

# The Origin of the Giant Hall Effect in Metal-Insulator Composites\*

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## Abstract

Near the metal-insulator transition, the Hall coefficient  $R$  of metal-insulator composites (M-I composite) can be up to  $10^4$  times larger than that in the pure metal called *Giant Hall effect*. Applying the physical model for alloys with phase separation developed in [1] [2], we conclude that the *Giant Hall effect* is caused by an electron transfer away from the metallic phase to the insulating phase occupying *surface states*. These *surface states* are the reason for the *granular* structure typical for M-I composites. This electron transfer can be described by  $-dn = \beta \cdot n \cdot d \left( \frac{\nu_B}{\nu_A} \right)$

[1] [2], provided that long-range diffusion does not happen during film production ( $n$  is the electron density in the phase A.  $\nu_A$  and  $\nu_B$  are the volume fractions of the phase A (metallic phase) and phase B (insulator phase).  $\beta$  is a measure for the average potential difference between the phases A and B). A formula for calculation of  $R$  of composites is derived and applied to experimental data of granular  $\text{Cu}_{1-y}(\text{SiO}_2)_y$  and  $\text{Ni}_{1-y}(\text{SiO}_2)_y$  films.

## Keywords

Metal-Insulator Composites, Granular Metals, Hall Coefficient, Conductivity, Electron Density

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## 1. Introduction

Nanocomposites play a growing role in both scientific research and practical applications because of the possibility of combination of special properties which cannot be reached in classical materials [3]-[5]. A prominent example for both scientific challenge and practical application is the *Giant Hall effect* (GHE) in metal-insulator

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composites (M-I composites): Near the metal-insulator transition (M-I transition), the Hall coefficient can be up to  $10^4$  times larger than that in the pure metal [6]-[16].

Applications of the GHE we find in magnetic field sensing elements, in read heads of magnetic recording devices and magnetic switching devices. Other examples for practical applications of nanocomposites are biomedical ones, materials with improved corrosion resistance, and thermoelectric materials with higher efficiency for energy harvesting, environmentally friendly refrigeration, direct energy transformation from heat into electricity, and temperature sensors.

As reasons for the GHE, quantum size effects and quantum interference effects on the mesoscopic scale have been discussed [8] [11]-[14] [17]. To our knowledge, until now, there is no explanatory model which can interpret the phenomenon of GHE. In the present paper, we present a discussion of the reasons for the GHE applying the electron transfer model [1] [2] developed for metal-metalloid alloys. This model can be summarized by three points<sup>1</sup>:

For large ranges of concentration there is

(1) *Phase separation* between two phases called phase *A* and phase *B*, where each phase has its “own” short-range order (SRO),

(2) The *phase separation* leads to *band separation* in the conduction band (CB) and valence band (VB) connected with the phases *A* and *B*, respectively, and the electrons are freely propagating and the corresponding *wave functions are extended* over connected regions of one phase as long as the phase forms an infinite (macroscopic) cluster through the alloy.

(3) Between the two coexisting phases there is *electron redistribution (electron transfer)* which can be described by

$$n(\zeta) = n_A \cdot \exp(-\beta\zeta), \quad (1)$$

where  $\zeta$  is the quotient of the volume or atomic fractions<sup>2</sup> of the two coexisting phases.  $n(\zeta)$  is the electron density in the phase *A* with  $n_A = n(0)$ .  $\beta$  is a constant for a given alloy, which is determined by the average potential difference between the two phases.

The *points* (1) and (2) imply the fact that each phase can be characterized by its own transport coefficients which can be calculated, in principle, by classical transport theory as done in [2] (conductivity) and [18] [19] (Seebeck coefficient).

Since M-I composites also consist of two separate phases with phase grains at the nanoscale, it is obvious to ask whether Equation (1) is reflected in the concentration dependence of the Hall coefficient  $R$  of M-I composites as well. Indeed, we have found that in the metallic regime of  $\text{Cu}_{1-y}(\text{SiO}_2)_y$  and  $\text{Ni}_{1-y}(\text{SiO}_2)_y$  thin films, the concentration dependence of  $R$  can be approximated by linear relations

$$d \ln |R| = \alpha' \cdot d\eta \quad (2)$$

with constant slope  $\alpha'$ . For  $\text{Cu}_{1-y}(\text{SiO}_2)_y$  and  $\text{Ni}_{1-y}(\text{SiO}_2)_y$  it follows from **Figure 1(a)** and **Figure 1(b)**,  $\alpha' = 7.9$  and  $\alpha' = 10.3$  with the coefficient of determination  $r^2 = 0.92$  and  $r^2 = 0.96$ , respectively.  $\eta = y/(1-y)$ , where  $y$  is the volume fraction of  $\text{SiO}_2$ . This finding is illustrated in **Figure 1(a)** and **Figure 1(b)**, where the absolute  $R$  values measured by Zhang *et al.* [12], Saviddes *et al.* [20] and Pakhomov *et al.* [10] are drawn versus  $\eta$ . The signs of the  $R$  values are negative. For  $\text{Ni}_{1-y}(\text{SiO}_2)_y$ , **Figure 1(b)**, the extraordinary  $R$  values (taken from Fig. 3 in [10]) are drawn.

