

Low-Loss Co₂-Y Ferrites with Added CuO Sintered in Air for High Frequency Application

Shigeo Fujii, Koji Wakamatsu, Hiroshi Satoh, Setsuo Yamamoto

Department of Material Science and Engineering, University of Yamaguchi, Ube, Japan
Email: s502wd@yamaguchi-u.ac.jp

Received 7 September 2014; revised 16 October 2014; accepted 5 November 2014

Copyright © 2014 by authors and Scientific Research Publishing Inc.
This work is licensed under the Creative Commons Attribution International License (CC BY).
<http://creativecommons.org/licenses/by/4.0/>



Open Access

Abstract

The sintering characteristics of hexagonal Co₂-Y-type ferrite, Ba₂Co₂Fe₁₂O₂₂, with the addition of 0.6 wt% CuO, were studied in order to allow for preparation in air, as opposed to the conventionally recommended O₂, for industrial production. The dependence of the resistivity, ρ magnetic loss, $\tan\delta$, and the permeability, μ , at 1 GHz on the sintering temperature was investigated. A low $\tan\delta$ of 0.05 with a μ of 2.7 at a frequency of 1 GHz, along with a high ρ (up to $7 \times 10^4 \mu\Omega$), were attained under sintering at 1170°C in air, which were the same features as those of samples sintered at 1200°C in O₂. The dependence of $\tan\delta$ on grain diameter was also examined, and it was determined that a small grain size (less than 2 μm) is preferable for low $\tan\delta$.

Keywords

Ferrite, Hexagonal, Y-Type, Sintering, Low Loss

1. Introduction

Ferrites and other magnetic materials have been widely used as the key elements in microwave devices [1]-[3] such as isolators, phase shifters [4] [5], and circulators [6]. Traditional ferrites, known as spinel types, such as Ni-Zn ferrites have been known to exhibit high permeability in the frequency range up to a few hundred MHz because of restriction by Snoek's law [7] [8]. Therefore, hexagonal ferrites are expected to be promising candidates for expansion of the device frequency to the GHz range [9]. Z- and Y-type ferrites show soft magnetic characteristics with moderate relative permeability, μ , up to 1 GHz [10]-[12]. The former is denoted as Ba₃Me₂Fe₂₄O₄₁, while the latter is labeled Ba₂Me₂Fe₁₂O₂₂, where Me represents a divalent metal ion from the first transition series or, alternatively, it may represent Zn or Mg. In particular, the Y-type ferrite has a high Curie temperature

[11] and higher magnetic resonance than the Z-type, despite a low μ [13] [14]. Therefore, it is more applicable to high frequency devices in the GHz range.

Recently, telecommunication devices applied to mobile phones have broadened their market extensively. For these applications, antennas are essential, and miniaturization of these devices is therefore necessary. Ferrites possess permeability as well as permittivity, and are considered as a candidate material for chip antennas [15]-[19], because the wavelength is reduced proportionally according to $1/\sqrt{\mu\varepsilon}$ where ε is the relative permittivity. The Y-type ferrite, $\text{Ba}_2\text{Co}_2\text{Fe}_{12}\text{O}_{22}\text{Y}$ ($\text{Co}_2\text{-Y}$), with a high Curie temperature of $\sim 330^\circ\text{C}$ [11], is a promising material for this application.

We have demonstrate that $\text{Co}_2\text{-Y}$ modified by the addition of 0.6 wt% CuO exhibited a moderate μ of ~ 2.7 and low magnetic loss, $\tan\delta$, of 0.05, even at 1 GHz [20]. This material has been prepared by means of a conventional powder metallurgical process, and sintering has been conducted under the conventionally recommended oxygen atmosphere. However, sintering of the $\text{Co}_2\text{-Y}$ in air would be preferable for industrial production because of cost effectiveness. To date, some studies have been conducted on Y-type $\text{Ba}_2\text{Zn}_{2-2x-2y}\text{Co}_{2x}\text{Cu}_{2y}\text{Fe}_{12}\text{O}_{22}$ ($0 \leq x \leq 0.1$) sintering in air [14] [21]. In addition, $\text{Co}_2\text{-Y}$ (with no added CuO) sintering in air has also been reported [22], which showed a high resistivity of $5 \times 10^4 \Omega\text{m}$ but did not show values of $\tan\delta$. The industrially favorable sintering conditions (in air) of 0.6 wt% CuO added to $\text{Co}_2\text{-Y}$ will be presented in this study in order to attain the same characteristics as the samples sintered in O_2 in our early study mentioned above. The effective factor of $\tan\delta$ will also be discussed.

