

Radon exhalation from phosphogypsum stabilized in sulfur polymer cement

Irene García-Díaz^{1*}, Francisco José Alguacil¹, Manuel Gázquez², Juan Pedro Bolívar², Israel López Coto², Félix A. López¹

¹Centro Nacional de Investigaciones Metalúrgicas (CENIM), CSIC, Avda. Gregorio del Amo, Madrid, Spain;

*Corresponding Author: irenegd@cenim.csic.es

²Departamento de Física Aplicada, Universidad de Huelva, Campus del El Carmen, Huelva, Spain

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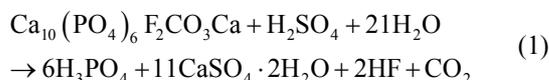
ABSTRACT

Phosphogypsum (PG), primary by-product from phosphoric acid production, is accumulated in large stock-piles which were active until 2010, when spills were banned. It is considered as NORM material that contains radionuclides from ²³⁸U and decay series which are of most radio-toxicity. PG was valorized and/or recycled in a building material, sulfur polymer cement (SPC). The SPC-PG samples reach the international regulation to use in the manufacture of building materials without radiological restrictions, except the sample with the 50% of PG. Under normal conditions of ventilation the contribution to the expected radon indoor concentration is also below the international recommendation.

Keywords: Radon; Phosphogypsum; NORM; Radioactivity; Sulfur polymer Cement

1. INTRODUCTION

The phosphate rock, due to its origin, is affected by high concentration of impurities, heavy metals, naturally occurring radionuclides and other so-called trace elements. A common mineral in phosphate rock is the carbonate fluorapatite, in which up to the 0.02% U can substitute for positions typically occupied by atoms of calcium in the structure [1]. The phosphate rock is treated with sulfuric acid to produce phosphoric acid by the dihydrate process according to Eq.1 [2,3]. During this process is also produced a by-product called phosphogypsum (PG).



The composition of PG is dominated by gypsum, impurities including Al, P, F, Si, Fe, Mg as well naturally-occurring radionuclides which originate mainly from the phosphate rock used in the processing. Concentration of these hazardous elements, may vary mainly depending on the origin of the phosphate rock and to a lesser extent, on factor such as plant generation and PG age [4].

Most sedimentary phosphate rock deposits contain elevated levels of radionuclides from ²³⁸U in secular equilibrium with its daughters [5]. Chemical processing of the phosphate rock in order to produce phosphoric acid, results in a fractionation into the acids and PG of radioelement contained in phosphate rock [6]. The phosphogypsum contains specific activities of ²²⁶Ra, the decay chain segment in the uranium series, between one and two orders of magnitude higher than the natural gypsum depending on the uranium content of the rock [7].

The radium 226 has a half life of 1620 years and is the long-term source radioactivity in most PG. One of the major concerns of materials which contain enhanced levels of ²²⁶Ra is the production of ²²²Rn gas. ²²²Rn and its short-lived decay products are the most important contributor to human exposure to ionizing radiation which can causes health damages.

Due to the radionuclides concentration the by-products, PG, is considered as NORM material (Naturally Occurring Radioactive Materials) [8,9].

Large quantities of PG are produced, the world production was 200 - 280 × 10⁶ t per year [10]. Several phosphate processing plants are located on the south-western coast of Spain (on the outskirts of the town of Huelva) close to the estuary of the Odiel and Tinto rivers, where phosphoric acid has been produced since 1968. The company imports sedimentary phosphate rocks from Morocco, which mainly contain around 100 - 150 ppm of U [3]. Until 2010 the PG production at Huelva was around 3 ×

10^6 t per year [11]. This by-product was accumulated in regulated stock-piles and occupied vast areas of land, located in the town's surroundings with the consequent environmental problem.

Therefore the waste and the by-products are gaining more and more attention nowadays, such research and/or production is being carried out to the incorporation of these wastes and by-products (fly ash, red mud, coal slag, ceramic waste) as building material [12-15].

The sulfur polymer cement, SPC, has been used in civil engineering (column supports, pump foundations, walls in storage areas, etc.) due to its excellent properties, which for certain applications are superior to ordinary Portland cement (OPC). The SPC presents high durability and fast setting time and rapid gain of high strength, achieving most of its mechanical strength in less than 1 day of curing. It has also recently emerged as a possible alternative as a binding and stabilizing agent for the solidification and stabilization of hazardous, low-level radioactive and mixed wastes [16].