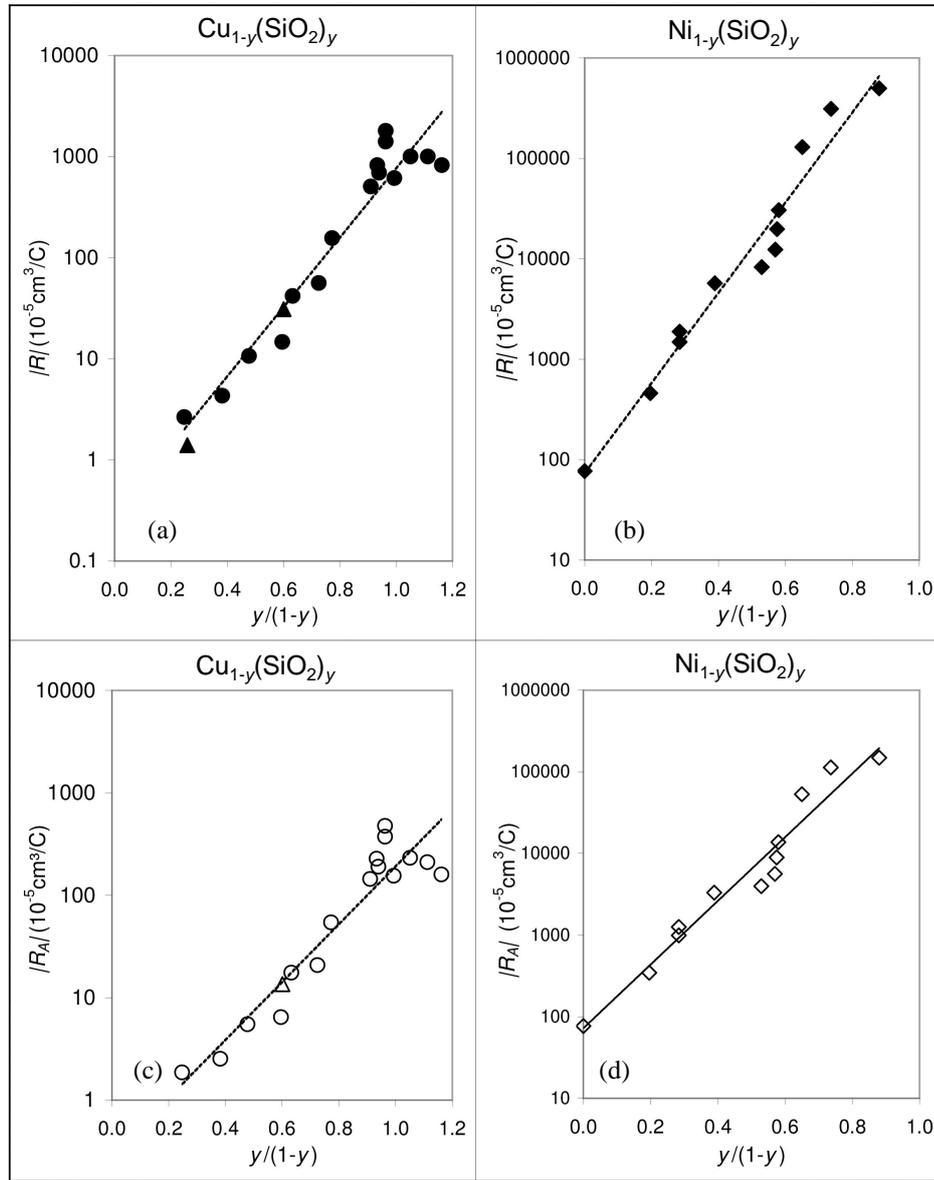
**Figure 1(a)** and **Figure 1(b)** reflect immediately Equation (1) provided that  $|R| \propto 1/n$  (nearly free electrons - NFE). For a more precise discussion, we have to separate the contribution of the metallic phase to  $R$ , which can be done applying effective medium theory (EMT, [2], Sec. IVA therein).

The known EMT-formula for the Hall coefficient derived by Cohen and Jortner [21] is

$$\sum_{i=A,B} \nu_i \cdot \frac{\sigma_i^2 R_i - \sigma^2 R}{(\sigma_i + 2\sigma)^2} = 0, \quad (3)$$

<sup>1</sup>The points (1) and (2) are now confirmed experimentally or supported by independent authors [39]-[50] (details in [2], Sec. I therein). Support for point (3) comes from the fact that it is successfully applied for a quantitative description of the concentration dependence of both conductivity and Seebeck coefficient in [18] [19] and of the M-I transition and structural features of metal-metalloid alloys and M-I composites in [2].

<sup>2</sup>In [1], the available experimental data were not sufficient to decide this question. This question was discussed in [2] with the result that  $\zeta$  is to be interpreted as volume quotient.



**Figure 1.** Experimental Hall coefficient data at 5 K versus  $y/(1-y)$  for  $\text{Cu}_{1-y}(\text{SiO}_2)_y$ , (a), (c), and  $\text{Ni}_{1-y}(\text{SiO}_2)_y$ , (b), (d), taken from [12] (circles), [20] (triangles) and [10] (diamonds). (c), (d):  $R_A$  calculated by  $R_A = R \frac{(3\nu_A - 1)}{2}$  according to Equation (16), where  $\nu_A = 1 - y$  is set.

where  $\sigma$  and  $R$  are the electrical conductivity and Hall coefficient of a composite, respectively.  $\sigma_i$  and  $R_i$  are the corresponding transport parameters of the phase  $i$ .<sup>3</sup>  $\nu_i$  is the volume fraction of the phase  $i$  ( $i$  stands for the phase A or B).

As will be argued in Sec. 3.1, Equation (3) seems to be a good approximation for two-phase composites if  $\sigma_A \approx \sigma_B$ , but not if  $\sigma_A \gg \sigma_B$ , as typical for M-I composites. Therefore, in Sec. 2 a  $R$  formula will be derived which holds for  $\sigma_A \gg \sigma_B$  as well. In Sec. 3.1 this  $R$  formula and Equation (3) will be compared and its applicability to M-I composites will be checked. In Sec. 3.2 it will be applied to a quantitative discussion of the GHE in M-I composites. In Sec. 3.3 the effect of the grain size on the GHE will be discussed. In Sec. 4 the results will be summarized.

<sup>3</sup>Equation (3) is a comprehensive formulation of the Equations (16)-(20) of [21].

