

Cocoa Cortex Ashes as Fluxing Additive for Vitrified Ceramic Making from Alluvial Clay

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Abstract

The aim of this study is to use Cocoa Cortex Ash (CCA) as alternative fluxing agent to manufacture vitrified ceramics at low temperatures from alluvial clay. Specimens of mixtures including clay and CCA (0%, 10%, 20% and 30% by mass) were used and fired respectively at 1050°C and 1100°C. X-ray diffraction and scanning electron microscopy were carried out. γ -alumina, mullite, akermanite, anorthite and grossular are new crystalline phases formed. Also, technological properties were determined on fired specimens as a function of CCA mass percentage. The results showed that firing shrinkage increased up to 8.5% for specimens with 10% by mass of CCA, then lessened up to 2% for specimens with 30% by mass of CCA. When fired at 1100°C, the specimens that initially contained 10% by mass of CCA allowed the formation of compact bodies with water absorption of 2% and flexural strength of 32 MPa. Hence, mixed at low percentage with poorly fluxing kaolinitic clay, CCA can be used successfully as flux for the production of vitrified ceramics such as stoneware at low temperatures. The mixture of CCA with kaolinitic clay also promotes the formation of mullite and anorthite at low temperature.

Keywords

Poorly Fluxing Clay, Cocoa Cortex Ash, Flux, Stoneware

1. Introduction

Vitrified ceramics are known for their quasi impermeability, their durability, their excellent mechanical performance and their resistance to corrosion and

chemical agents. They can be designated by porcelain or stoneware, depending on the purity of the raw material. They are used for domestic purposes as sanitary bodies, in construction as wall and floor tiles, and even in the environmental protection as sanitation pipes [1]. Vitriified ceramics are manufactured either from a clay alone containing enough amounts of fluxing oxides or from a mixture of poorly fluxing clay and additive fluxes. The firing temperature is usually between 1120°C and 1300°C [2] [3] [4]. Low sintering temperatures lead to insufficient maturation and less compact products with important amount of pores. Also, very high temperature leads to deformation of specimens as a result of the formation of great quantity of viscous phase due to the flux content [2] [3] [4] [5]. Feldspars are fluxes generally used for manufacturing vitriified ceramics because of their high content in alkali oxides such as K_2O and Na_2O which are responsible of the vitrification process. The formation of vitreous phase is favorable to improve densification of the products, mechanical properties and decrease of the water absorption because of few amounts of pores [6] [7]. Fluxes also influence the new minerals phase formation and the microstructure of the firing products during sintering. However, difficult access to pure feldspars and sometimes their high melting point due to the presence of other phases such as quartz [8] led some authors to experiment with other sources of flux: Ergul *et al.* [7] have studied the physical properties of a batch of specimens composed of 50% by mass of basaltic tuffs and 50% by mass of industrial clay at 1150°C. Elsewhere, for the manufacture of wall tiles, Das *et al.* [9] used kaolinitic clay with other raw materials including fly ash, wollastonite and dolomite and obtained products whose flexural strength reached 30 MPa at 1150°C. For the preparation of glass-ceramic, Vu *et al.* [10] formulated a mixture composed of bottom ash (80% by mass) and fly ash (20% by mass) to get specimens which were fired at 950°C. Kamseu *et al.* [11] used pegmatite and nepheline syenite to experiment at 1175°C low process of porcelainized stoneware and to evaluate pore size distribution. Recently, Njindam *et al.* [12] used glass powder with clay mixture to manufacture porcelain stoneware wall and floor tiles at 1150°C. The production of cocoa is well developed in most tropical regions around the world, and such exploitation leads to a significant volume of cocoa cortex waste. Cultivation of Cocoa is very large in the world-wide. Cameroon is the world's fifth large producer of Cocoa, and it is closely concerned with the valorization of such waste [13]. The cocoa cortex which represents 68 wt% of the whole fruit, carries a toadstool responsible for brown rot on cocoa plants. The valorization of this waste is effective in sectors such as agriculture and livestock [14]. When cocoa cortex is calcined at 1000°C, the obtained ashes contains high amount of potassium oxide, which make this waste a potential flux source for the manufacturing of vitriified ceramics. Regarding the existing literature, the effect of cocoa cortex ashes (CCA) on the mechanism of novel phases formation and the microstructure of clay based vitriified ceramics has not yet experimented. The present works is focusing on the elaboration of vitriified ceramic at low temperature using cocoa cortex ashes as alternative fluxing agent for improve vitrification of ceramic

made from a poorly fluxing clay. The raw materials and the fired one were submitted to X-ray diffraction, electronic microscope and physico-mechanical testing for the evaluation of the phase conversion from raw to fired product and performances of the fired products.