Due to the relatively high levels of natural radionuclides in the PG an important radiation exposure could be received from building materials containing this by-product. This implies the need to control it.

Different international recommendations propose reference values of the natural radionuclide concentrations in building materials (Publication No. 112 from monographic collection "Radiation Protection" issued by the European Union) [17]. The activity concentration index (I), is calculated on the bases of the activity concentrations of radium (^{226}Ra) in the uranium (^{238}U) decay series, radium (^{238}Ra) in the thorium (^{232}Th) decay series and potassium (^{40}K), **Eq.2**. I index ensures that external gamma dose rate inside de room from building materials does not exceeded 1 mSv per year, **Table 1**. When the gamma dose are limited to levels below 1 mSV per year, the ^{226}Ra concentration in the materials are limited, to levels which are unlike to cause indoor radon concentration exceeding the design level of $200 \text{ Bq}\cdot\text{m}^{-3}$.

$$I = C(^{226}\text{Ra})/300 + C(^{228}\text{Ra})/200 + C(^{40}\text{K})/3000 \quad (2)$$

where $C(^{226}\text{Ra})$, $C(^{228}\text{Ra})$, $C(^{40}\text{K})$ are the activity concentrations for ^{226}Ra , ^{228}Ra and ^{40}K , respectively in the building material considered, expressed in $\text{Bq}\cdot\text{Kg}^{-1}$.

Other countries considered to the radiological control of building material the equivalent radium concentration parameter, $\text{Ra}(\text{eq})$, which is shown in **Eq.3**:

$$\text{Ra}(\text{eq}) = C(^{226}\text{Ra}) + 1.43 C(^{228}\text{Ra}) + 0.077C(^{40}\text{K}) \quad (3)$$

The reference value for $\text{Ra}(\text{eq})$ in many countries for building materials is $370 \text{ Bq}\cdot\text{kg}^{-1}$ [18]. The radon-222 and its short-lived daughters contributions are on 50% of the total natural effective dose received by the population [19]. As a consequence, many countries have established

reference levels for radon in houses and work places, being these values of 200 and $400 \text{ Bq}\cdot\text{m}^{-1}$, respectively.

So the main objective of this research was to evaluate the radiological impact of phosphogypsum stabilized in sulfur polymer cement.

2. EXPERIMENTAL

Various SPC samples were studied. These were obtained by a mix of different proportions of phosphogypsum, sulfur, gravel, sand and a thermoplastic material used as modified sulfur containing polymer [20], **Table 2**. The SPC samples were manufactured according to López *et al.* [21].

The ratio of gravel/sand and sulfur/modified sulfur (STX^{TM}) was maintained constant at 0.5 and 10 respectively. These relations are the best condition for the viscosity and workability of the mixture [21,22].

Phosphogypsum has been added to the mixtures at dosages between 10 and 50 wt%.

Each sample was called as SPC X-Y where "X" is the percentage wt% of elemental sulfur and "Y" is the percentage wt% of phosphogypsum of the mixtures.

The SPC sample reference, SPC 21 - 0, was manufactured as to the PG-SPC samples, but in this case, calcium carbonate (99.5% purity, Panreac) was added as filler in substitution of PG.

2.1. Measurement of Radionuclides

A gamma spectrometry system with an XtRa coaxial germanium detector (Canberra), which has a 38% relative

Table 1. Dose criteria recommendation to activity concentration index (I).

0.3 mSV/year	1.0 mS/per year	Uses
$I \leq 0.5$	$I \leq 1$	Materials used in bulk amount, e.g. concrete, cement etc.
$I \leq 2$	$I \leq 6$	Material superficial and other materials with restricted use, e.g. tiles, boards etc.

Table 2. Composition of SPC samples (wt%) and sulfur/PG ratio.

Samples	Sulfur (S)	Gravel	Sand	PG	S^{STX}	S/PG
SPC 21-0	21.0	23.1	46.1	0.0	2.1	0.00
SPC 17-10	17.0	23.8	47.5	10.0	1.7	1.70
SPC 19-20	19.0	19.7	39.4	20.0	1.9	0.95
SPC 21-30	21.0	15.6	31.3	30.0	2.1	0.70
SPC 26-40	26.0	10.5	20.9	40.0	2.6	0.65
SPC 30-50	30.0	5.7	11.3	50.0	3.0	0.60

efficiency, and FWHM of 0.95 keV at the 122 keV line of ^{57}Co and 1.9 keV at the 1333 keV line of ^{60}Co were used to the radioactive characterization. The detector was coupled to a conventional electronic chain, including a multichannel analyser and was shielded with Fe 15 cm thick. The samples were dried at 60°C and grounded. The whole procedure of calibration and this gamma spectrometry system are described elsewhere [18].

