

# Asymptotic Expansion of Temperature Close to a Singularity of a Plate

Isabelle Titeux

Laboratoire de Génie Civil, Université de Reims Champagne Ardenne, Moulin de la Housse, Reims, France

E-mail: [isabelle.titeux@univ-reims.fr](mailto:isabelle.titeux@univ-reims.fr)

Received March 22, 2011; revised April 21, 2011; accepted May 5, 2011

## Abstract

The thermal conduction in a thin laminated plate is considered here. The lateral surface of the plate is not regular. Consequently, the boundary of the middle plane admits a geometrical singularity. Close to the origin, the lateral edge forms an angle. We shall prove that the classical bidimensional problem associated with the thin plate problem is not valid. In this paper, using the boundary layer theory, we describe the local behavior of the plate, close to the perturbation.

**Keywords:** Thin Plate, Boundary Layers, Singularities, Asymptotic Expansion

## 1. Introduction

A thin plate is a three dimensional body, a dimension of which (the thickness) is smaller than the other dimensions. Usually, under the assumption of small thickness with respect to the characteristic length of the middle plane, instead of a three-dimensional description, a bi-dimensional one is used. The problem is then posed over the middle plane of the plate. In this way, the numerical methods are less expensive in time and in memory.

In this paper, we deal with the modelling of the thermal behavior of a thin laminated plate. The thermal conductivity can be considered as an exemplary problem similar to the elasticity problem. Instead of displacement, the unknown is the temperature, but the equations are similar.

The temperature and thermal flux established by the asymptotic expansion are good approximations. But close to the lateral surface, the bi-dimensional behavior is not suited: for a laminated body, boundary conditions are only satisfied on average. However, on the edge damage phenomena can appear, like delamination, crack... A bi-dimensional description of the behavior of the plate is not enough. In order to predict these phenomena, we need a good, local description of the behavior of the plate, in these areas. In this case, the bi-dimensional expansion is no more sufficient, we need a local three-dimensional description, which is valid only close to the lateral surface. Moreover, the distance to the edge and the position in the thickness have the same range of

magnitude; the assumption of small thickness with respect to the other directions is no more valid. Close to the edge, the body must be considered like a three-dimensional domain, with thickness and distance to the edge of the same order.

In previous works, the cases of a classical regular edge [1] and edge with a local perturbation [2] were considered. Recently, Saidi *et al.* [3,4] studied singularities in the edge of moderately thick plates. They studied the effect of the boundary layer term added to the Mindlin's plate theory. In this paper, the case of thin laminated plate with an angle in the lateral edge is considered. We lose the symmetry of the local perturbation [2] and new arguments must be used. Because of this angle, the boundary of the plate cannot be considered as a smooth surface. The boundary layer theory must be adapted to take into account the new geometry of the perturbed edge. Therefore, we obtain a new local description which is posed on an unbounded domain. The existence and uniqueness of the solution must be proved in order to implement a numerical method of resolution.

## 2. Generalities and Description of a Thin Laminated Plate

### 2.1. Classical Problem for a Thin Plate

Insert **Figure 1**: The plate  $P^\varepsilon$

Let us consider a thin plate  $P^\varepsilon = \omega \times (-\varepsilon, \varepsilon)$  characterized by its middle plane  $\omega \subset \mathbb{R}^2$  and its thickness

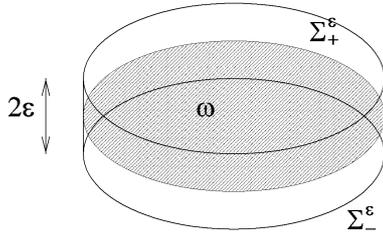


Figure 1. The plate  $P^\epsilon$ .

$2\epsilon$  (cf. **Figure 1**). In fact,  $\epsilon$  denotes the ratio between the characteristic length of the middle plane of the plate and the thickness. Let  $\Sigma_+^\epsilon \equiv \omega \times \{+\epsilon\}$  and  $\Sigma_-^\epsilon \equiv \omega \times \{-\epsilon\}$  denote the upper and lower faces respectively and  $\Gamma^\epsilon \equiv \partial\omega \times (-\epsilon, +\epsilon)$  denotes the lateral edge.