2. Materials and Experimental Techniques

Alluvial clay (EB) collected from the locality of Ebebda, (Center Region of Cameroon) according to the following geological coordinates: 04°23'30"N and 11°15'21"W) is used. This clay is grey with random appearance of red and brown spots, compact and very plastic. According to Munsel Code [15], its dried powder color code is 5YR6/4 (brown). Crude cocoa cortex was collected in a cocoa farm also located at Ebebda. The collected cortex, was washed with distilled water, oven dried at 105°C, ground and sieved over a 100 µm mesh. The cocoa cortex ash (CCA), was obtained after firing the raw cocoa cortex powder at 1000°C in a programmable electrical furnace (Nabertherm, model LH 60/14) at a heating rate of 5°C/min and soaking time of two hours. The ashes was furnace cooled to room temperature, and sieved over a 100 µm mesh and store in polyethylene bags prior to their use. Powdered raw materials were subject to chemical analysis and X-ray diffraction analysis. The chemical composition of the raw materials (alluvial clay and cocoa cortex ash) was obtained using a XRF PANalytical Zetium Spectrometer. The XRD pattern was registered using a Bruker Advanced D8 diffractometer device, with Cu K α = 1.5418 Å and the JCPDF files were used for mineralogical identification. For the ceramic bodies, mixtures of raw materials (alluvial kaolinite clay and cocoa cortex ash) were made by varying the content of CCA from 0% to 30% by mass to get specimens denoted as C0, C10, C20 and C30 respectively (Table 1). Each mixture was moistened with distilled water (5% by mass) and the obtained paste was molded and pressed using uniaxial hydraulic press (SPECAC Model). Test samples forms and dimensions were the following: parallelepiped (2 cm × 2 cm × 6 cm) for determination of flexural strength and firing shrinkage; cylindrical (height 6 mm; diameter 12 mm) to determine bulk density, apparent porosity and microstructure. The resulted specimens were dried at ambient temperature of laboratory for 48 hours and then oven dried at 105°C till constant mass. Before being fired at 1050°C and 1100°C in a programmable electric furnace (Nabertherm, Model LH 60/14), the thermal behavior of the alluvial kaolinite clay and the experimented mixtures were obtained through differential scanning calorimetry (DSC), thermogravimetric

Table 1. Composition of the mixtures expressed as percentage by mass.

specimens	EB	CCA
C0	100	0
C10	90	10
C20	80	20
C30	70	30

(TG) and dilatometric analyses. Dilatometric analysis was done using a Setaram TMA Setsys Evo device at 5°C/min under air, while the DSC and TG analyses were obtained by using coupled DSC/TGA NETZSCH STA 429 (CD) equipment under air at 10°C/min. For DSC/TG experiments, a Pt crucible was used for both sample and reference powders, the reference material used consisted of alumina powder previously heated at 1600°C. Firing shrinkage was determined according to ASTM C326-03 [16], water absorption, bulk density were determined according to the normNF EN ISO 10545-3 [17], and Flexural strength was measured in accordance with the normNF EN ISO 10545-4 [18], using an electro hydraulic press (M & O, model). Scanning Electron Microscopy (SEM) was achieved using a QUANTA 450 FEG microscope equipped with LINK –OXFORD XLII EDAX system.

3. Results and Discussion

3.1 Raw Materials Characterization

3.1.1. Chemical Composition and Mineralogy

Chemical compositions of alluvial clay (EB), CCA and the experimented mixtures (C0, C10, C20 and C30) are given in **Table 2**. Also, **Figure 1** gives the EDS spectrum of powder of cocoa cortex ash (CCA).

EB is mainly composed of SiO₂ (53.05% by mass), Al₂O₃ (22.12% by mass) and Fe₂O₃ (7.87% by mass). So, the silica (SiO₂) and alumina (Al₂O₃) contents are corresponding to kaolinite content in the sample, along with the presence of hematite as impurity. The color of the clay (brown, 5YR6/4) according to Munsel Code is probably related to the presence of both Fe₂O₃ and TiO₂ (2.5% by mass). The value of the loss on ignition in EB (12.5% by mass) is close to that

Table 2. Chemical compositions of EB and CCA, and the mixtures (C10 and C20 and C30).

OXIDES	EB (% by mas)	CCA (%)	C10 (%)	C20 (%)	C30 (%)
SiO ₂	53.05	3.73	48.13	43.19	38.25
Al ₂ O ₃	22.12	1.05	20.01	17.90	15.80
K ₂ O	1.17	45.83	5.63	10.10	14.57
Na ₂ O	0.12	0.21	0.13	0.14	0.14
Fe ₂ O ₃	7.87	0.42	7.17	6.38	5.64
TiO ₂	2.50	0.14	2.26	2.03	1.79
MgO	0.37	7.71	1.05	1.73	2.41
CaO	0.05	10.23	1.07	2.09	3.11
P ₂ O ₅	0.11	6.29	0.73	1.35	1.95
MnO	/	0.13	0.013	0.026	0.039
SrO	/	0.13	0.013	0.026	0.039
SO ₃	/	2.49	0.249	0.498	0.747
LOI at 1050°C	12.46	22.12			