2.2. Radon Potential and Bulk Exhalation Measurements

The radon exhalation is the radon flow released through the available surfaces ($\text{Bq}\cdot\text{m}^{-2}\cdot\text{h}^{-1}$), influenced by the material geometry and the boundary conditions. On the other hand, the radon potential is defined as the radon concentration generated inside the material and that is available to be transported through its pores.

The method to measure the radon potential and the emanation factors is described by López-Coto *et al.* [19]. From growth curves of radon inside a closed chamber it is possible to calculate the exhalation rate of the block and, under specific experimental conditions, the radon potential of the tested material. In addition, once crushed a portion of the specimen (about one third), from a second measurement in the chamber for obtaining radon potential and the real emanation factor of the material.

2.3. Radon Transport Simulations

The equation of radon conservation in the building material has allowed us to develop a 3D model of diffusive transport in porous media. This model has been solved for two geometries; a block of $0.04 \times 0.04 \times 0.16 \text{ m}^3$ and a plate of $1 \times 1 \times 0.04 \text{ m}^3$, which was carried out by using a numerical algorithm based on finite elements on an unstructured tetrahedral mesh.

Knowing the exhalation rate of the building materials

used to construct a specific room, it is possible by modeling to estimate the expected radon concentration in this room under certain ventilation conditions [23]. In this sense, it has been applied a simple model of radon accumulation in a standard room of $5 \times 5 \times 2 \text{ m}^3$ coated on all sides by plates of the same material.

3. RESULT AND DISCUSSION

3.1. Activity Concentration and Index Risk

Table 3 shows the radionuclide concentration of PG and SPC samples. Prior to possible use of PG-SPC as building materials, a preliminary radiological analysis have been carried out in order to reliably assess the radiation dose. Attending to these results it will be possible to decide whether these materials can be used, from a radiological point of view.

The activity concentrations of ^{238}U and ^{226}Ra in the pure PG sample are around 100 and $600 \text{ Bq}\cdot\text{kg}^{-1}$ respectively, these values are in agreement with typical values given in the literature for PGs from Huelva [24], which are significantly higher than the average world-wide values from soils ($25 \text{ Bq}\cdot\text{kg}^{-1}$ of ^{238}U and daughters) [25].

The radionuclides with the highest activity concentration in the SPC samples are ^{226}Ra (and its daughters of small half live: ^{222}Rn , ^{218}Pb , ^{218}Bi , ^{214}Pb , ^{214}Bi , etc.), and ^{40}K .

Linear decrease in activity concentration of ^{40}K at increases the PG content in the sample it is observed, **Figure 1**. It is due to the very low content of potassium in PG ($<18 \text{ Bq}\cdot\text{kg}^{-1}$ of ^{40}K , *i.e.*, $<0.06\%$ of natural potassium). The concentration of ^{40}K in all SPC-PG samples remains below the world average of ^{40}K from soil, $400\text{-}500 \text{ Bq}\cdot\text{kg}^{-1}$, only SPC 17 - 10 slightly exceeds this value.

Figure 1 shows a strong lineal dependence ($r^2 =$

Table 3. Radionuclide concentration of SPC samples and PG ($\text{Bq}\cdot\text{Kg}^{-1}$).

Code	SPC 21 - 0	SPC 17 - 10	SPC 19 - 20	SPC 21 - 30	SPC 26 - 40	SPC 30 - 50	PG
% PG	0	10	20	30	40	50	100
^{210}Pb	8.0 ± 0.6	70 ± 5.0	143 ± 9.0	219 ± 13.0	264 ± 16.0	340 ± 20.0	624 ± 37.0
^{238}U (^{234}Th)	12 ± 2.0	21 ± 2.0	12 ± 2.0	38 ± 3.0	50 ± 4.0	60 ± 4.0	97 ± 6.0
^{232}Th (^{212}Pb)	9.1 ± 0.6	9.4 ± 0.7	8.6 ± 0.6	8.1 ± 0.5	5.9 ± 0.4	5.8 ± 0.4	8.2 ± 1.0
^{226}Ra	7.4 ± 0.5	63 ± 4.0	115 ± 7.0	179 ± 11.0	226 ± 13.0	282 ± 17	589 ± 34.0
^{228}Th	8.8 ± 0.8	8.7 ± 0.7	<6	6.8 ± 0.7	7.3 ± 0.6	6.1 ± 0.6	7.8 ± 0.7
^{228}Ra (^{228}Ac)	8.2 ± 0.8	8.6 ± 0.8	8.8 ± 0.8	6.9 ± 0.7	<4	<4	8 ± 1.0
^{40}K	580 ± 30.0	528 ± 32.0	394 ± 24.0	347 ± 21	239 ± 15.0	143 ± 10.0	<18
Index	0.26	0.43	0.56	0.75	0.85	1.01	2.01
Ra(eq) ($\text{Bq}\cdot\text{Kg}^{-1}$)	63	117	253	158	217	301	600