## 2. Derivation of the $R$ Formula

Let us consider a non-magnetic two-phase composite, where the phase grains are spherical without preferred orientations and arranged in a symmetrical fashion and each phase  $i$  can be characterized by a set of transport coefficients. The *local* electric current density in a single grain of the phase  $i$  ( $i = A$  or  $B$ ) can be written as

$$\mathbf{J}_i = \overset{\leftrightarrow}{\sigma}_i \mathbf{E}_i, \quad (4)$$

where  $\mathbf{E}_i$  and  $\overset{\leftrightarrow}{\sigma}_i$  are the electric field and the magnetoconductivity tensor [22] in this grain. For the electric current density outside of this grain we write analogously

$$\mathbf{J} = \overset{\leftrightarrow}{\sigma} \mathbf{E}, \quad (5)$$

where  $\mathbf{E}$  and  $\overset{\leftrightarrow}{\sigma}$  are the electric field and the magnetoconductivity tensor outside of this grain (effective medium). For the determination of the coefficients in  $\overset{\leftrightarrow}{\sigma}_i$  we start with the equation for  $\mathbf{J}_i$  under the influence of an electrical and magnetic field, [23]-[25]

$$\mathbf{J}_i = e_i^2 K_{11,i} \mathbf{E}_i + \frac{e_i^3}{m_i} K_{12,i} (\mathbf{E}_i \times \mathbf{B}) + \frac{e_i^4}{m_i^2} K_{13,i} \mathbf{B} (\mathbf{E}_i \cdot \mathbf{B}). \quad (6)$$

$K_{rs,i}$  are the transport integrals,  $e_i = -|e|$  and  $+|e|$  for electrons and holes, respectively.  $|e|$  is the elementary charge. The third summand in Equation (6) disappears only if  $\mathbf{E}$  (or  $\mathbf{E}_i$ ) is always perpendicular to  $\mathbf{B}$ . In a composite, however,  $\mathbf{B}$  and  $\mathbf{E}$  (or  $\mathbf{E}_i$ ), are generally not perpendicular to each other because of the spherical boundary between a phase grain and its surroundings. Without loss of generality, the external fields applied to the sample,  $\mathbf{E}_{ext}$  and  $\mathbf{B}$ , have the directions of the  $X$  and  $Z$  axes, respectively. Then Equation (6) and Equation (4) lead to

$$\overset{\leftrightarrow}{\sigma}_i = \frac{\sigma_i}{1 + \xi_i^2} \begin{pmatrix} 1 & \xi_i & 0 \\ -\xi_i & 1 & 0 \\ 0 & 0 & 1 + \nu_i \xi_i^2 \end{pmatrix}, \quad (7)$$

where  $\xi_i \equiv \mu_i B = \sigma_i R_i B$ . Analogously we write for  $\overset{\leftrightarrow}{\sigma}$ ,

$$\overset{\leftrightarrow}{\sigma} = \frac{\sigma}{1 + \xi^2} \begin{pmatrix} 1 & \xi & 0 \\ -\xi & 1 & 0 \\ 0 & 0 & 1 + \nu \xi^2 \end{pmatrix} \quad (8)$$

with  $\xi \equiv \mu B = \sigma R B$ .  $\nu_i = 1 + \cos \gamma_i$  and  $\nu = 1 + \cos \gamma$ , where  $\gamma_i$  and  $\gamma$  are the angle between  $\mathbf{E}_i$  and  $\mathbf{B}$ , respectively between  $\mathbf{E}$  and  $\mathbf{B}$ .  $\mu$  and  $\mu_i$  are the Hall mobility in the composite and phase  $i$ , respectively.

At the interface between a single phase grain and its surroundings continuity of the normal components of the current density and the tangential components of the potential gradient are to be fulfilled. For the limiting case  $\mathbf{B} = 0$ , this demand is fulfilled by

$$f(\sigma, \sigma_i) \equiv \sigma_A \sigma_B + \sigma \sigma_A (3\nu_A - 1) + \sigma \sigma_B (3\nu_B - 1) - 2\sigma^2 = 0 \quad (9)$$

following from the EMT-formula for  $\sigma$ , [27] [28]

$$\sum_i \nu_i \frac{\sigma_i - \sigma}{\sigma_i + 2\sigma} = 0. \quad (10)$$

For the case  $\mathbf{B} \neq 0$ , the tensor properties of  $\overset{\leftrightarrow}{\sigma}_i$  and  $\overset{\leftrightarrow}{\sigma}$ , Equation (7) and Equation (8), are to be taken into account. Equation (9) expressed in tensor form reads

$$\overset{\leftrightarrow}{\sigma}_A \overset{\leftrightarrow}{\sigma}_B + \overset{\leftrightarrow}{\sigma} \overset{\leftrightarrow}{\sigma}_A (3\nu_A - 1) + \overset{\leftrightarrow}{\sigma} \overset{\leftrightarrow}{\sigma}_B (3\nu_B - 1) - 2 \overset{\leftrightarrow}{\sigma} \overset{\leftrightarrow}{\sigma} = 0, \quad (11)$$

where the identities  $\overset{\leftrightarrow}{\sigma}_A \overset{\leftrightarrow}{\sigma}_B = \overset{\leftrightarrow}{\sigma}_B \overset{\leftrightarrow}{\sigma}_A$  and  $\overset{\leftrightarrow}{\sigma} \overset{\leftrightarrow}{\sigma}_i = \overset{\leftrightarrow}{\sigma}_i \overset{\leftrightarrow}{\sigma}$  have been used. Equation (11) determines the coeffi-

icients of Equation (8) as a function of the coefficients of Equation (7). Inserting Equation (7) and Equation (8) into Equation (11) and comparing coefficients for the tensor elements, we get

$$\xi = \frac{\sigma_A \sigma_B (\xi_A + \xi_B) + \sigma \sigma_A \xi_A (3\nu_A - 1) + \sigma \sigma_B \xi_B (3\nu_B - 1)}{4\sigma^2 - \sigma \sigma_A (3\nu_A - 1) - \sigma \sigma_B (3\nu_B - 1)}, \quad (12)$$

following from the tensor elements  $\sigma_{xy}$  or  $\sigma_{yx}$ , where quadratic and higher powers of  $\xi$ ,  $\xi_i$  are neglected, *i.e.*, Equation (12) and the following Equations (13), (14) are low-field approximations. Within this approximation the parameters  $\nu_i$  and  $\nu$  do not have an influence on the result. From the tensor elements  $\sigma_{xx}$ ,  $\sigma_{yy}$ , or  $\sigma_{zz}$ , Equation (10) follows.