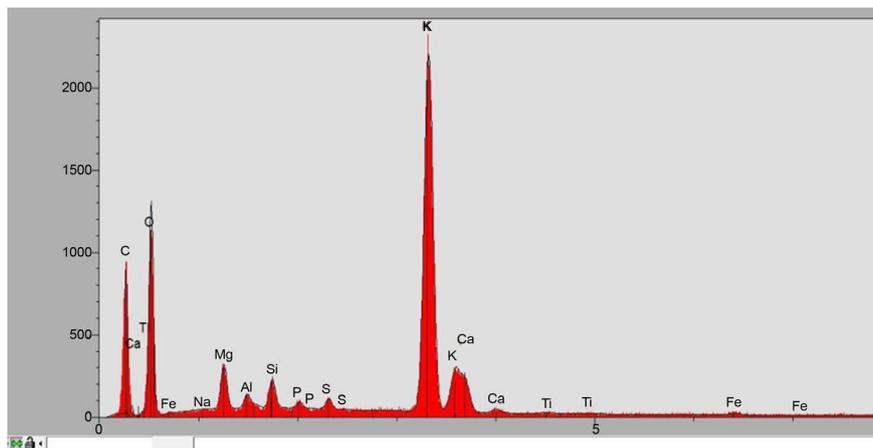


Figure 1. EDS analysis of CCA.

observed by Pialy *et al.* and Nkoumbou *et al.* [19] [20] within kaolinitic clays. Cocoa cortex ash exhibits high content of K_2O (45.83% by mass) (**Table 2** and **Figure 1**), which is of interest for the use of CCA as a flux source. Also, Al_2O_3 (1.05% by mass), SO_3 (2.49% by mass), SiO_2 (3.17% by mass), P_2O_5 (6.28% by mass), MgO (7.17% by mass) and CaO (10.23% by mass) are present in CCA and could indicate the presence of various compounds. Other oxides as Fe_2O_3 , Na_2O , TiO_2 , MnO , SrO are also present in CCA at very low content. X-ray diffraction pattern of EB shows that kaolinite (JCPDF 01-0527) is the main mineral phase. It is associated to hematite (JCPDF 03-0812), rutile (JCPDF 77-0443) and quartz (JCPDF 89-8937) (**Figure 2(a)**). X-ray pattern of CCA (**Figure 2(b)**) shows the presence of arcanite (JCPDF 24-0703), potassium phosphate oxide (JCPDF 08-0225), potassium oxide (JCPDF 77-2176) and Merwinite (JCPDF 02-0949) as crystalline phases.

SEM observation of EB shows pseudo hexagonal platelets of kaolinite with irregular shape (**Figure 3**) which indicates that the latter mineral is not well crystallized [21]. SEM observation of CCA shows white flocculated clusters of variable forms with black stains that can be assigned to carbon resulted by combustion of organic matter.

3.1.2. Thermal Behavior of Alluvial Clay and Experimented Mixtures

The thermal analyses curves (DSC and TG) of EB and of the mixtures C10 and C30 are shown in **Figure 4**. The three DSC curves exhibit an endothermic peak with the maximum between $95^\circ C$ and $116^\circ C$ which corresponds to elimination of hygroscopic water. For the specimens C10 and C30, the latter peak increased with increasing amount of CCA and it was accompanied by a significant weight loss. Indeed, according to our observation, when the powder of CCA was in contact with ambient air of laboratory, it became more and more moisten, which explains its increase content of hygroscopic water. The weak exothermic peak observed in EB at $290^\circ C$ is assigned to decomposition of organic matter [19] [21]. The second endothermic peak with maximum located between $490^\circ C$ and $516^\circ C$ corresponds to the dehydroxylation of kaolinite, which is transformed

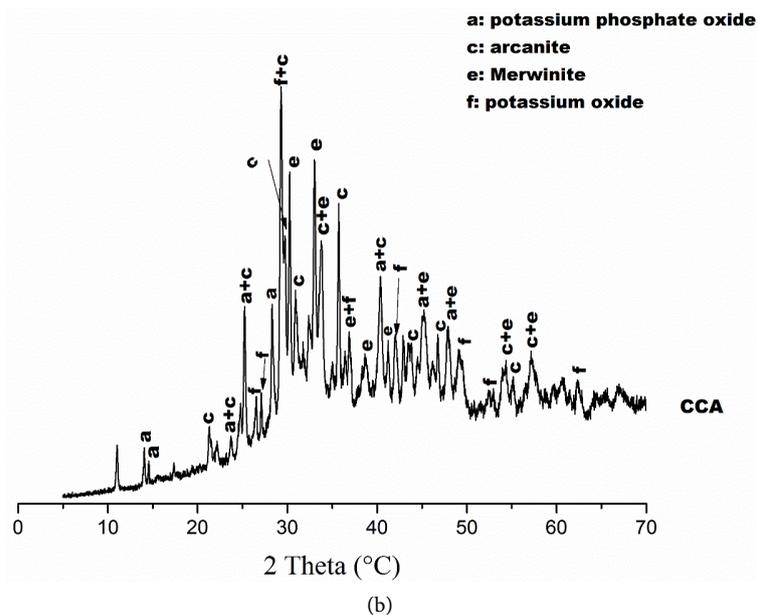
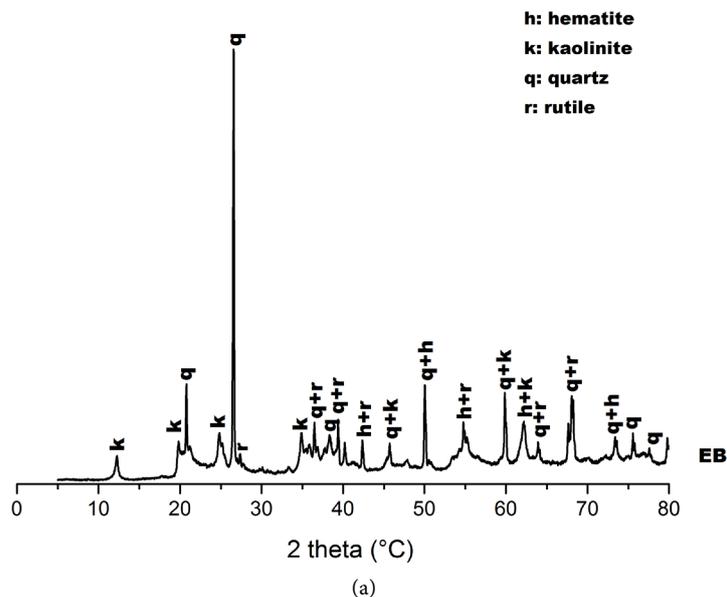