Coordinates in the middle plane are  $(X_1, X_2)$  and position in the thickness is  $X_3$ . Symbols in boldface denote vectors. We use the summation convention on repeated indices. Latin indices take their values in the set  $\{1, 2, 3\}$  while Greek ones take their values in the set  $\{1, 2\}$ .

For given external sources of heat, we have to determine the temperature field  $u^\epsilon = u^\epsilon(X_1, X_2, X_3)$ . The thermal flux vector is related to  $u^\epsilon$  by the constitutive law

$$\sigma_i^\epsilon \equiv \sigma_i(u^\epsilon) = k_{ij} \left( \frac{\partial u^\epsilon}{\partial X_j} \right), i = 1, 2, 3$$

The coefficients  $k_{ij}$  are the conductivity coefficients. They satisfy symmetry and coerciveness properties:

$$k_{ij} = k_{ji}, \forall i, j = 1, 2, 3,$$

$$k_{ij} \xi_i \xi_j \geq C \xi_i \xi_i, C > 0, \forall \xi \in \mathbb{R}^3.$$

The equilibrium equation is

$$-\frac{\partial \sigma_i^\epsilon}{\partial X_i} = f^\epsilon(X_1, X_2, X_3) \text{ in } P^\epsilon. \tag{2.1}$$

The order of magnitude of  $f^\epsilon$  is  $O(1)$  it means that  $f^\epsilon$  has the same order than the characteristic length of the middle plane. The upper and lower faces of the plate are free of heat source

$$\sigma_i^\epsilon n_i = 0 \text{ on } \Sigma_+^\epsilon \text{ and } \Sigma_-^\epsilon \tag{2.2}$$

On the lateral edge of the plate, there are Neumann's boundary conditions:

$$\sigma_i(u^\epsilon) n_i = \varphi^\epsilon(X_1, X_2, X_3) \text{ on } \Gamma^\epsilon, \tag{2.3}$$

where  $\varphi^\epsilon$  is  $O(1)$  and  $\mathbf{n}$  is the outer normal.

The external sources of heat satisfy the compatibility condition

$$\int_{P^\epsilon} f^\epsilon dX + \int_{\Gamma^\epsilon} \varphi^\epsilon dS = 0$$

The plate is laminated, *i.e.* composed of several materials. We assume that the interfaces between two materials are parallel to the middle plane of the plate. In this way, the conductivity coefficients depend on the position in the thickness  $\frac{X_3}{\epsilon}$ , we assume that they do not depend on the other variables:

$$k_{ij} = k_{ij} \left( \frac{X_3}{\epsilon} \right), i, j = 1, 2, 3.$$

At the interface between two different materials, the temperature and the normal thermal flux are continuous:

$$\llbracket u^\epsilon \rrbracket = 0 \text{ across the interfaces,} \tag{2.4}$$

$$\llbracket \sigma_i^\epsilon n_i \rrbracket = 0 \text{ across the interfaces,} \tag{2.5}$$

where the brackets denote the jump across the interfaces.

Problem (2.1)-(2.5) is the plate problem.

**Remark 1.** In (2.1) and (2.3), external sources of heat are taken with an order of magnitude of 1 in order to get an asymptotic expansion of the solution with the leading term  $O(1)$  (see (2.7) thereafter). But, because of the linearity of the problem, if the external sources of heat are multiplied by a constant (even depending on  $\epsilon$ ), the solution is also multiplied by the same constant.

