + 144B^2}, \tag{11}$$

where $M_1 = \frac{AP + 2B^2}{A^2}$, $A = -\frac{s}{n^2 + pk^2}$, $B = -\frac{r}{n^2 + pk^2}$, $P = -\frac{q}{n^2 + pk^2}$, and $\xi = kx - \frac{n}{\Gamma(1+\alpha)}t^\alpha$. The solution (11) is shown in **Figure 1(a)** with $A = 1$, $B = 2$, $C = 1$.

2) If $P < 0$, $A < 0$, corresponding to the homoclinic orbit $E_0(0,0)$ defined by $H(U, V) = h_0$, the Equation (1) has a solution of shown in **Figure 1(b)**. By $H(U, V) = h_0 = 0$, it gets

$$V = \pm U \sqrt{-\frac{A}{2} \sqrt{\left(U + \frac{2B}{3A}\right)^2 + \frac{2PA}{9A^2}}}. \tag{12}$$

By (8) and Equation (12), we get

$$u(t, x) = \pm \frac{8A^2 M_1 e^{-\frac{1}{3}\xi\sqrt{-AM_1}}}{e^{\frac{2}{3}\xi\sqrt{-AM_1}} A^2 - 72A^2 M_1 - 24ABe^{-\frac{1}{3}\xi\sqrt{-AM_1}} + 144B^2}, \tag{13}$$

where $M_1 = \frac{AP + 2B^2}{A^2}$, $A = -\frac{s}{n^2 + pk^2}$, $B = -\frac{r}{n^2 + pk^2}$, $P = -\frac{q}{n^2 + pk^2}$, and $\xi = kx - \left(\frac{n}{\Gamma(1+\alpha)}t^\alpha\right)$. The solution (13) is shown in **Figure 1(b)** with $A = -1$, $B = 2$, $C = -1$.

4.2. Consider Case 2 in Section 3

1) If $P = 0$, $A > 0$, corresponding to the homoclinic orbit $E_0(0,0)$ defined by $H(U, V) = h_0$, Equation (1) has a solution of shown in **Figure 6(a)**. By $H(U, V) = h_0 = 0$, it infers

$$V = \pm U \sqrt{\frac{A}{2} \sqrt{\left(U + \frac{4B}{3A}\right)U}}. \tag{14}$$

Combining the first equation of system (8) and Equation (14), we have

$$u(t, x) = \frac{12B}{2\xi^2 B^2 - 9A}, \tag{15}$$

where $A = -\frac{s}{n^2 + pk^2}$, $B = -\frac{r}{n^2 + pk^2}$, and $\xi = kx - \frac{n}{\Gamma(1+\alpha)}t^\alpha$. The solution (15) is shown in **Figure 6(a)** with $A = 1$, $B = 3$.

2) If $P = 0$, $A < 0$, corresponding to the homoclinic orbit $E_0(0,0)$ defined by $H(U, V) = h_0$, the Equation (1) has a solution of shown in **Figure 6(b)**. By $H(U, V) = h_0 = 0$, it gets

$$V = \pm U \sqrt{-\frac{A}{2} \sqrt{\left(U + \frac{4B}{3A}\right)U}}. \tag{16}$$

Applying (8) and (16), we get

$$u(t, x) = -\frac{12B}{2\xi^2 B^2 + 9A}, \tag{17}$$

where $A = -\frac{s}{n^2 + pk^2}$, $B = -\frac{r}{n^2 + pk^2}$, and $\xi = kx - \frac{n}{\Gamma(1+\alpha)}t^\alpha$. The solution (17) is shown in **Figure 6(b)** with $A = -1$, $B = 3$.

3) If $P > 0$, $A > 0$ and $\Delta > 8PA$ or $P < 0$, $A < 0$ and $\Delta > 8PA$, corresponding to the homoclinic orbit $E_0(0,0)$ defined by $H(U, V) = h_0$, Equation (1) has the solution of shown in **Figure 2** or **Figure 5**. By $H(U, V) = h_0 = 0$, it obtains

$$V = \pm U \sqrt{\frac{A}{2} \sqrt{\left(U + \frac{2B}{3A}\right)^2 + \frac{18PA - 4B^2}{9A^2}}}. \tag{18}$$

It follows from (8) and (18), we obtain

$$u(t, x) = \frac{24A^2 M_2 e^{\mp \xi \sqrt{P}}}{\left(e^{\mp \xi \sqrt{P}}\right)^2 A^2 - 72A^2 M_2 - 8Ae^{\mp \xi \sqrt{P}} B + 16B^2},$$

where $M_2 = \frac{P}{A}$, $A = -\frac{s}{n^2 + pk^2}$, $B = -\frac{r}{n^2 + pk^2}$, $P = -\frac{q}{n^2 + pk^2}$, and

$$\xi = kx - \frac{n}{\Gamma(1+\alpha)}t^\alpha.$$

4) If $P > 0$, $A < 0$ or $P < 0$, $A > 0$ corresponding to the homoclinic orbit $E_0(0,0)$ defined by $H(U, V) = h_0$, Equation (1) has the solution of shown in **Figure 3** or **Figure 4**. By $H(U, V) = h_0 = 0$, it gets

$$V = \pm U \sqrt{-\frac{A}{2} \sqrt{\left(U + \frac{2B}{3A}\right)^2 + \frac{18PA - 4B^2}{9A^2}}}. \tag{19}$$