Substituting  $\xi$  and  $\xi_i$  in Equation (12) by  $R$  and  $R_i$  and considering Equation (9) we get the  $R$  formula for two-phase composites:

$$R = \frac{\sigma_A^2 R_A [\sigma_B + \sigma(3\nu_A - 1)] + \sigma_B^2 R_B [\sigma_A + \sigma(3\nu_B - 1)]}{\sigma(\sigma_A \sigma_B + 2\sigma^2)}. \quad (13)$$

The same formalism can also be applied to composites with more than two phases leading to relatively complex formulae for  $R$ . A self-contained and more manageable description of these  $R$  formulae is given by

$$\left( R\sigma^2 \frac{\partial}{\partial \sigma} + \sum_{i=A,B,\dots} R_i \sigma_i^2 \frac{\partial}{\partial \sigma_i} \right) f(\sigma, \sigma_i) = 0 \quad (14)$$

with

$$f(\sigma, \sigma_i) = \left( \prod_{i=A,B,\dots} (\sigma_i + 2\sigma) \right) \left( \sum_{i=A,B,\dots} \nu_i \frac{\sigma_i - \sigma}{\sigma_i + 2\sigma} \right). \quad (15)$$

### 3. Discussion

#### 3.1. Comparison between Equation (3) and Equation (13)

For three examples of two-phase composites, in **Figure 2(b)**, **Figure 2(d)**, and **Figure 2(f)**, the concentration dependence of  $R$  related to its values at  $\nu_A = 1$  is shown, calculated by Equation (13), and compared with Equation (3), denoted as ‘‘C & J’’. In **Figure 2(a)**, **Figure 2(c)**, and **Figure 2(e)**, the corresponding concentration dependence of the Hall mobility  $\mu$  ( $= \sigma R$ ) is shown, where  $\sigma$  is calculated by Equation (9). There are two essential differences between the two solutions Equation (3) and Equation (13):

(1) The most striking difference appears in **Figure 2(a)** and **Figure 2(c)**: The ‘‘C & J’’ curves decrease dramatically with increasing  $\nu_A$  and pass through a pronounced minimum at  $\nu_A = 1/3$ , although  $\mu_A = \mu_B$  and  $\mu_A > \mu_B$ , respectively. In contrast, the  $\mu$  curves calculated by Equation (13) agree with the expectation: **Figure 2(a)**:  $\mu$  agrees with  $\mu_A$  for all  $\nu_A$ ; **Figure 2(c)** and **Figure 2(e)**:  $\mu$  increases and decreases with increasing  $\nu_A$ , respectively.

A possible interpretation for such dramatic decrease of  $\mu$  at  $\nu_A = 1/3$  (‘‘C & J’’ curves) could be additional scattering centres in the added phase boundaries. Such an effect by the phase boundaries is expected to be the more pronounced the smaller the sizes of the phase grains,  $D_i$ . However, the C & J formula [21] [26] does not contain  $D_i$ .

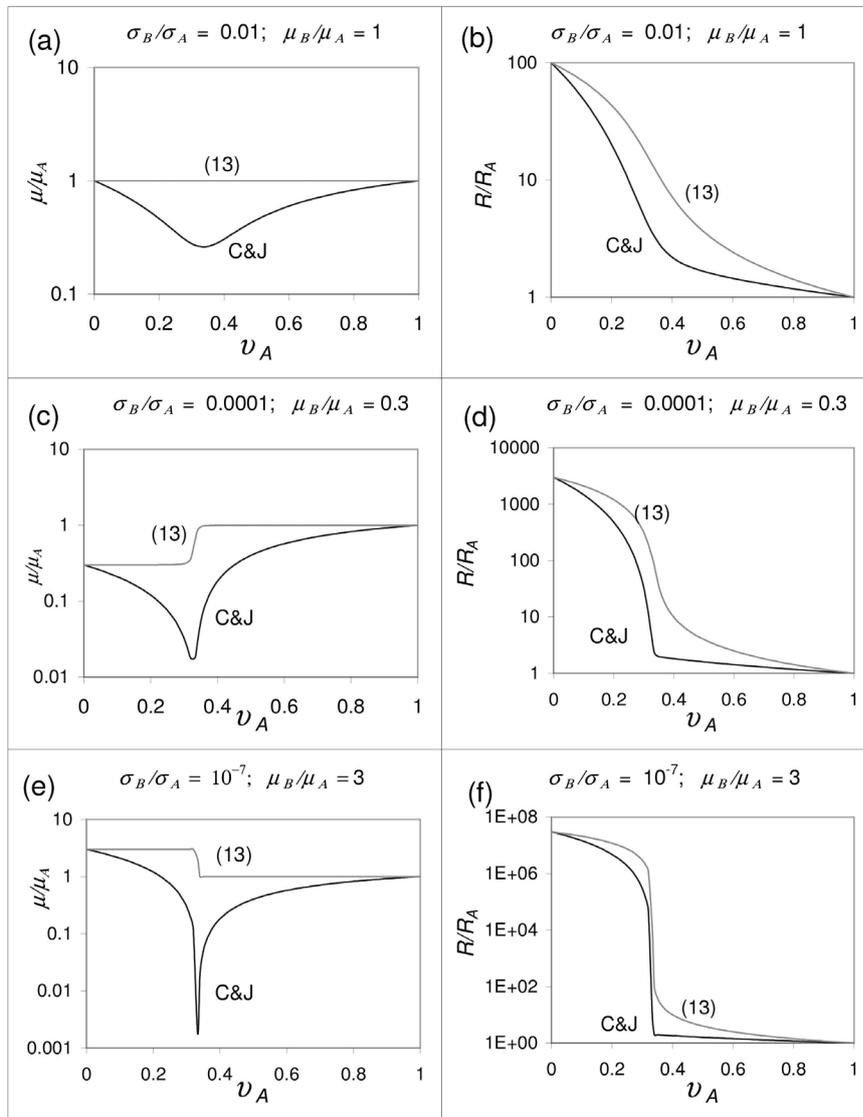
The differences between Equation (13) and the curves ‘‘C & J’’ are the larger the larger the difference between  $\sigma_A$  and  $\sigma_B$ . On the other hand, for the limiting case,  $\sigma_A = \sigma_B$ , Equation (3) and Equation (13) agree.