Using the change of variables

$$\begin{cases} x = (x_1, x_2, 0); x_\alpha = X_\alpha \\ y = (0, 0, y_3); y_3 = \frac{X_3}{\epsilon} \end{cases} \tag{2.6}$$

the asymptotic expansion theory [5,6] involves temperature of the form

$$u^\epsilon = u^0(x) + \epsilon \left( \frac{\partial u^0}{\partial x_\alpha} w^\alpha(y_3) + \hat{u}^1(x) \right) + \dots \tag{2.7}$$

The functions  $w^\alpha$  only depend on the conductivity coefficients; they are solutions of the variational problems

$$\text{Find } w^\alpha \in \tilde{H}^1(-1, 1) \text{ such that } \forall v \in \tilde{H}^1(-1, 1)$$

$$\int_{-1}^1 k_{ij} \frac{\partial w^\alpha}{\partial y_j} \frac{\partial v}{\partial y_i} dy_3 = - \int_{-1}^1 k_{\alpha j} \frac{\partial v}{\partial y_j} dy_3$$

$$\text{where } \tilde{H}^1(-1, 1) \equiv \left\{ v \in H^1(-1, 1) : \int_{-1}^1 v(y_3) dy_3 = 0 \right\}.$$

The change of variables (2.6) is equivalent to dilate the thickness of the plate. In this way, we obtain a new plate  $P$  which does not depend on  $\epsilon$  (cf. **Figure 2**). All the directions of the plate have now the same range of magnitude. The thickness of  $P$  is no more small with respect to the other directions. We shall denote by  $\Sigma_+ \equiv \omega \times \{1\}$  and  $\Sigma_- \equiv \omega \times \{-1\}$  the upper and lower faces of the plate  $P$ , and by  $\Gamma \equiv \partial\omega \times (-1, 1)$  the lateral

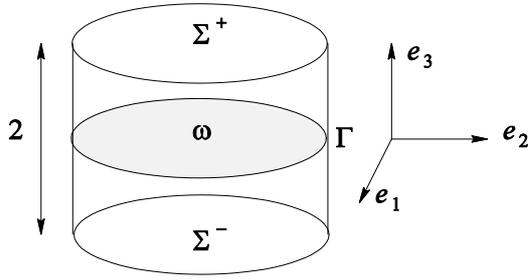


Figure 2. The plate  $P$ .

edge.

Insert **Figure 2** The plate  $P$ .

Let us remind certain features of the asymptotic structure of the plate problem [5,6]. The asymptotic structure of the mean value of the thermal flux is of the form:

$$\tilde{\sigma}_i^0 = k_{i\alpha}^h \frac{\partial u^0}{\partial x_\alpha} \text{ on } \omega,$$

where the tilde denotes the average on the thickness and  $\sigma^0$  is the leading term of the thermal flux. The homogenized conductivity coefficients are given by

$$k_{\alpha\beta}^h \equiv \int_{-1}^1 k_{\beta j} \left( \delta_{j\alpha} + \frac{\partial w^\alpha}{\partial y_j} \right) dy_3, \alpha, \beta = 1, 2,$$

$k_{3i} \equiv 0, i = 1, 2, 3$ . The problem for  $\tilde{\sigma}_i^0$  is posed over the middle plane. So that it is a bi-dimensional problem

$$-\frac{\partial \tilde{\sigma}_i^0}{\partial x_\alpha} = \tilde{f} \text{ in } \omega \tag{2.8}$$

$$\tilde{\sigma}_i^0 n_i = \tilde{\varphi} \text{ on } \partial\omega \tag{2.9}$$

where  $f$  and  $\varphi$  are the leading terms of  $f^\varepsilon$  and  $\varphi^\varepsilon$  respectively.

If the plate is laminated, it means that the plate is not homogeneous. Equations (2.3) and (2.9) are not equivalent: the mean value is different from the value on each point of the lateral surface. Consequently, the asymptotic solution is not valid everywhere on the plate. Close to the edge, a corrective term must be added.

### 2.2. Behavior of the Thin Plate Close to a Classical edge

It can be important to have a good approximation of the boundary of the plate, if for instance the damage is studied. As a matter of fact the cracks appear on the edge, like delamination. In this case, a local three-dimensional description of the behavior of the plate is necessary.

On the lateral edge the assumption of very small  $\varepsilon$  with respect to the other variables is not justified. Distance to the edge is of the same range of magnitude than the thickness of the plate.

Insert **Figure 3** The specific directions.

In order to study the temperature close to the edge, let us define local axes  $Oy$  (cf. **Figure 3**):  $Oy_1$  is the tangent direction of the edge of the middle plane  $\partial\omega$ ,  $Oy_2$  is normal to  $\partial\omega$  in the middle plane, pointing inside  $\omega$ ,  $Oy_3$  is normal to  $\omega$ .