2. Experimental

Samples of $\text{Co}_2\text{-Y}$ ferrite were prepared as a stoichiometric composition by means of conventional powder metallurgy. Raw material powders of Fe_2O_3 , BaCO_3 , and Co_3O_4 were well-mixed using ball-milling and calcinated at 1000°C for 2 h in air. The calcinated powders were ground, with the addition of 0.6 wt% CuO powders and of a 1 wt% PVA binder, followed by compacting into predetermined shapes at a pressure of 20 MPa and then sintered at 1200°C for 3 h under atmospheres with varying oxygen content (balance: nitrogen).

The resistivity, ρ , was measured for samples whose dimensions were 13 mm in diameter and 3 mm in thickness. An electrode was then printed on both sides of the samples as a silver paste. The permeability and permittivity frequency response were characterized by means of a network analyzer (Agilent E8364A) and a coaxial airline fixture (KANTOH E.A.D. Co. Model: CSH2-APC-7) up to 18 GHz, after the Nicolson-Ross method [23]. Ring shaped samples (ID: 3.0 mm, OD: 7.0 mm, thickness: 3.5 mm) were used in this characterization.

The sample densities were determined by means of Archimedes' method, while their morphologies were investigated using a scanning electron microscope (SEM) (Hitachi S-800). The grain diameters were defined as the average diagonal length of approximately 30 grains, orienting the hexagonal shape towards the top, in the SEM images.

3. Results and Discussion

The $\text{Co}_2\text{-Y}$ samples with the added 0.6 wt% CuO were prepared in various O_2 volume configurations at a sintering temperature of 1200°C . The O_2 volume fraction varied from 15% - 100%. The dependence of μ , $\tan\delta$ at 1 GHz, the density, and ρ , on the O_2 volume fraction are shown in **Figure 1(a)** and **Figure 1(b)**, respectively. Both μ and $\tan\delta$ decrease with increasing O_2 volume fraction. The lowest $\tan\delta$ (at 0.05) with a μ of 2.7 was achieved at a full O_2 atmosphere (100%), while the atmospheric case, *i.e.*, sintering in air (20% O_2), exhibited a high $\tan\delta$ of 0.15 along with a high μ of ~ 4 . It can be seen that the density increases while ρ decreases with decreasing O_2 volume fraction. A high density of $5.24 \times 10^3 \text{ kg/m}^3$ and a low ρ of $1.2 \times 10^4 \Omega\text{m}$ were achieved in air. Low $\tan\delta$ is required for energy-conversion devices such as inductors and antennas. High ρ is also required, because winding coils or printed electrodes make contact with ferrites directly. These characteristics were not attained when sintering at 1200°C conducted in air, as shown in **Figure 1**. Therefore, the sintering temperature in air must be considered.

The dependence of ρ on the sintering temperature in O_2 and in air is shown in **Figure 2**, where open and black circles denote sintering in O_2 and in air, respectively. ρ decreases with sintering temperature for both atmospheres, although the change in air is steeper than that in O_2 . A resistivity greater than $7 \times 10^4 \Omega\text{m}$ in the case of sintering in O_2 is reached below 1180°C in air.

The change in μ and $\tan\delta$ at 1 GHz due to sintering temperature in O_2 and in air are shown in **Figure 3(a)** and

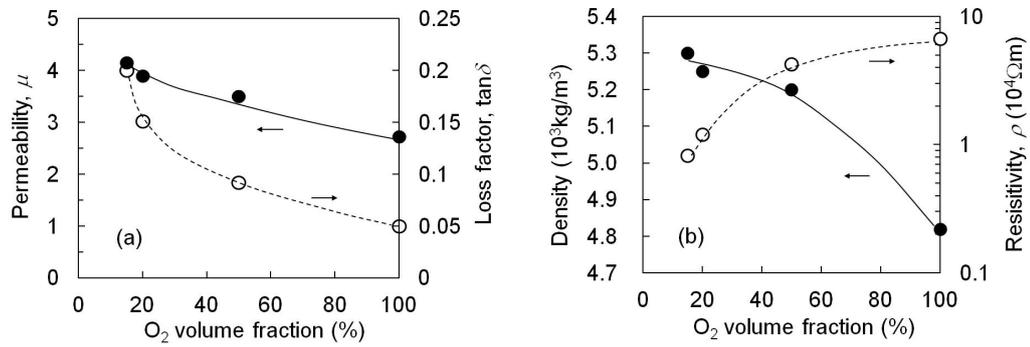


Figure 1. Dependence of (a) μ and $\tan\delta$, and (b) density and ρ , on O₂ volume fraction at sintering.