Using the first equation of system (8) and Equation (19), we get the following parameter expression:

$$u(t, x) = \frac{24A^2 M_2 e^{\mp \xi \sqrt{-P}}}{\left(e^{\mp \xi \sqrt{-P}}\right)^2 A^2 - 72A^2 M_2 - 8Ae^{\mp \xi \sqrt{-P}} B + 16B^2},$$

where $M_2 = \frac{P}{A}$, $A = -\frac{s}{n^2 + pk^2}$, $B = -\frac{r}{n^2 + pk^2}$, $P = -\frac{q}{n^2 + pk^2}$, and

$$\xi = kx - \frac{n}{\Gamma(1+\alpha)}t^\alpha.$$

5) If $P > 0$, $A > 0$ or $P < 0$, $A > 0$ corresponding to the homoclinic orbit $E_0(0,0)$ defined by $H(U, V) = h_0$ has the solution of shown in **Figure 2** or **Figure 4**. It follows from $H(U, V) = h_0 = 0$ that

$$V = \pm \sqrt{\frac{A}{2} \sqrt{(U - U_4)(U - U_5)(U_6 - U)(U_7 - U)}}. \tag{20}$$

The relation $U_4 < U_5 < U < U_6 < U_7$ holds on the U -axis. Therefore, by using

the first equation of system (8) and equation (20), we get the following parameter expression

$$u(t, x) = 1 + \frac{U_7(U_5 + U_6 - U_7) - U_5U_6}{sn^2\left(\frac{|\xi|}{g}\sqrt{\frac{A}{2}}\right)(U_5 - U_6) - U_5 + U_7},$$

where $A = -s/(n^2 + pk^2)$, $g = \frac{2}{\sqrt{(U_7 - U_5)(U_6 - U_4)}}$ and

$$\xi = kx - \frac{n}{\Gamma(1+\alpha)}t^\alpha.$$

4.3. Consider Case 3 in Section 3

1) If $P < 0$, $A < 0$, corresponding to the homoclinic orbit $E_0(0, 0)$ defined by $H(U, V) = h_0$, Equation (1) has the solution of shown in **Figure 7(b)**. By $H(U, V) = h_0 = 0$, it gets

$$V = \pm U \sqrt{-\frac{A}{2} \sqrt{\left(U + \frac{2B}{3A}\right)^2 + \frac{2PA}{9A^2}}}. \quad (21)$$

Using the first equation of system (8) and Equation (21), we get the following parameter expression

$$u(t, x) = \pm \frac{8A^2M_1e^{\frac{1}{3}\xi\sqrt{-AM_1}}}{e^{-\frac{2}{3}\xi\sqrt{-AM_1}}A^2 - 72A^2M_1 - 24ABe^{-\frac{1}{3}\xi\sqrt{-AM_1}} + 144B^2}, \quad (22)$$

where $M_1 = \frac{AP + 2B^2}{A^2}$, $A = -\frac{s}{n^2 + pk^2}$, $B = -\frac{r}{n^2 + pk^2}$, $P = -\frac{q}{n^2 + pk^2}$,

and $\xi = kx - \frac{n}{\Gamma(1+\alpha)}t^\alpha$. The solution (22) is shown in **Figure 7(b)** with

$$A = -2, \quad B = 1, \quad C = -1.$$

(2) If $P > 0$, $A > 0$, corresponding to the homoclinic orbit $E_0(0, 0)$ defined by $H(U, V) = h_0$, Equation (1) has the solution of shown in **Figure 7(a)**. By $H(U, V) = h_0 = 0$, it gets

$$V = \pm U \sqrt{\frac{A}{2} \sqrt{\left(U + \frac{2B}{3A}\right)^2 + \frac{2PA}{9A^2}}}. \quad (23)$$

Using the first equation of system (8) and Equation (23), we get the following parameter expression

$$u(t, x) = \pm \frac{8A^2M_1e^{\frac{1}{3}\xi\sqrt{AM_1}}}{e^{-\frac{2}{3}\xi\sqrt{AM_1}}A^2 - 72A^2M_1 - 24ABe^{\frac{1}{3}\xi\sqrt{AM_1}} + 144B^2}, \quad (24)$$

where $M_1 = \frac{AP + 2B^2}{A^2}$, $A = -\frac{s}{n^2 + pk^2}$, $B = -\frac{r}{n^2 + pk^2}$, $P = -\frac{q}{n^2 + pk^2}$,

and $\xi = kx - \frac{n}{\Gamma(1+\alpha)}t^\alpha$. The solution (24) is shown in **Figure 7(a)** with

$$A = 2, \quad B = 1, \quad C = 1.$$

5. Conclusion

In conclusion, we obtained the phase portraits of the traveling wave system by using the fractional complex transformation and the dynamical system method [19] [20]. Moreover, we construct all possible accurate traveling wave solutions of Equation (1) under different parameter conditions.

Data Availability

The data used to support the findings of this study are available from the corresponding author upon request.

Conflicts of Interest

The authors declare no conflicts of interest regarding the publication of this paper.

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