A corrective term is added to the asymptotic expansion of the temperature [1] to improve it. In order to act on the leading term of the thermal flux, we have to correct the second term of the temperature. As a matter of fact, if we act on the first term  $u^0$ , we shall change the order of the thermal flux.

Let  $u^{1c}$  be the corrective term of the temperature, the new asymptotic expansion close to the edge is

$$u^\varepsilon = u^0(x_1, x_2) + \varepsilon \left( \frac{\partial u^0}{\partial x_\alpha} w^\alpha(y_3) + \hat{u}^1(x) + u^{1c}(x_1, x_2; y_2, y_3) \right) + \dots \tag{2.10}$$

The corrective term must depend on the position in the thickness  $y_3$  and on the distance to the lateral edge  $y_2$ . The position on the edge  $(x_1, x_2)$  is a parameter. So that, it is defined in a semi infinite strip,

$$S \equiv \{(y_2, y_3) : y_2 \in (0, +\infty), y_3 \in (-1, 1)\} \tag{2.11}$$

It can be proved [6] that  $u^{1c}$  is the unique solution of the variational problem

Find  $u^{1c} \in W$  such that

$$\forall v \in \dot{W} \equiv \{v \in (C^\infty(S)) / \mathbb{R} : v \text{ with bounded support}\}$$

$$\int_S k_{ij} \frac{\partial u^{1c}}{\partial y_j} \frac{\partial v}{\partial y_i} dy_3 dy_2 = \tag{2.12}$$

$$\int_{-1}^1 [\sigma_i^0 n_i + \varphi]_{(x_1, x_2) \in \partial\omega} [v]_{y_2=0} dy_3 \equiv \Phi(v)$$

where  $W$  is the completed space of  $\dot{W}$  for the norm associated with

$$(v, w)_W \equiv \int_S \nabla v \cdot \nabla w dy_2 dy_3 \tag{2.13}$$

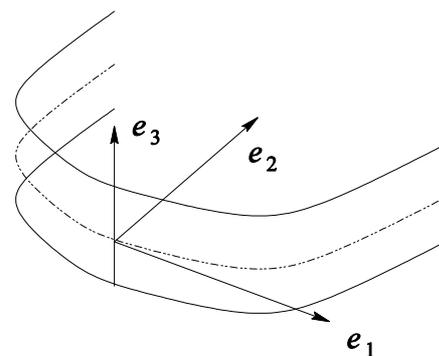


Figure 3. The specific directions.

The separation of variables method [6,7], allows to assume that the corrective term decreases exponentially.

### 3. Boundary Layer Close to an Angle

As it was seen in subsection 2.2, the corrective term allows to improve the description of the thermal flux close to a regular edge of the plate. In the same way, the behavior of the plate close to an angle, can be given by an asymptotic expansion with a new corrective term, a new boundary layer term.

Now, the boundary of the plate is not regular, it admits a perturbation. Close to the origin, the edge forms an angle of magnitude  $2\beta$ . (cf. **Figure 4**). The middle plane of the plate is no more regular. The lateral edge  $\Gamma$  can be split into two parts:  $\Gamma^1 \equiv \gamma_1 \times (-1, 1)$  and  $\Gamma^2 \equiv \gamma_2 \times (-1, 1)$ .

Figure 4 The perturbation of the edge

In order to lighten the notations, we shall assume that  $\varphi$  vanishes in the vicinity of the origin.

The edge is assumed to be regular everywhere but not in the vicinity of the origin.

Far from the origin, but on the lateral edge, the boundary layer problems are similar to those described in section 2, corresponding to a classical, regular surface.

Let  $u^{1cl}$  denotes the corrective term on  $\Gamma^1$  far from the origin. In the same way, let  $u^{1c2}$  denotes the corrective term on  $\Gamma^2$  far from the origin. These functions  $u^{1cl}$ ,  $l=1,2$ , are solutions of the variational problem (2.12) with unknown  $u^{1cl}$  instead of  $u^{1c}$ .