Figure 2. XRD patterns of EB and CCA.

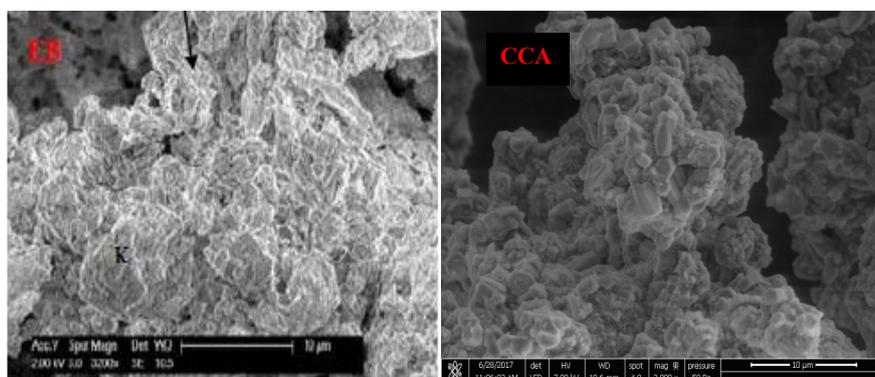


Figure 3. SEM micrographs of EB and CCA.

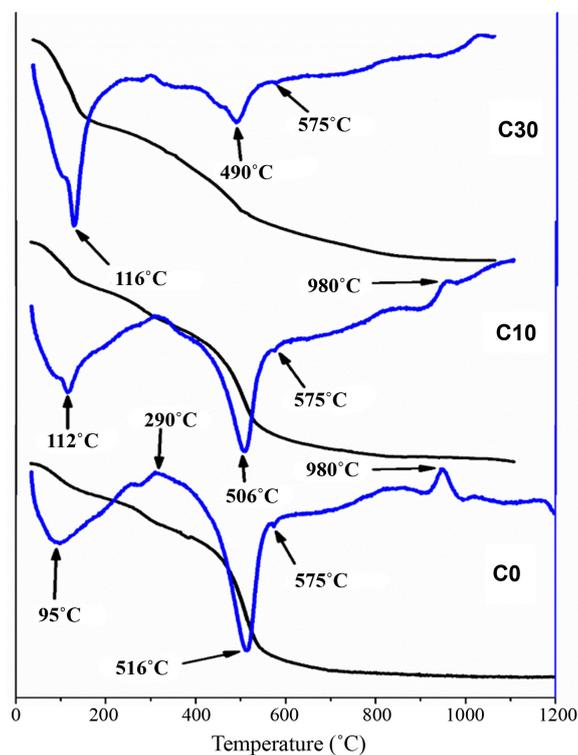


Figure 4. TGA and DSC curves of specimens C0 and C10 and C30.

into metakaolinite. With the increase of CCA amount (**Table 1**), the latter peak shifted to low temperatures. The weak endothermic peak at 575°C corresponds to the polymorphic transformation of quartz α to quartz- β [22] [23]. The exothermic peak related to the rearrangement of metakaolinite network around 980°C decreased with CCA increasing and it became hardly observable in the mixture C30 probably due to the interaction between metakaolinite and the secondary phase or to the diffusion of potassium contained in CCA [24] [25] [26] [27]. **Figure 5** shows the dilatometric behavior of C0 (EB) and C10. In each, or the other curve the first shrinkage between 575°C and 700°C corresponds to the dehydroxylation of kaolinite (**Figure 4**). This shrinkage appears earlier in C10 than C0 probably due to the K_2O content in CCA. The second shrinkage around 900°C - 975°C could correspond to the transformation of metakaolinite into either a spinel phase or mullite [28] [29]. At temperatures greater than 975°C, there is a great shrinkage which is the result of sintering that includes solid state diffusion and viscous flow mechanisms. It is likely that the consolidation of CCA containing sample is enhanced, and begins at a lower temperature in comparison to EB sample behavior.

3.2. Fired Products Characterization

3.2.1. Mineral Transformation and Micro Morphological Changes

Figure 6 & **Figure 7** show the X-ray patterns of samples fired at 1050°C and 1100°C respectively. Quartz, hematite, rutile and γ -alumina occurred in all fired samples. Mullite appeared from C10 to C30 at 1050°C and from C0 at 1100°C.