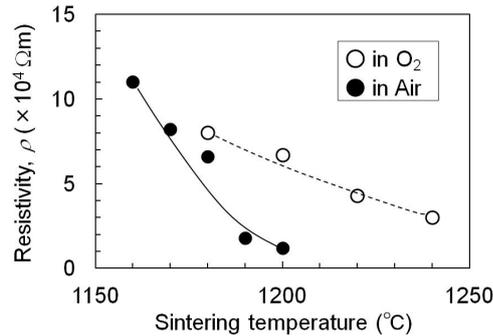


Figure 2. Dependence of ρ on sintering temperature in O₂ and in air.

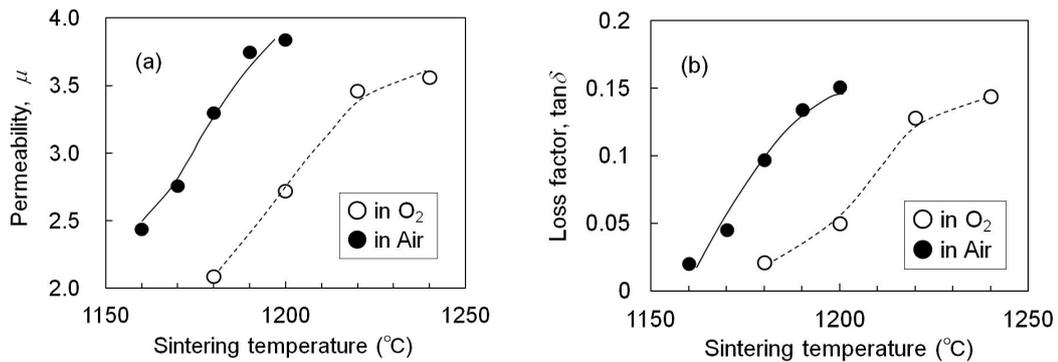


Figure 3. Change in (a) μ and (b) $\tan\delta$ at 1 GHz due to sintering temperature in O₂ and in air.

Figure 3(b), respectively. μ and $\tan\delta$ increase with sintering temperature for both atmospheres, and the behavior in the air case are shifted to a lower temperature than that of the O₂ case. The target characteristics, namely, μ of 2.8 with a low $\tan\delta$ (less than 0.05 at 1 GHz), are attained at 1170 °C in the case of sintering in air, which is almost identical to the sample sintered at 1200 °C in O₂. It was proven that the crystal structure of this sample was that of a Co₂-Y ferrite using X-ray diffraction as shown in Figure 4, where no spinel phase was detected as in [21].

The fractured surfaces of the samples with identical characteristics and sintered in different atmospheres are shown in Figure 5. Here, Figure 5(a) is an image of a sample sintered at 1200 °C in O₂, while Figure 5(b) shows a sample sintered at 1170 °C in air. The density of the former is $4.82 \times 10^3 \text{ kg/m}^3$ and that of the latter is $4.90 \times 10^3 \text{ kg/m}^3$, respectively. Both samples have the same morphological aspect with small grains isolated by fine pores. In addition, the majority of the grains have a pseudo-hexagonal platelet shape with thin thickness. The grain sizes, defined as the diagonal length of the hexagonal faces, are estimated as being 2.0 μm in the O₂ case and 1.8 μm for the air case from these images. It is assumed that the same magnetic characteristics are attributed to the same morphological nature in both samples.

The relationship between grain diameter and $\tan\delta$ is shown in **Figure 6**. All samples fabricated in this study are plotted on this figure regardless of sintering conditions. The value of $\tan\delta$ increases with grain diameter, and rises abruptly from 0.05 to 0.15 around a grain diameter of $\sim 2 \mu\text{m}$. It has been reported previously that energy dissipation in inductors composed of NiZn ferrites is affected by grain size, and that the dissipation was minimized at a single domain size of 2 - 3 μm [24]. The magnetization process is classified into a spin rotational mode or a magnetic domain wall motion depending on magnetic domain sizes. The rotational mode dominates in the case of small grain diameters equal to magnetic single domain sizes, while larger grain sizes lead to two- or multi-domain structures.