We can also prove that they are solutions of

$$-\frac{\partial}{\partial y_i} \left( k_{ij} \frac{\partial u^{1cl}}{\partial y_j} \right) = 0 \text{ in } S \tag{3.1}$$

$$k_{3j} \frac{\partial u^{1cl}}{\partial y_j} = 0 \text{ for } y_3 = \pm 1 \tag{3.2}$$

$$k_{ij} \frac{\partial u^{1cl}}{\partial y_j} n_i = -k_{ij} \left( \frac{\partial u^0}{\partial x_j} + \frac{\partial u^1}{\partial x_j} \right) n_i, \text{ on } \Gamma^l \tag{3.3}$$

$$\lim_{y_2 \rightarrow +\infty} \nabla u^{1cl}(y_2, y_3) = 0 \tag{3.4}$$

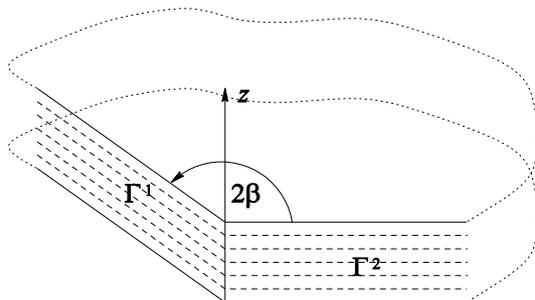


Figure 4. The perturbation of the edge.

$$\llbracket u^{1cl} \rrbracket = 0 \text{ across the interfaces} \tag{3.5}$$

$$\left\llbracket k_{ij} \frac{\partial u^{1cl}}{\partial y_j} n_i \right\rrbracket = 0 \text{ across the interfaces} \tag{3.6}$$

where  $S$  is defined in (2.11).

Close to the origin, a corrective term,  $v^*$  is added to  $u^1$  in the asymptotic expansion (2.7). It depends on the three space components. It is defined in an unbounded domain  $D$  which is the dilatation of the origin. As a matter of fact, close to the origin, all directions (the position in the thickness and the distance to the origin) have the same range of order. Because of the geometry of the domain, it will be useful to introduce the cylindric coordinates to describe the domain:

$$D \equiv \{r \in (0, +\infty), \theta \in (-\beta, \beta), z \in (-1, 1)\}.$$

The asymptotic expansion of the temperature is now

$$u^\varepsilon = u^0(0) + \varepsilon \left( \frac{\partial u^0}{\partial x_\alpha}(0) w^\alpha(z) \hat{u}^1(0) + v^*(r, \theta, z) \right) + \dots,$$

where the unknown is  $v^*$ .

When  $\theta = \pm\beta$ , the boundary condition (2.3) must be exactly satisfied at the corresponding order. When  $r$  becomes great, the corrective term must tend to the classical boundary layer term. We shall gather  $u^{1cl}$  and  $u^{1c2}$  into a unique function  $u^{1c}$  defined by

$$u^{1c} \equiv \begin{cases} u^{1cl} & \text{if } \theta > 0, \\ u^{1c2} & \text{if } \theta < 0. \end{cases}$$

**Remark 2.** For small values of  $\theta$  and great values of  $r$ , it means far from the lateral edge, the influence of each corrective term  $u^{1cl}$  is very small because of the exponentially decreasing. So that they can be neglected.

We can then see that, because  $D$  is unbounded, and because the corrective term must tend to  $u^{1c}$  when  $r$  becomes great, it cannot belong to  $L^2(D)$ . We shall transform the corrective term in order to obtain an unknown which belongs to  $L^2(D)$ . Let us define:

$$v^*(r, \theta, z) = u^{BL}(r, \theta, z) + \zeta(r) u^{1c}$$

where the new unknown is now  $u^{BL}$ .

The function  $\zeta$ , which is  $C^\infty(\mathbb{R}^+)$ , is a cut off function such that for little  $r$ ,  $\zeta$  is equal to 0 and for great value of  $r$ ,  $\zeta$  is equal to 1 (cf. **Figure 5**).