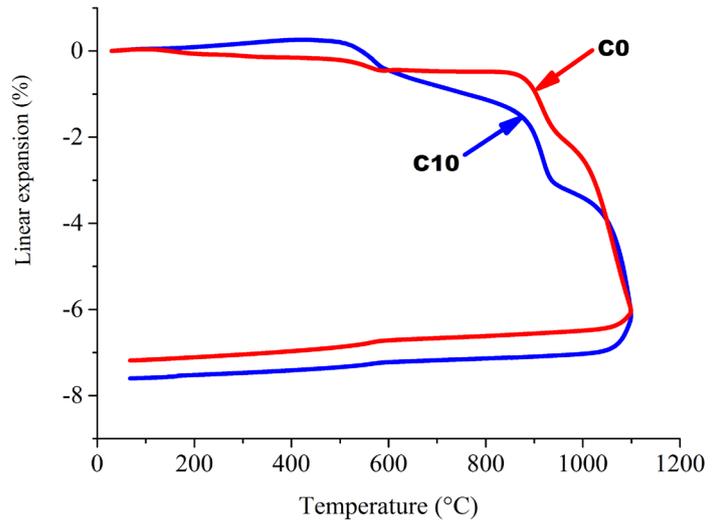


Figure 5. Dilatometric curves of specimens C0 and C10.

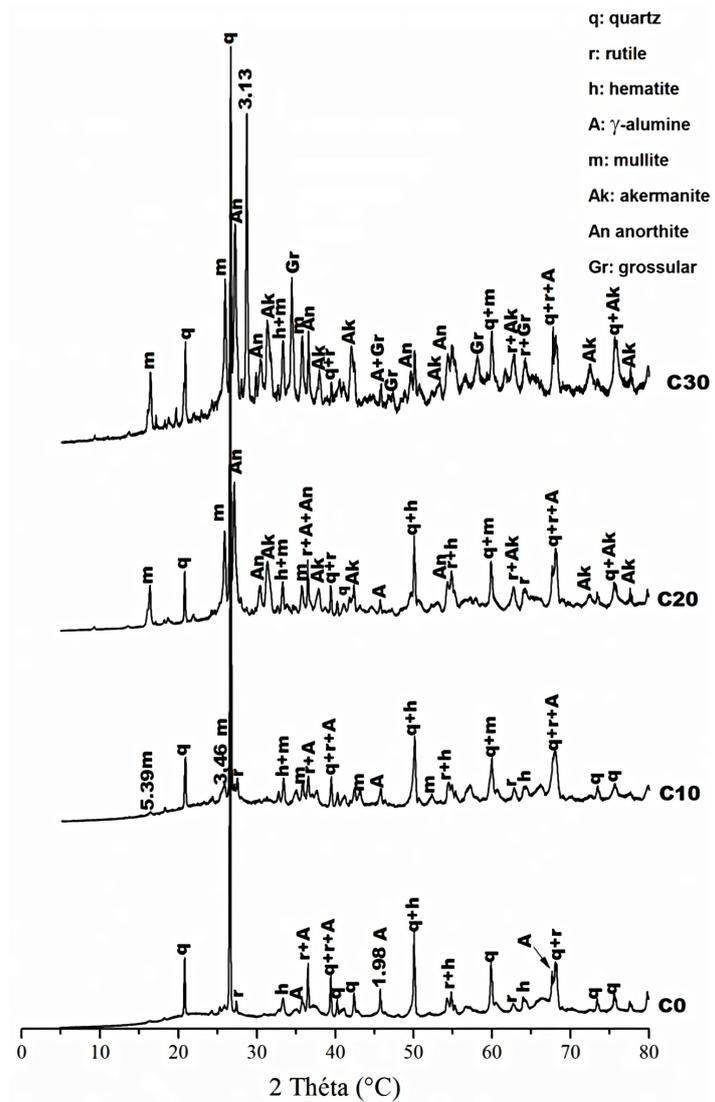


Figure 6. XRD patterns of specimens fired at 1050 °C.