(2) Another striking difference between Equation (13) and Equation (3) is represented by the boundary case ‘‘ $\sigma_B = 0$  and  $\sigma_A \neq 0$ ’’, for which one obtains

$$\frac{1}{R^{(13)}} = \frac{1}{R_A} \frac{(3\nu_A - 1)}{2}, \quad (16)$$

and

$$\frac{1}{R^{C\&J}} = \frac{1}{R_A} \frac{(3\nu_A + 1)}{4}, \quad (17)$$



**Figure 2.**  $\mu/\mu_A$  and  $R/R_A$  versus  $\nu_A$  calculated by Equation (3) (“C & J”) and by Equation (13). The “C & J”-curves in **Figure 2(a)** and **Figure 2(c)** agree with the curves “5” and “7” shown in Fig. 1(b), Fig. 1 (c) of [21] and Fig. 13, Fig. 14 of [26], where the same examples are chosen.

respectively, and for  $\sigma$ , Equation (9) gives

$$\sigma = \sigma_A \frac{(3\nu_A - 1)}{2}. \quad (18)$$

Starting at  $\nu_A = 1$ , with decreasing  $\nu_A$  both  $\sigma$  and  $\frac{1}{R^{(13)}}$  decrease continuously until they vanish at  $\nu_A = 1/3$ . This result corresponds to the fact that for  $\nu_A < 1/3$  there is no longer a connected metal cluster through the composite (in correspondence with the assumption made earlier that the phase grains are spherical without preferred orientations and arranged in a symmetrical fashion). This result is, however, not reflected by Equation (17) which gives  $\frac{1}{R^{C\&J}} > 0$  even for  $\nu_A < 1/3$ , where all the metallic granules are separated by adjacent insulating phase regions, that is, electron transport through the sample does not happen, if additional

tunneling is excluded.

These two differences, (1) and (2), suggest the fact that Equation (16) represents the physical situation better than Equation (17). Therefore, in the following, Equation (13), respectively Equation (16), will be applied in a discussion of the Hall coefficient in M-I composites.

### 3.2. The Giant Hall Effect in M-I Composites

For  $R_A$  calculated by Equation (16) applied to the  $R$  data of **Figure 1(a)**, **Figure 1(b)**, we find that they can be approximated by a relation similar to Equation (2),

$$d \ln |R_A| = \beta' \cdot d\eta, \quad (19)$$

where  $\beta'$  is a constant for a given M-I composite: For  $\text{Cu}_{1-y}(\text{SiO}_2)_y$  and  $\text{Ni}_{1-y}(\text{SiO}_2)_y$  it follows from **Figure 1(c)** and **Figure 1(d)**,  $\beta' = 6.5$  and  $\beta' = 9.0$  with the coefficient of determination  $r^2 = 0.89$  and  $r^2 = 0.95$ , respectively.<sup>4</sup> This finding suggests that the colossal increase of  $|R|$  is caused by *one* (!) effect acting in the *complete* metallic regime. Inserting  $|R_A| \propto 1/n$  (NFE approximation) in Equation (19) leads to Equation (1), or in differential form,

$$-dn = \beta \cdot n \cdot d\zeta, \quad (20)$$

where  $\beta \approx \beta'$ .  $n$  is the electron density in the metallic phase and  $\zeta = \nu_B/\nu_A \cdot \nu_B$  and  $\nu_A$  are the volume fractions of the insulator phase ( $B$ ) and metallic phase ( $A$ ), respectively.  $\nu_B$  and  $\nu_A$  are identical with  $y$  and  $1 - y$ , respectively, if the insulating phase consists only of  $\text{SiO}_2$  and the metallic phase only of  $\text{Cu}$  or  $\text{Ni}$ . In this case,  $\beta = \beta'$ . If, however, a certain portion of the metalloid atoms is dissolved in the metallic phase and/or a certain portion of the metal atoms is solved in the insulating phase, then  $\beta'$  is only an approximation for  $\beta$ . Equations (1) and (20) agree with the equations (15a) and (15b) in [1], respectively, which describe electron transfer between the phases in amorphous transition-metal—metalloid alloys.<sup>5</sup> There the parameter  $\beta$  was interpreted to be a constant for a given composite, which is determined by the average potential difference between the phases,  $\Delta V$ .<sup>6</sup> Phase  $B$  is the phase with the deeper potential. Because of this analogy, Equation (19) suggests the following interpretation of the GHE: The colossal increase of  $|R|$  with decreasing metal content is essentially caused by a decrease of  $n$  due to electron transfer to the insulator phase ( $\text{SiO}_2$ ) which can be described by Equation (1), respectively Equation (20).

Because the Fermi level lies in the energy gap between the valence band and conduction band of the insulator  $\text{SiO}_2$  phase, the transferred electrons occupy surface states on the  $\text{SiO}_2$  phase. This is the reason for the *granular* structure: spherical metal grains are embedded in the amorphous  $\text{SiO}_2$  phase (see, e.g., [29], Figs. 13-16 therein). A minimum energy is realized if, *firstly*, the transferred (pinned) electrons are arranged on *spherical* surfaces and, *secondly*, the insulating phase forms very thin layers around the metal grains providing the largest possible surface to accommodate the large number of transferred electrons. This electron transfer from the metallic phase to the phase boundaries provides the logical explanation for the *granular* structure in M-I composites. Such a granular structure has been found in many M-I films [7] [13] [15] [29]. This proposal applies to magnetic M-I composites as well. For *nonmagnetic* M-I composites the parameter  $C$  in

$$R_A = -\frac{C}{|e| \cdot n} = \frac{\mu_A}{\sigma_A} \quad (21)$$

(NFE approximation) is of the order of *one*, depending slightly on the magnetic field. [23] [24]  $\sigma_A$  and  $\mu_A$  are the conductivity and Hall mobility, respectively, of the phase  $A$ .  $|e|$  is the elementary charge. For *magnetic* M-I composites Equation (21) holds approximately if “=” is replaced by “ $\propto$ ” considering the effect of the additional *internal* magnetic field due to the magnetization: An electron sees the effective magnet field  $H_w = H + H_i$ , where  $H_i \gg H$ .  $H$  is the external field applied to the specimen and  $H_i$  is the internal field produced by the quantum mechanical exchange forces ([30], p. 341). An electron does not distinguish between  $H$  and  $H_i$ . It moves according to the Lorentz force determined by  $H_w$  and the electrical field  $E$ . One can as-

<sup>4</sup> $R_A$  calculated by Equation (17) can also be approximated by Equation (19) with the slopes  $\beta' = 7.5$  and  $\beta' = 9.9$  and  $r^2 = 0.92$  and  $r^2 = 0.96$ , for  $\text{Cu}_{1-y}(\text{SiO}_2)_y$  and  $\text{Ni}_{1-y}(\text{SiO}_2)_y$ , respectively.