Insert figure 5 The cutoff function  $\zeta$

The problem for  $u^{BL}$  is now:

$$-\frac{\partial}{\partial y_i} \left( k_{ij} \frac{\partial u^{BL}}{\partial y_j} \right) = \frac{\partial}{\partial y_i} \left( k_{ij} \frac{\partial}{\partial y_j} (\zeta u^{1c}) \right) \text{ in } D \tag{3.7}$$

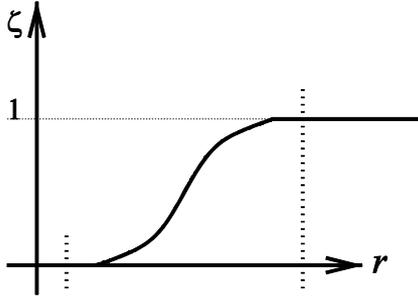


Figure 5. The cutoff function  $\zeta$ .

$$k_{3j} \frac{\partial u^{BL}}{\partial y_j} = -k_{3j} \frac{\partial}{\partial y_j} (\zeta u^{lc}) \text{ for } y_3 = \pm 1 \tag{3.8}$$

$$k_{ij} \frac{\partial u^{BL}}{\partial y_j} n_i = -k_{ij} \left( \frac{\partial u^0}{\partial x_j} + \frac{\partial u^1}{\partial y_j} + \frac{\partial}{\partial y_j} (\zeta u^{lc}) \right) n_i \text{ on } \Gamma^1 \text{ and } \Gamma^2 \tag{3.9}$$

$$\lim_{r \rightarrow +\infty} \lim_{r \rightarrow +\infty} u^{BL}(r, \theta, z) = 0, \tag{3.10}$$

$$u^{BL} = 0 \text{ across the interfaces,} \tag{3.11}$$

$$k_{ij} \frac{\partial u^{BL}}{\partial y_j} n_i = -k_{ij} \frac{\partial}{\partial y_j} (\zeta u^{lc}) n_i \text{ across the interfaces.} \tag{3.12}$$

Equation (3.7) is the equilibrium equation, (3.8) is the boundary condition on  $\Sigma_+$  and  $\Sigma_-$ , (3.11) and (3.12) are the continuity conditions across the interfaces, (3.9) is the boundary condition on the lateral edge, and (3.10) means that the corrective term is inefficient far from the origin.

**Remark 3.** When  $r$  is sufficiently great,  $\zeta(r)$  is equal to 1 and the right-hand sides of (3.7), (3.8), (3.9) and (3.12) vanish.

Problem (3.7)-(3.12) is equivalent to the following variational problem:

Find  $u \in V$  such that  $\forall w \in \dot{V} \equiv \{v \in \mathcal{D}(D) \setminus \mathbb{R}\}$

$$\int_D k_{ij} \frac{\partial u}{\partial y_j} \frac{\partial w}{\partial y_i} = L(w) \tag{3.13}$$

with

$$\begin{aligned} & -\int_{\Gamma^1} k_{ij} \left( \frac{\partial u^0}{\partial x_j} + \frac{\partial u^1}{\partial y_j} \right) n_i w ds \\ & -\int_{\Gamma^2} k_{ij} \left( \frac{\partial u^0}{\partial x_j} + \frac{\partial u^1}{\partial y_j} \right) n_i w ds \equiv \int_D \frac{\partial}{\partial y_i} \left( k_{ij} \frac{\partial}{\partial y_j} (\zeta u^{lc}) \right) w dy \\ & -\int_{\Gamma^1} k_{ij} \left( \frac{\partial u^0}{\partial x_j} + \frac{\partial u^1}{\partial y_j} + \frac{\partial}{\partial y_j} (\zeta u^{lc}) \right) n_i w ds \end{aligned}$$

$$\begin{aligned} & -\int_{\Gamma^2} k_{ij} \left( \frac{\partial u^0}{\partial x_j} + \frac{\partial u^1}{\partial y_j} + \frac{\partial}{\partial y_j} (\zeta u^{lc}) \right) n_i w ds \\ & -\int_{\Sigma_+} k_{ij} \frac{\partial}{\partial y_j} (\zeta u^{lc}) n_i w ds - \int_{\Sigma_-} k_{ij} \frac{\partial}{\partial y_j} (\zeta u^{lc}) n_i w ds \\ & -\int_{\text{interfaces}} k_{ij} \frac{\partial}{\partial y_j} (\zeta u^{lc}) n_i w ds \end{aligned}$$