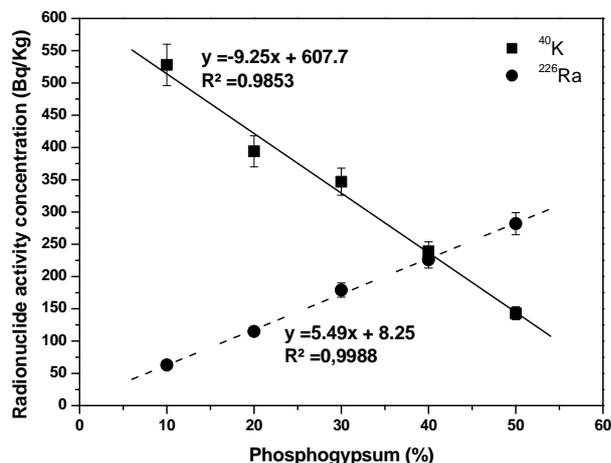


Figure 1. Variation of activity concentration of ^{40}K and ^{226}Ra ($\text{Bq}\cdot\text{kg}^{-1}$) with content of PG in the SPC samples.

0.9988) between the percentage of PG added and the activity concentration of ^{226}Ra . To the value of $x = 0\%$ PG, the activity concentrations obtained is very low, around $8 \text{ Bq}\cdot\text{kg}^{-1}$ of ^{226}Ra , similar to ^{226}Ra activity concentration in SPC 21 - 0. On the contrary, if we considering $x = 100\%$, pure PG, it is obtained an activity concentration for ^{226}Ra of $557 \text{ Bq}\cdot\text{kg}^{-1}$, value very similar to indicated in **Table 3** for PG sample, $589 \text{ Bq}\cdot\text{kg}^{-1}$. These considerations can be also used to ratify the radiometric measuring methods applied to the studied samples.

The SPC-PG samples contain radioactive nuclides if the sulfur polymer cements are used as building materials, it must be confirmed that the action level of $1 \text{ mSV}\cdot\text{year}^{-1}$ is not be exceeded.

So, in relation to the radiological assessment, according to the recommendations of the radioactivity protection commission of EU [17], the activity concentration index (I) in the studied samples are agree with the EU references values the range of $0.3 - 1 \text{ mSv}\cdot\text{a}^{-1}$ (**Table 1**). Only SPC 30 - 50, with the 50% of PG, presents an I value around 1, so this could not be used in bulk amounts. On the other hand, the values of $\text{Ra}(\text{eq})$ for all samples are below the set limit of $370 \text{ Bq}\cdot\text{kg}^{-1}$ [18,19], which is the limit considered in USA to building materials.

3.2. Radon Potential and Exhalation Rate of Matrix and Blocks

The emanation factor is the fraction of radon produced in the material that is free to be transported through its pores. The product of radium concentration per the emanation factor is the radon potential, Rn Pot, it is characteristic of the material and is not influenced by the experimental conditions during its determination. Rn Pot is a suitable parameter for classifying/comparing porous material in relation to its potential radon radiological risk [26]. **Table 4** shows the results of radon potential and the

emanation factor for PG and SPC in milled samples.

The highest value of Rn Pot is obtained to the pure PG sample, $68.4 \text{ Bq}\cdot\text{kg}^{-1}$. An increase in the fraction of PG in the PG-SPC samples increases the Rn Pot, with ranging values from 10.3 to $30.6 \text{ Bq}\cdot\text{kg}^{-1}$. On the other hand, the emanation factors are very similar for all samples, including PG, with values ranging from 0.1 and 0.16.

The evaluation of apparent emanation factor was also studied, **Table 4**. This parameter is affected by the structural change in the solid sample. The SPC-PG samples show an E_a always lower than the original components for its manufacturing, because the curing process significantly reduces the emanation factor.