<sup>5</sup>For large ranges of composition, amorphous transition-metal—metalloid alloys are composed of different amorphous phases [39]-[43] with  $D_i \sim 1 - 2 \text{ nm}$  [42] [43].

<sup>6</sup>The potential difference  $\Delta V$  is identical with the difference of the electrochemical potentials of the phases, as long as they are not in contact to each other. Only, when a contact is realized, a common electrochemical potential is realized by electron transfer between the phases.

sume that  $H_w$  is nearly proportional to  $H$  as long as  $H_i$  is nearly proportional to the magnetization produced by  $H$ .

This assumption is supported by the experimental finding by Xiong *et al.* [31] that (for not too small fields  $H$ ), in the granular Co-Ag system, the Hall resistivity  $\rho_{xy}$  is linearly proportional to  $H$ . If so, the measured  $R$  values differ from the calculated  $R$  values, Equation (21), only by a factor which is nearly constant. Therefore, we assume that the EMT-formula for  $R$ , Equation (13), can be applied to magnetic composites as well.

If the metallic phase of a M-I composite is a *noble metal*, the NFE approximation is a good one for the metallic phase, above all as the Fermi surface moves away from the Brillouin zone boundary as  $n$  decreases. For the metallic phase in Ni-SiO<sub>2</sub> the NFE approximation is surely also a good one, because Ni has only 0.55 4s valence electrons per Ni atom ([30], p. 271).

If the metallic phase of a M-I composite is a *transition-metal*, the electron transfer is expected to be composed of both the  $d$  and  $s$  electrons. As the  $d$  density of states at the Fermi level is essentially larger than the  $s$  density of states, the principal share of electrons transferred to the insulating phase, is made up of  $d$  electrons, that is, the  $s$  electron density in the metallic phase remains relatively large. Because the electronic transport is determined by the  $s$  valence electrons in the  $A$  phase, the effect of the electron transfer on the electronic transport in the metallic phase is expected to be relatively small, and the increase of  $R_A$  due to electron transfer should be essentially smaller as in M-I composites containing a noble metal as metallic phase. For instance, in Mo<sub>1-y</sub>(SnO<sub>2</sub>)<sub>y</sub> ([7], Fig. 2 therein), we do not find an exponential change of  $R_A$  with increasing  $y/(1-y)$ : for  $0 < y < 0.55$  (*i.e.*  $0 < y/(1-y) < 1.22$ ), the experimental  $R$  values [7] of Mo-SnO<sub>2</sub> fluctuate slightly where the average of  $R_A$  calculated by Equation (16) remains nearly independent of  $y$ . Only approaching the M-I transition ( $y > 0.6$ ),  $R_A$  increases drastically.<sup>7</sup>

Now the question arises: why do we find an exponential dependence of  $n(\zeta)$  in Ni<sub>1-y</sub>(SiO<sub>2</sub>)<sub>y</sub> although Ni is a transition-metal? X-ray emission spectra of amorphous and crystalline Ni<sub>1-y</sub>Si<sub>y</sub> and Pd<sub>1-y</sub>Si<sub>y</sub> alloys by Tanaka *et al.* [32] have shown that there are strong bonds between  $d$  orbitals (of Ni and Pd) and Si  $p$  orbitals leading to a stronger splitting of the  $d$  band into a bonding and antibonding fraction, where the former is lifted, whereas the latter lies below the Fermi level. Analogously, for Ni<sub>1-y</sub>(SiO<sub>2</sub>)<sub>y</sub> one can also expect strong bonds between Ni  $d$  orbitals and Si (and O)  $p$  orbitals which leads to a strong reduction or disappearance of the  $d$  density of states at the Fermi level. Therefore, we find an experimental increase of  $|R_A|$  (Figure 1(d)). Moreover, there is strong evidence for the assumption that the metallic phase does not consist of Ni alone, but that there is a certain fraction of Si (and O atoms) dissolved in the metallic phase.

In summary, for M-I composites containing a *noble metal*, we expect an exponential  $n(\zeta)$  dependence because the electron transfer is made up entirely of the  $s$  electron density. For M-I composites containing a *transition-metal*, an exponential  $n(\zeta)$  dependence can be expected if the  $d$  density of states at the Fermi level is strongly reduced, for instance caused by a hybridization of the  $d$  states with the  $p$  states of the metalloid.