where  $V$  is the completed space of  $\dot{V}$  for the norm associated with

$$(v, w)_V \equiv \int_D \nabla v \cdot \nabla w dy$$

**Lemma 1.** The right-hand side of (3.13) is a functional over  $\dot{V}$ .

**Proof.**  $L(\cdot)$  is defined over a space of equivalent classes. Two elements of a same class differ by a constant. It follows that  $L(\cdot)$  is a functional over  $\dot{V}$  if two elements of a same class take the same value by  $L(\cdot)$ , or if, for any constant  $C$ ,  $L(C) = 0$ . Using the first expression of  $L(\cdot)$  in (3.14), we get

$$\begin{aligned} L(C) &= -C \int_{\Gamma^1} k_{ij} \left( \frac{\partial u^0}{\partial x_j} + \frac{\partial u^1}{\partial y_j} \right) n_i ds - C \int_{\Gamma^2} k_{ij} \left( \frac{\partial u^0}{\partial x_j} + \frac{\partial u^1}{\partial y_j} \right) n_i ds \\ &= -C \int_{\gamma_1} \int_{-1}^1 k_{ij} \left( \frac{\partial u^0}{\partial x_j} + \frac{\partial u^1}{\partial y_j} \right) n_i dy_3 dl - \\ & C \int_{\gamma_2} \int_1^{-1} k_{ij} \left( \frac{\partial u^0}{\partial x_j} + \frac{\partial u^1}{\partial y_j} \right) n_i dy_3 dl \\ &= -C \int_{\gamma_1} \sigma_i n_i dl - C \int_{\gamma_2} \sigma_i n_i dl = 0 \end{aligned}$$

by virtue of (2.9) and the assumption on  $\varphi$ .

**Lemma 2.** The functional  $L(\cdot)$  is bounded over  $\dot{V}$ . It means that there exists a constant  $C$  such that for all  $w \in \dot{V}$ ,  $|L(w)| \leq C w_V$ .

**Proof.** Let  $w$  be any element of  $\dot{V}$ , using the second expression of  $L(\cdot)$  in (3.14)

$$\begin{aligned} L(w) &\equiv \int_D k_{ij} \frac{\partial}{\partial y_i} \left( \frac{\partial}{\partial y_j} (\zeta u^{lc}) \right) w dy \\ & -\int_{\Gamma^1} k_{ij} \left( \frac{\partial u^0}{\partial x_j} + \frac{\partial u^1}{\partial y_j} + \frac{\partial}{\partial y_j} (\zeta u^{lc}) \right) n_i w ds \\ & -\int_{\Gamma^2} k_{ij} \left( \frac{\partial u^0}{\partial x_j} + \frac{\partial u^1}{\partial y_j} + \frac{\partial}{\partial y_j} (\zeta u^{lc}) \right) n_i w ds \\ & -\int_{\Sigma_+} k_{ij} \frac{\partial}{\partial y_j} (\zeta u^{lc}) n_i w ds - \int_{\Sigma_-} k_{ij} \frac{\partial}{\partial y_j} (\zeta u^{lc}) n_i w ds \\ & -\int_{\text{interfaces}} k_{ij} \frac{\partial}{\partial y_j} (\zeta u^{lc}) n_i w ds \end{aligned}$$

By virtue of remark 3 each integral can be applied on a bounded domain which does not depend on  $w$ . As a consequence,  $L(w)$  can be read