The abrupt increase in $\tan\delta$ by more than 0.1 beyond a diameter of 2 μm could be attributed to the switching of the magnetization mode from the spin rotational mode to the magnetic domain wall motion. The critical size of a magnetic single domain could be estimated as being approximately 2 μm in the $\text{Co}_2\text{-Y}$ ferrite. Therefore, controlling the grain size has an effect on reducing $\tan\delta$.

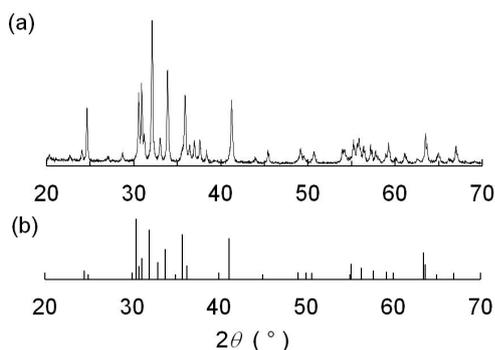


Figure 4. X-ray diffraction profiles of (a) the sample sintering at 1700°C in air, and (b) calculated standard Y-type ($\text{CuK}\alpha$, $\lambda = 0.15405 \text{ nm}$).

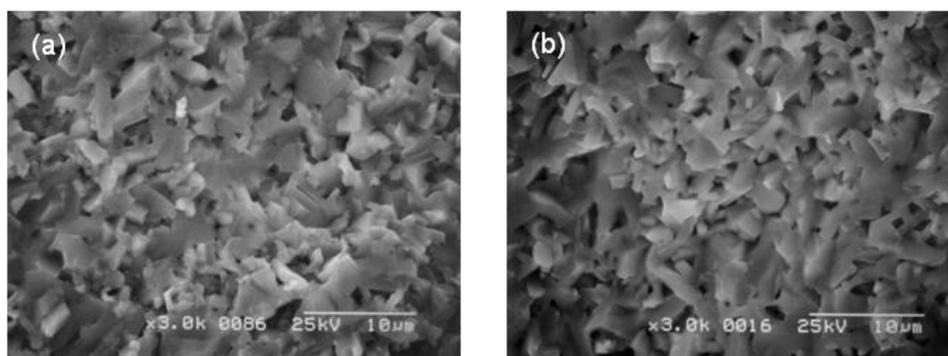


Figure 5. Fractured surface of the samples sintered at (a) 1200°C in O_2 and (b) 1700°C in air. Grain sizes were estimated as being $\sim 2.0 \mu\text{m}$ and $\sim 1.8 \mu\text{m}$, respectively.

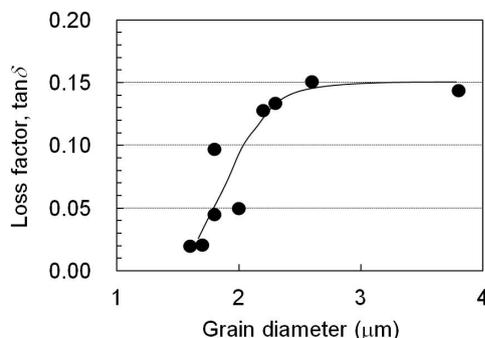


Figure 6. The relationship between grain diameter and $\tan\delta$.

It is apparent that the Co₂-Y ferrite with low $\tan\delta$ even at 1 GHz fabricated in air is favorable for industrial production, and is a promising magnetic material for application to high frequency devices.

4. Conclusion

The sintering characteristics of the hexagonal Co₂-Y-type ferrite, Ba₂Co₂Fe₁₂O₂₂, with the addition of 0.6 wt% CuO in air were examined in order to apply the ferrite to industrial production. It was found that sintering at 1170°C in air resulted in a low $\tan\delta$ of 0.05, with a high μ of 2.7 at 1 GHz and a high ρ of $7 \times 10^4 \mu\text{m}$, identical to a sample sintered at 1200°C in the conventionally recommended oxygen atmosphere. The relationship between grain size and $\tan\delta$ was also examined. It was found that $\tan\delta$ was dependent on grain size, and that a size of less than 2 μm is preferable for reducing $\tan\delta$, which suggests the ferrite can be applied to microwave devices with low energy dissipation.