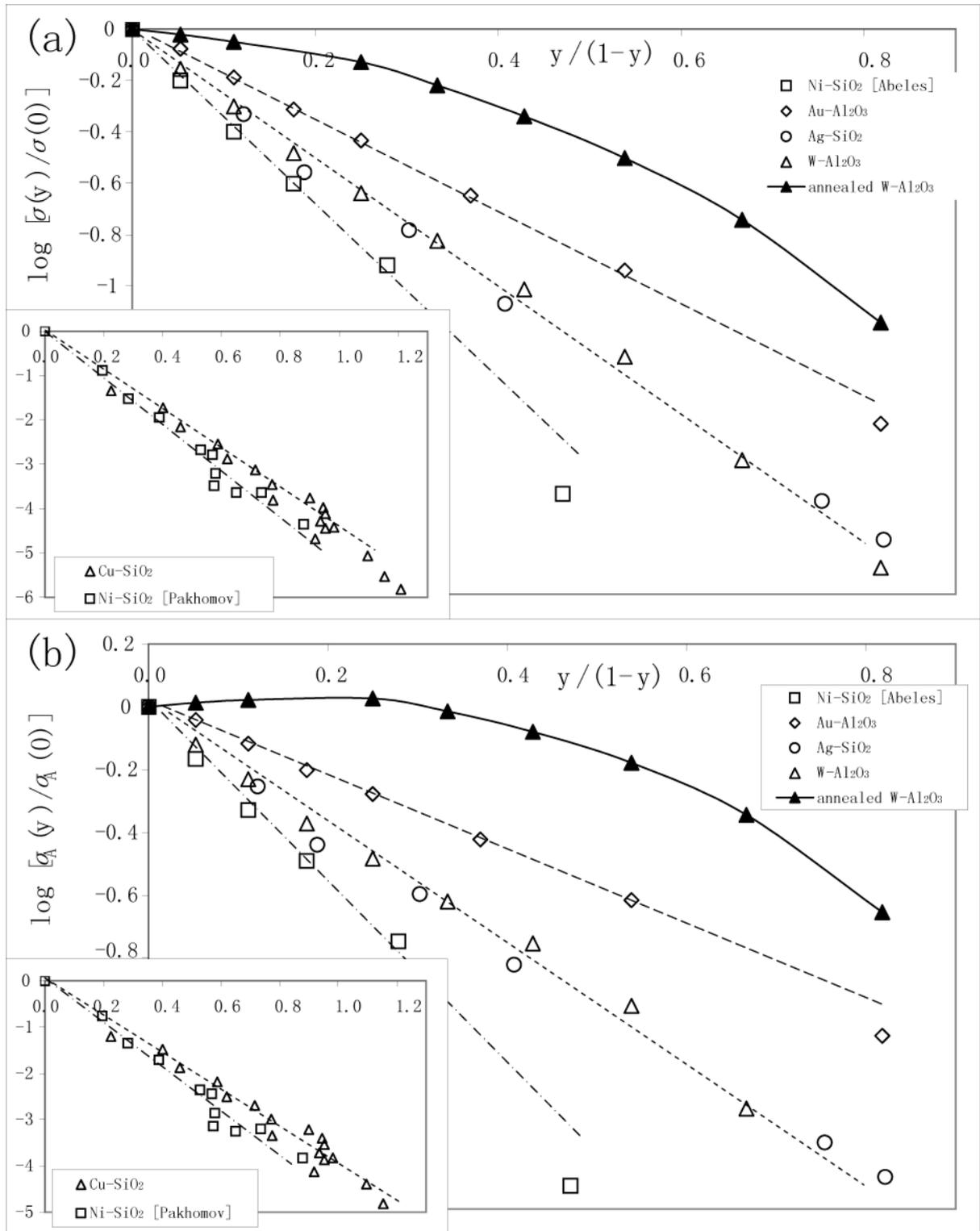
Comparing granular M-I composites with amorphous transition-metal—metalloid alloys ([11]), we state that the exponential increase of  $R$  and the exponential decrease of  $\sigma$  with  $y$  (respectively  $y/(1-y)$ ) is essentially caused by the same phenomenon: decrease of the electron density in the metallic phase due to electron transfer to the metalloid or insulator phase. The essential difference between these two material classes is the fact that in the metalloid phase of the amorphous transition-metal—metalloid alloys an *incompletely occupied*  $sp$  band can exist ([2], Sec. IIA therein) for accepting the transferred electrons. In contrast, in the insulator phase of M-I composites only localized states on the surface of it are available for acceptance of the transferred electrons. This difference is also the reason for the different microscopic structures of M-I composites and amorphous transition-metal—metalloid alloys. Another, rather quantitative difference is the fact that the decrease of  $n$  is essentially larger than in amorphous transition-metal—metalloid alloys, as the average potential difference between the phases,  $\Delta V$ , is essentially larger.

Our *electron transfer* model is compatible with a series of other experimental findings:

1) The GHE occurs both in magnetic M-I composites and non-magnetic ones suggesting a mechanism independent from magnetism [13].

2) In M-I composites,  $\sigma$  and  $\sigma_A$  decrease exponentially with decreasing metal content in correspondence with the exponential increase of  $R$ . For some M-I composites, in Figure 3,  $\log[\sigma(y)/\sigma(0)]$  and  $\log[\sigma_A(y)/\sigma_A(0)]$  are drawn versus  $y/(1-y)$ . In the NFE approximation the connection between  $\sigma_A$  and  $n$  is given by

<sup>7</sup>In Mo<sub>1-y</sub>(SnO<sub>2</sub>)<sub>y</sub>, the carriers are holes [7]; electron transfer away from the metallic phase can lead to an increase of the hole density  $p$ , but also to a decrease of it depending on the position of the Fermi surface in relation to the Brillouin zones.



**Figure 3.** (a)  $\log[\sigma(y)/\sigma(0)]$  versus  $y/(1-y)$  for  $\text{Ni}_{1-y}(\text{SiO}_2)_y$ ,  $\text{Au}_{1-y}(\text{Al}_2\text{O}_3)_y$ ,  $\text{W}_{1-y}(\text{Al}_2\text{O}_3)_y$  and *annealed*  $\text{W}_{1-y}(\text{Al}_2\text{O}_3)_y$  (at 1200°C in H<sub>2</sub>) taken from Abeles *et al.* ([29], Fig. 19 therein) and  $\text{Ag}_{1-y}(\text{SiO}_2)_y$ , Priestley *et al.* [33]. (b)  $\log[\sigma_A(y)/\sigma_A(0)]$  versus  $y/(1-y)$ , calculated by Equation (18) and  $\nu_A = 1-y$ . Insets in (a) and (b):  $\text{Cu}_{1-y}(\text{SiO}_2)_y$  and  $\text{Ni}_{1-y}(\text{SiO}_2)_y$ , taken from Liu *et al.* [14] and Pakhomov *et al.* [10], respectively.

$$\sigma_A = 2 \left( \frac{\pi}{3} \right)^{1/3} \frac{e^2}{h} L n^{2/3} = |e| \mu_A n, \quad (22)$$

where  $\mu_A$  is the mobility of the carriers which is assumed to be equal to the Hall mobility introduced in Sec. 2.  $h$  is Planck's constant.  $L$  is the (elastic) mean free path of the electronic carriers in the (metallic) phase A. Because of Equation (22) the exponential concentration dependence of  $n$ , Equation (1), is also reflected by the concentration dependence of  $\sigma_A(y)/\sigma_A(0)$  in **Figure 3** if the concentration dependences of  $L$  or  $\mu_A$  can either be neglected or change exponentially with  $y/(1-y)$  as well. For  $W_{1-y}(Al_2O_3)_y$  we assume that there are strong bonds between  $W$   $d$  orbitals and  $Si$  (and  $O$ )  $p$  orbitals, comparable with the situation in  $Ni_{1-y}(SiO_2)_y$  discussed earlier.

The only exception in **Figure 3**, where such an exponential concentration dependence of  $\sigma$ , respectively  $\sigma_A$ , does not occur, is represented by the *annealed*  $W_{1-y}(Al_2O_3)_y$  samples. This phenomenon will be discussed in Sec. 3.3.