$$\begin{aligned}
 L(w) \equiv & \int_{D^b} \frac{\partial}{\partial y_i} \left( k_{ij} \frac{\partial}{\partial y_j} (\zeta u^{1c}) \right) w dy \\
 & - \int_{\Gamma^{1b}} k_{ij} \left( \frac{\partial u^0}{\partial x_j} + \frac{\partial u^1}{\partial y_j} + \frac{\partial}{\partial y_j} (\zeta u^{1c}) \right) n_i w ds \\
 & - \int_{\Gamma^{2b}} k_{ij} \left( \frac{\partial u^0}{\partial x_j} + \frac{\partial u^1}{\partial y_j} + \frac{\partial}{\partial y_j} (\zeta u^{1c}) \right) n_i w ds \\
 & - \int_{\Sigma_+^b} k_{ij} \frac{\partial}{\partial y_j} (\zeta u^{1c}) n_i w ds - \int_{\Sigma_-^b} k_{ij} \frac{\partial}{\partial y_j} (\zeta u^{1c}) n_i w ds \\
 & - \int_{\text{interfaces}^b} k_{ij} \frac{\partial}{\partial y_j} (\zeta u^{1c}) n_i w ds
 \end{aligned}$$

where the upper-script  $b$  means that the domain is bounded. Using the Cauchy-Schwarz inequality,

$$\begin{aligned}
 |L(w)| < C & \left\{ w_{L^2(D^b)} + w_{L^2(\Gamma^{1b})} + w_{L^2(\Gamma^{2b})} \right. \\
 & \left. + w_{L^2(\Sigma_+^b)} + w_{L^2(\Sigma_-^b)} + w_{L^2(\text{interfaces}^b)} \right\}
 \end{aligned}$$

Using the trace theorem and because  $D^b$  is a bounded domain, we get

$$|L(w)| < C \left\{ \|w\|_{L^2(D^b)} + \|w\|_{H^1(D^b)} \right\}.$$

Passing to the quotient space  $\dot{V}$

$$|L(w)| < C \|\nabla w\|_{L^2(D^b)} \text{ but}$$

$$C \|\nabla w\|_{L^2(D^b)} \leq C \|\nabla w\|_{L^2(D)} \equiv \|w\|_V.$$

Because of the density of  $\dot{V}$  into  $V$ , Equation (3.13) is valid in the whole  $V$ . It follows from the Lax-Milgram theorem, lemma 2 that

**Theorem.** The corrective term  $u^{BL}$  is uniquely defined over  $V$ .

### 4. Conclusions

In order to improve the description of the behavior of the plate close to the singularity, a boundary layer term was added. This term is solution of (3.7)-(2.12). It has no influence far from the edge but it is defined over an unbounded domain.

At first, the equivalent variational problem was found. Then, the previous theorem allows us to prove the existence and the uniqueness of the solution. In this way the numerical resolution can be implement.

### 5. References

- [1] H. Dumontet, "Homogénéisation et Effets de Bords dans les Matériaux Composites," Ph.D. Thesis, Paris, 1990.
- [2] I. Titeux, "Problèmes de Fracture et Comportement Local Pour les Plaques Composites Anisotropes," Ph.D. Thesis, Paris, 1995.
- [3] A. R. Saidi, F. Hejripour and E. Jomehzadeh, "On the Stress Singularities and Boundary Layer in Moderately Thick Functionally Graded Sectorial Plates," *Applied Mathematical Modelling*, Vol. 34, No. 11, 2010, pp 3478-3492. [doi:10.1016/j.apm.2010.02.036](https://doi.org/10.1016/j.apm.2010.02.036)
- [4] E. Jomehzadeh and A. R. Saidi, "Analytical Solution for Free Vibration of Transversely Isotropic Sector Plates Using a Boundary Layer Function," *Thin Walled Structures*, Vol. 47, No. 1, 2009, pp. 82-88. [doi:10.1016/j.tws.2008.05.004](https://doi.org/10.1016/j.tws.2008.05.004)
- [5] J. Sanchez-Hubert and E. Sanchez-Palencia, "Introduction Aux Methods Asymptotiques et à L'homo-généisation," Masson, Paris, 1992.
- [6] D. Leguillon and E. Sanchez-Palencia, "Computation of Singular Solutions in Elliptic Problems and Elasticity," Masson, Paris, 1988.
- [7] I. Titeux and Y. Yakubov, "Completeness of Root Functions for Thermal Conduction in a Strip with Piecewise Continuous Coefficients," *Mathematical Models and Methods in Applied Sciences*, Vol. 7, No. 7, 1997, pp. 1035-1050.