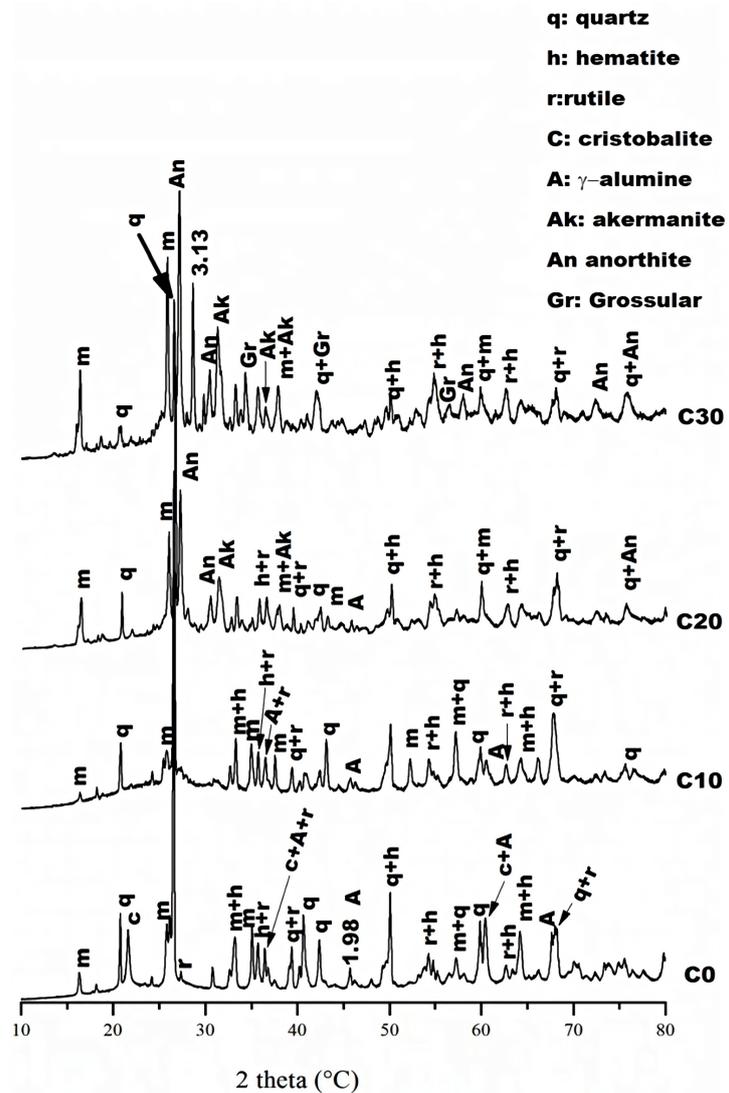
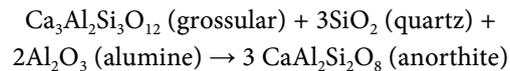


Figure 7. XRD patterns of specimens fired at 1100°C.

Cristobalite is observed only at 1100°C on C0 sample. The latter crystalline phase is absent in specimens C10 - C30 probably as a result of its dissolution in the increase glassy phase formed [30] [31]. Anorthite and akermanite are found in C20 and C30 fired mixtures. The γ -alumine phase observed results from the discharge of Al from clay minerals [32] [33]. Its main peak intensity (1.98 Å) diminishes with increasing amount of CCA in both temperatures, due to the decrease amount of clay minerals or its involvement to new minerals formation. The presence of CCA in the samples leads to the formation of mullite at lower temperature (Figure 6). Mullite main peaks intensities (5.39 Å and 3.46 Å) increase with increasing CCA content and temperature. The diffusion of potassium contained in CCA modifies structural reorganization process of metakaolinite. The exothermic peak around 980°C is strongly diminished (Figure 4) and leads to the mullite crystallization at lower temperatures [24]. Reaction of merwinite, quartz and sometimes aluminum silicates (clay minerals) give way to the forma-

tion of calcium and magnesium metastable phases, as grossular ($\text{Ca}_3\text{Al}_2\text{Si}_3\text{O}_{12}$) and akermanite ($\text{Ca}_2\text{MgSi}_2\text{O}_7$). Main peaks intensities of quartz (4.26 \AA , 3.34 \AA), γ -alumina (1.98 \AA), grossular (2.62 \AA) lessen when temperature and CCA increase respectively from 1050°C to 1100°C and from 20% to 30% by mass, while anorthite main peaks intensities (3.25 \AA , 2.92 \AA) increase. The formation of the latter mineral can be presented according to the following reaction:



SEM images and EDS spectra of the specimens C0, C10, C20 and C30 fired at 1100°C are given in **Figure 8**. All the micrographs show compact specimens except the one free from CCA (**Figure 8(a)**) which exhibits large pores as a result of absence of vitreous phase. The specimen C10 is more compact and denser than the specimens C20 and C30. Also, the glassy phase is well spread in C10