Table 5 shows the values of radon exhalation, E, in the SPC-PG blocks. These values are in the order of magnitude of the detection limit of the measurement system, being the uncertainties associated relatively high. However, these measurements allow to verify the low radon exhalation rates obtained in any case exceed of $5 \text{ Bq}\cdot\text{m}^{-2}\cdot\text{h}^{-1}$.

The diffusion coefficient was also studied, **Table 5**. It is a parameter characteristic of radon diffusion flow. Lower values of D_b indicated a less radon diffusion flow.

Table 4. Radon potential, Rn Pot, apparent emanation factor, E_a and radon emanation factor, E_f (σ and Σ are their standard deviations).

Sample	Milled samples				
	Rn Pot $\text{Bq}\cdot\text{kg}^{-1}$	σ $\text{Bq}\cdot\text{kg}^{-1}$	E_a	E_f	Σ
SPC 17 - 10	10.3	0.9	0.015	0.164	0.020
SPC 19 - 20	11.3	1.0	0.08	0.098	0.012
SPC 21 - 30	22.3	1.7	0.08	0.132	0.014
SPC 26 - 40	19.1	1.0	0.07	0.084	0.007
SPC 30 - 50	30.6	1.7	0.05	0.108	0.009
PG	68.4	4.2		0.116	0.011

Table 5. Radon exhalation, E (σ is standard deviations), and diffusion coefficient, D_b , calculated for blocks, $0.04 \times 0.04 \times 0.16 \text{ m}^3$.

Sample	E	σ	D_b
	$\text{Bq}\cdot\text{m}^{-2}\cdot\text{h}^{-1}$	$\text{Bq}\cdot\text{m}^{-2}\cdot\text{h}^{-1}$	$\text{m}^2\cdot\text{s}^{-1}$
SPC 17 - 10	1.0	3.8	4.58×10^{-8}
SPC 19 - 20	1.0	3.8	2.27×10^{-8}
SPC 21 - 30	1.4	0.9	4.24×10^{-8}
SPC 26 - 40	1.5	0.9	6.57×10^{-8}
SPC 30 - 50	1.5	1.0	1.24×10^{-7}

The sample with 50% of PG, SPC 30 - 50, presents the higher value $1.24 \times 10^{-7} \text{ m}^2 \cdot \text{s}^{-1}$.

3.3. Simulation by Modeling of Exhalation Rates

It has been carried out by modeling a simulation of a block of polymer cement (SPC 30 - 50) that emanates through all its sides excepting for the base ($0.04 \times 0.16 \text{ m}^2$). The blocks not have a radon exhalation rate uniform, showing the geometry effect of this parameter, **Figure 2**. In turn, the mean value for radon exhalation throughout its surface in contact with air is $3.6 \pm 1.6 \text{ Bq} \cdot \text{m}^{-2} \cdot \text{h}^{-1}$, very similar to the experimental values ones.

This model was applied to different plate $1 \times 1 \times 0.04 \text{ m}^3$ made off SPC-PG samples, the exhalation rates range, **Table 5**, were from 4 to $12 \text{ Bq} \cdot \text{m}^{-2} \cdot \text{h}^{-1}$, being of the same order of magnitude or slightly higher of typical building materials, which have a range of 1 - $10 \text{ Bq} \cdot \text{m}^{-2} \cdot \text{h}^{-1}$ [27-29].

The plate made with SPC 30 - 50 present the highest mean values for the exhalation rate, $11.7 \pm 1.4 \text{ Bq} \cdot \text{m}^{-2} \cdot \text{h}^{-1}$, assuming an exhalation only in one side, it is due to the highest Rn Pot values, $30.6 \text{ Bq} \cdot \text{kg}^{-1}$. **Figure 2** shows the radon exhalation rates obtained for different surface points of plate SPC 30 - 50, the highest values are founded near the edges of the plate. Thus, the central part of the plate presents a value of $9 \text{ Bq} \cdot \text{m}^{-2} \cdot \text{h}^{-1}$, while their edges have values until above $15 \text{ Bq} \cdot \text{m}^{-2} \cdot \text{h}^{-1}$.