3) With increasing  $y$  the temperature coefficient of resistivity, TCR, decreases and changes sign from positive to negative. [6] [11] [12] [14] [15] [34] The reason is an activation of localized electrons to the conduction band of the metallic phase. This conductivity contribution by activation is in competition with the positive contribution to the TCR due to scattering. The activation contribution is the larger the larger the amount of transferred electrons, *i.e.*, the larger  $y$ , in correspondence to Equation (1).

In earlier papers it was suggested “that the GHE is a result of the drastic reduction of both the effective electron density and (in case of EHE) the effective carrier mobility”<sup>8</sup> (Pakhomov *et al.* [11]) or a drastic reduction of carrier density (Jing *et al.* [35]). These two suggestions [11] [35] correspond to our physical model summarized in Sec. I. We emphasise, however, that it is not any *effective* electron density or *carrier* density (electrons or holes), but it is the *real electron* density which is reduced in the M-I composites.

### 3.3. The Effect of the Grain Size on the GHE

Approaching the M-I transition, the charging energy arising from the positively charged metal ions grows more and more and one could assume that such ‘metal’ phase cannot exist, because the electrostatic contribution by the positive ions increases more and more as  $n$  decreases. However, the growth of the electrostatic energy is not unbounded; decrease of  $n$  is accompanied with a decrease of the sizes of the metal grains. For *granular*  $Al_{1-y}Ge_y$  films, with increasing  $y$  the sizes of the metal grains decrease from 10 - 20 nm (on the metallic-rich side) to sizes  $< 2$  nm beyond the MIT (Rosenbaum *et al.* [36] [37]). This decrease of  $D_A$  with decreasing metal content even continues in the dielectric regime, as found for  $Ni_{1-y}(SiO_2)_y$ ,  $Pt_{1-y}(SiO_2)_y$  and  $Au_{1-y}(Al_2O_3)_y$  thin films ([29], Fig. 17 therein), where  $D_A$  decreases from 4 nm at  $y \approx 0.5$  to 1 nm at  $y \approx 0.9$ . For co-sputtered granular  $Ni_{1-y}(SiO_2)_y$  films, Abeles *et al.* found that the average particle size,  $D_A$ , decreases with Ni content:  $D_A = 14$  nm, 9.4 nm, 5.7 nm, and 3.7 nm for 87, 67, 56 and 37 vol % Ni, respectively ([29], Fig. 11 therein).

We suppose that the electron transfer described by Equation (1), respectively Equation (20), holds also beyond the M-I transition. This assumption correlates with the concentration dependence of  $D_A$ , which decreases continuously through the M-I transition as cited.

As mentioned earlier ([18], Sec. IVA therein), Equation (1), is part and result of a complex energy balance realized during solidification of the alloy, where *the sizes of the phase grains are part of this balance*. Equation (1) holds for situations, where atomic diffusion does practically not play a role because of the high cooling rate during the film deposition process. Because of this suppression of the long-range diffusion, the EMT provides a more realistic description of the electrical properties of disordered alloys with phase separation than any percolation description. This is justified in [2] (Sec. IVA therein).

On the other hand, at sufficiently high temperatures, appreciable diffusion can take place leading to additional growth of  $D_A$ . With increasing  $D_A$ , for instance due to annealing, the electron transfer to the phase boundaries can no longer be expected to follow Equation (1). Otherwise, the growth of the electrostatic energy could be shoreless.

Therefore, the GHE decreases or disappears by annealing at sufficiently high temperatures [14]. This phenomenon is also reflected by the concentration dependences of  $\sigma$  and  $\sigma_A$  which can be essentially smaller than before annealing. One typical example is  $W_{1-y}(Al_2O_3)_y$ , [29], **Figure 3**: Before annealing,  $\log[\sigma(y)/\sigma(0)]$  is

<sup>8</sup>EHE is applied in [11] for the extraordinary Hall effect in magnetic M-I composites.

approximately linear in  $y/(1-y)$ , but after annealing at 1200°C it is not. Reason is the fact that after annealing the metallic phase grains are essentially larger than before, for instance  $D_A \approx 20$  nm for  $y \approx 0.47$  (Abeles *et al.* [38], Fig. 2 therein), whereas  $D_A \approx 2$  nm for the unannealed samples (Abeles *et al.* [38], Fig. 1 therein). Because of the large phase grains in the *annealed*  $W_{1-y}(Al_2O_3)_y$  samples [38], the electron transfer (related to  $n(0)$ ) is essentially smaller than in the unannealed samples. Otherwise, the electrostatic energy would be too large.

This can also explain the experimental finding [14] that the maximum of the enhancement of  $R$  in  $Zn_{1-y}(SiO_2)_y$  is about 60, but 700 in  $Cu_{1-y}(SiO_2)_y$ : the size of the granules in  $Zn_{1-y}(SiO_2)_y$  is much larger ( $D_A \approx 20$  nm, [14], p.608) than in  $Cu_{1-y}(SiO_2)_y$ , for which  $D_A \approx 1$  nm is given as the minimum value ([14], p. 606). Apparently, in  $Zn_{1-y}(SiO_2)_y$  a certain measure of atomic diffusion has been happen during film deposition, so that this balance was shifted to smaller electron transfer, *i.e.*, Equation (1) does no longer apply.

## 4. Conclusions

A formula is derived for the Hall coefficient  $R$  of composites and applied to a discussion of the concentration dependence of  $R$  in M-I composites. From the empirical relation  $d \ln |R| = \alpha' \cdot d\eta$  with  $\eta = y/(1-y)$  found for experimental  $R$  data of  $Cu_{1-y}(SiO_2)_y$  and  $Ni_{1-y}(SiO_2)_y$  thin films, it is concluded that both the GHE and the *granular* structure typical for M-I composites are caused by *electron transfer* from the metallic phase to the insulating phase which obeys  $-dn = \beta \cdot n \cdot d \left( \frac{v_B}{v_A} \right)$ . This equation holds for nanocomposites, where long-range

atomic diffusion does practically not play a role during the film deposition process. It is part and result of a complex energy balance realized during solidification of the alloy, where the sizes of the phase grains are part of this balance.

In M-I composites, the decrease of electron density  $n$  in the metallic phase occurs as interface charges occupying surface states on the insulating phase which is responsible for the *granular* structure.

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