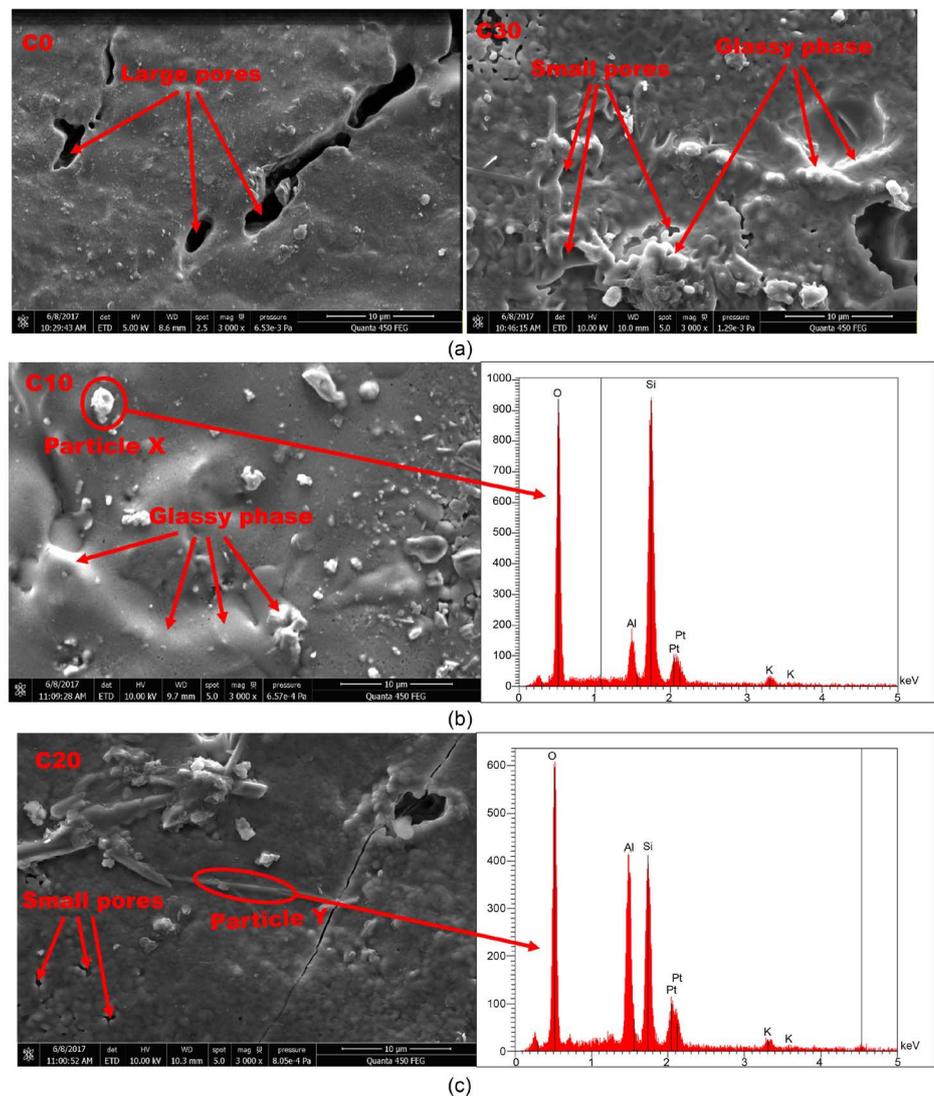


Figure 8. SEM micrographs and EDS spectra of specimens sintered at 1100°C ((a) = C0; (b) = C10; (c) = C20; (d) = C30).

than in C20 and C30, the latter specimens exhibiting pores, due probably to the organic origin of ash and/or emission of gas from thermal decomposition of arcanite (**Figure 2(b)**). Indeed, Vassileva *et al.* [34] showed that from 1100°C, there is a thermal decomposition of arcanite according to the reaction:



From EDS spectra, the main chemical elements observed in the “particle x” are silicon and oxygen (specimen C10) while in the “particle y” (specimens C20) there are aluminum, silicon and oxygen. The latter observations are in accordance with that of XRD (**Figure 6** and **Figure 7**) that showed in a major extent, the presence of quartz in C10 while both quartz and mullite are observed in C20 and C30. Also, the presence of the latter crystalline phase is highlighted by the presence of needles [35] in **Figure 8(c)**.

3.2.2. Physical and Mechanical Properties

The densification behavior of the fired bodies was evaluated via physical (firing shrinkage, apparent porosity and bulk density) and mechanical properties (flexural strength) as a function of CCA amount in specimens fired respectively at 1050°C and 1100°C. Firing shrinkage and bulk density firstly increased respectively till 8.5% and 2.41 g/cm³ for specimen with 10% mass of CCA, thereafter they lessen for specimens C20 and C30 (**Figure 9(a)** & **Figure 9(b)**). This drop results from the formation of increasing amount of anorthite. Indeed the sintered bodies' volume increase with anorthite formation [36] [37]. Also, specimens with 10% by mass of CCA (C10) leads to the decrease of water absorption (WA) up to 5% and 2% respectively at 1050°C and 1100°C. Conversely, WA increases for specimens with 20% or 30% by mass of CCA (**Figure 9(c)**). The decrease of WA in fired products is due to the sintering phenomenon. This sintering is favored by the formation of a glassy phase due to the fluxes from CCA. As far as, increasing amount of CCA, leads to the formation of abundant glassy phase in the fired products. However, the glassy phase is concomitantly accompanied by pores released from emission of gas (SO₃) induced by the thermal transformation of arcanite (K₂SO₄) which generates pores. Hence, fired specimens C20 and C30 contain both abundant glassy phase along with pores (**Figure 8**) which lead to concomitant increase of WA and decrease of bulk density (BD). The formation of anorthite (**Figure 6** & **Figure 7**) which increases the fired body's volume can also explained the decrease of BD for specimen C20 and C30 (**Figure 9(b)**). For one to another firing temperature (1050°C or 1100°C), there is increase of flexural strength for specimens C0. This is in accordance with **Figure 6** and **Figure 7** which show the formation of mullite only for the specimens fired at 1100°C. As for the fired specimens C10 - C30, there is an increase of flexural strength (σ) up to 32 MPa (**Figure 9(d)**) by addition of 10% by mass of CCA followed by a drop for specimens with great amount of additive. At 1100°C, Cocoa cortex ash (up to 10% by mass) lead to vitrified ceramics with better technological properties compare to other flux agents. For example, Elimbi *et al.* [38] used syenite and nepheline syenite as fluxing agent with kaolinitic