The expected radon concentration inside a standard room ($5 \times 4 \times 2.5 \text{ m}^3$) built with the plates shown in **Figure 3**, is presented in **Table 6**. In the standard room with a good ventilation (air enhance, $\lambda_v = 2 \text{ h}^{-1}$) the highest expected radon concentration is reached inside the room with SPC 30 - 50, sample with 50% of PG, $C_{Rn} = 10 \text{ Bq} \cdot \text{m}^{-3}$, but this value not exceeded the average radon

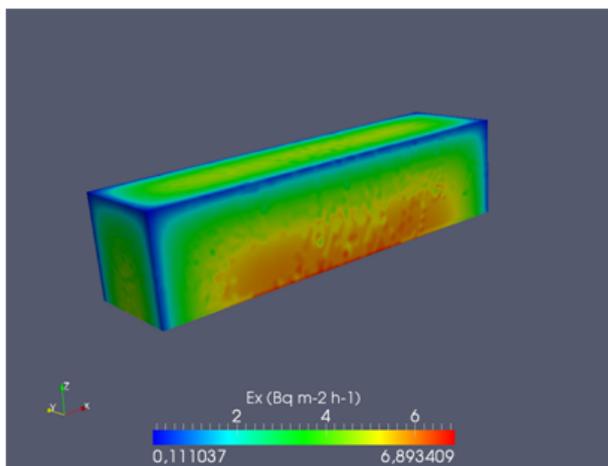


Figure 2. Radon exhalation rate obtained by modeling a specimen of $0.04 \times 0.04 \times 0.16 \text{ m}^3$ made with SPC 30 - 50 samples.

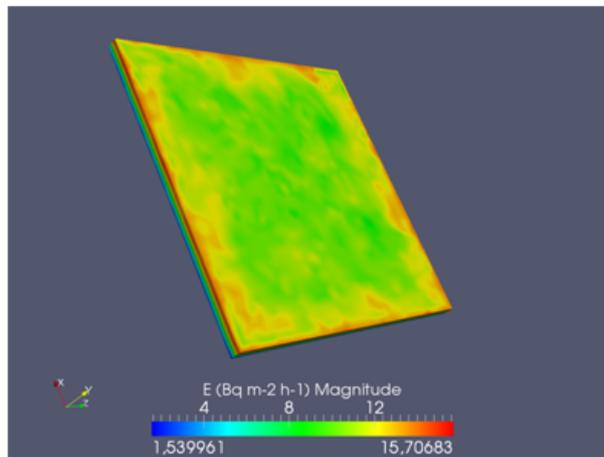


Figure 3. Radon exhalation rate obtained for different surface points of plate ($1 \times 1 \times 0.04 \text{ m}^3$) of SPC 30 - 50 samples.

Table 6. Radon exhalation rate (E) of a plate ($1 \times 1 \times 0.04 \text{ m}^3$) and the expected radon concentration (C_{Rn}) in a standard room.

Sample	E $\text{Bq} \cdot \text{m}^{-2} \cdot \text{h}^{-1}$	σ $\text{Bq} \cdot \text{m}^{-2} \cdot \text{h}^{-1}$	C_{Rn}	C_{Rn}
			($\lambda_v = 2 \text{ h}^{-1}$) $\text{Bq} \cdot \text{m}^{-3}$	($\lambda_v = 0.1 \text{ h}^{-1}$) $\text{Bq} \cdot \text{m}^{-3}$
SPC 17 - 10	4.0	0.5	4	67
SPC 19 - 20	4.4	0.5	4	74
SPC 21 - 30	8.7	1.1	8	146
SPC 26 - 40	7.5	0.9	7	125
SPC 30 - 50	11.7	1.4	10	196

concentrations to $200 \text{ Bq} \cdot \text{m}^{-3}$, reference value in the EU for new houses. Under poor ventilation ($\lambda_v = 0.1 \text{ h}^{-1}$) the average radon concentrations increases. In SPC 30 - 50 the radon concentration achieved was $196 \text{ Bq} \cdot \text{m}^{-3}$, this value is very similar to the reference value in the EU, $200 \text{ Bq} \cdot \text{m}^{-3}$.

4. CONCLUSIONS

The activity concentration indexes, I, in the SPC-PG samples are lower than the reference value, not exceeding the $1 \text{ mSv} \cdot \text{year}^{-1}$. Therefore, these cements can be used without radiological restrictions in the manufacture of building materials, except in the sample with the 50% of PG.

On the other hand, the equivalent radium concentration, $Ra(\text{eq})$, in all the SPC samples have values less than the reference values set by the EPA for constructions materials ($370 \text{ Bq} \cdot \text{kg}^{-1}$). The higher values of $Ra(\text{eq})$ are obtained in SPC 30 - 50.

Under normal conditions of ventilation, the contribu-

tion to the expected radon indoor concentrations is below the international recommendations for indoor radon, so the building materials studied in this work can be applied in the house' construction under normal ventilation conditions.

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