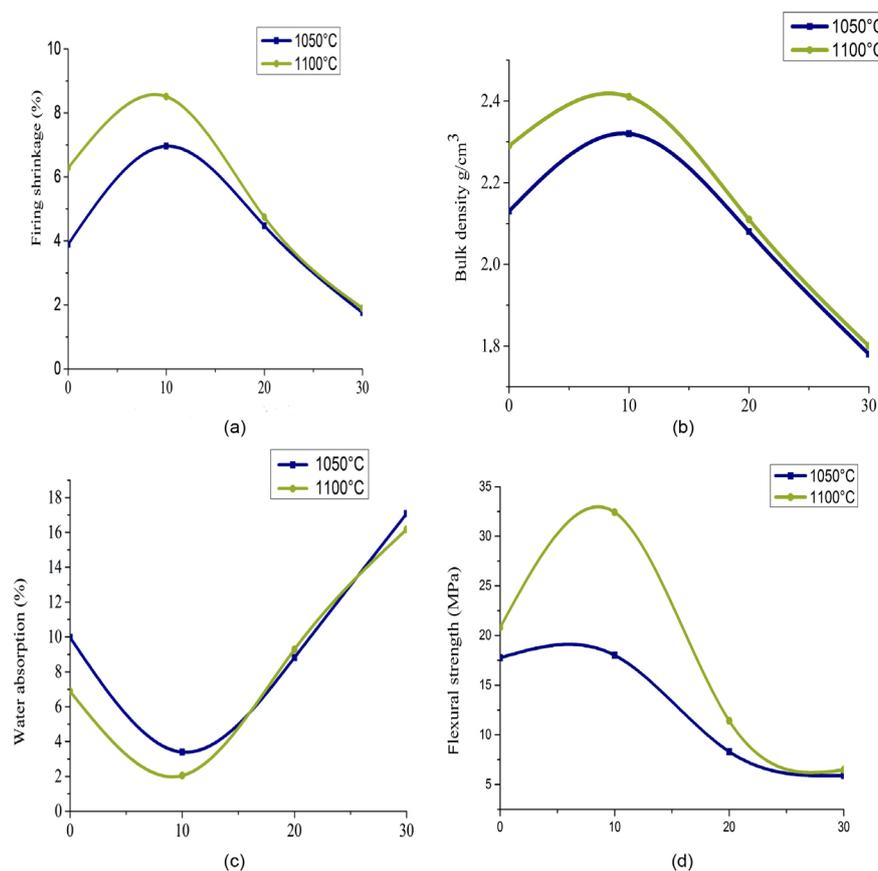


Figure 9. Physical and mechanical characteristics of fired bodies as a function of CCA mass percentage ((a) firing shrinkage; (b) bulk density; (c) water absorption; (d) flexural strength).

clay to manufacture vitrified ceramics. With the syenite and nepheline syenite content varied from 10% to 25% by mass and fired at 1100°C, flexural strength of the obtained products is less than 15 MPa; in the same way, Njindam *et al.* [12] with addition of 10% by mass of glass powder in kaolinitic clay, obtained specimens with a flexural strength of 12 MPa and 20 MPa respectively at 1100°C and 1200°C. In the micrograph of specimen C10, the product is compact contrarily to specimens C20 and C30 whose micrographs show pores (Figure 8). Hence, when fired at 1100°C, specimens with 10% by mass of CCA led to products that correspond to vitrified ceramics such as stoneware, according to the norm ISO 13006 [39].

4. Conclusion

The objective of this work was to manufacture vitrified ceramics using Cocoa Cortex Ash (CCA), as fluxes source, and a poor fluxes containing alluvial clay. The effect of cocoa cortex ash was investigated on mineralogy, microstructure as well as on technological properties of fired products obtained from its mixtures with the alluvial clay. Crystalline phases initially present in CCA disappeared in the fired bodies, due to their involvement in the vitrification and/or in the new

mineralization process. New crystalline phases formed are mullite, anorthite and grossular. γ -alumina phase was also formed due to release of Al from clay minerals. At 1100 °C, the specimens that were initially free from CCA contained cristobalite as a neo-formed crystalline phase but the latter was absent in the specimens which initially contained the additive, probably as a result of its dissolution in a vitreous phase. All the specimens fired at 1100 °C were compact but the one which was free from CCA exhibited large pores. When fired, the specimens that initially contained 10% by mass of CCA were more compact and exhibited low water absorption (2%), high density (2.41 g/cm³) and flexural strength (σ) of 32 MPa. Conversely, when fired, specimens that initially contained 20% or 30% by mass of CCA showed both abundant glassy phases along with pores which led to the increase of water absorption and decrease of both bulk density and flexural strength. The present research work pointed out that cocoa cortex ashes are effective source of fluxes for vitrified dense ceramics, such as stoneware, at dosage \leq 10% and at lowered temperature of 1100 °C.

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Conflicts of Interest

The authors declare no conflicts of interest regarding the publication of this paper.

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