References

- [1] Pardavi-Horvath, M. (2001) Microwave Applications of Soft Ferrite. *Journal of Magnetism and Magnetic Materials*, **215-216**, 171-183. [http://dx.doi.org/10.1016/S0304-8853\(00\)00106-2](http://dx.doi.org/10.1016/S0304-8853(00)00106-2)
- [2] Harris, V.G., Geiler, A., Chen, Y., Yoon, S. D., Wu, M., Yang, A., Chen, Z., He, P., Parimi, P. V., Zuo, X., Patton, C. E., Abe, M., Acher, O. and Vittoria, C. (2009) Recent Advances in Processing and Applications of Microwave Ferrites. *Journal of Magnetism and Magnetic Materials*, **321**, 2035-2047. <http://dx.doi.org/10.1016/j.jmmm.2009.01.004>
- [3] Harris, V.G. (2012) Modern Microwave Ferrites. *IEEE Transactions on Magnetics*, **48**, 1075-1104. <http://dx.doi.org/10.1109/TMAG.2011.2180732>
- [4] Zuo, X., How, H., Shi, P., Oliver, S.A. and Vittoria, C. (2001) Development of High Frequency Ferrite Phase-Shifter. *IEEE Transactions on Magnetics*, **37**, 2395-2397. <http://dx.doi.org/10.1109/20.951183>
- [5] Wang, J.W., Geiler, A.L., Harris, V.G. and Vittoria, C. (2010) Numerical Simulation of Wave Propagation in Y- and Z-Type Hexaferrites for High Frequency Applications. *Journal of Applied Physics*, **107**, Article ID: 09A515.
- [6] Singh, P., Babbar, V.K., Razdan, A., Srivastava, S.L. and Puri, R.K. (1999) Complex Permeability and Permittivity, and Microwave Absorption Studies of Ca(CoTi)_xFe_{12-2x}O₁₉ Hexaferrite Composites in X-band Microwave Frequencies. *Materials Science and Engineering: B*, **B67**, 132-138. [http://dx.doi.org/10.1016/S0921-5107\(99\)00328-1](http://dx.doi.org/10.1016/S0921-5107(99)00328-1)
- [7] Snoek, L.L. (1948) Dispersion and Absorption in Magnetic Ferrites at Frequencies above One Mc/s. *Physica*, **14**, 207-217. [http://dx.doi.org/10.1016/0031-8914\(48\)90038-X](http://dx.doi.org/10.1016/0031-8914(48)90038-X)
- [8] Nakamura, T. (2000) Snoek's Limit in High-Frequency Permeability of Polycrystalline Ni-Zn, Mg-Zn, and Ni-Cu-Zn Spinel Ferrites. *Journal of Applied Physics*, **88**, 348-353. <http://dx.doi.org/10.1063/1.373666>
- [9] Nakamura, T. and Hatakeyama, K. (2000) Complex Permeability of Polycrystalline Hexagonal Ferrites. *IEEE Transactions on Magnetics*, **36**, 3415-3417. <http://dx.doi.org/10.1109/20.908844>
- [10] Obol, M. and Vittoria, C. (2003) Measurement of Permeability of Oriented Y-Type Hexaferrites. *Journal of Magnetism and Magnetic Materials*, **265**, 290-295. [http://dx.doi.org/10.1016/S0304-8853\(03\)00277-4](http://dx.doi.org/10.1016/S0304-8853(03)00277-4)
- [11] Lee, S.G. and Kwon, S.J. (1996) Saturation Magnetizations and Curie Temperatures of Co-Zn Y-Type Ferrites. *Journal of Magnetism and Magnetic Materials*, **153**, 279-284. [http://dx.doi.org/10.1016/0304-8853\(95\)00559-5](http://dx.doi.org/10.1016/0304-8853(95)00559-5)
- [12] How, H., Zuo, X. and Vittoria, C. (2005) Wave Propagation in Ferrite Involving Planar Anisotropy—Theory and Experiment. *IEEE Transactions on Magnetics*, **41**, 2349-2354. <http://dx.doi.org/10.1109/TMAG.2005.852954>
- [13] Obol, M. and Vittoria, C. (2003) Microwave Permeability of Y-Type Hexaferrites in Zero Field. *Journal of Applied Physics*, **94**, 4013-4017. <http://dx.doi.org/10.1063/1.1601291>
- [14] Bai, Y., Zhou, J., Gui, Z., Yue, Z. and Li, L. (2003) Complex Y-Type Hexagonal Ferrites: An Ideal Material for High-Frequency Chip Magnetic Components. *Journal of Magnetism and Magnetic Materials*, **264**, 44-49. [http://dx.doi.org/10.1016/S0304-8853\(03\)00134-3](http://dx.doi.org/10.1016/S0304-8853(03)00134-3)
- [15] Hansen, R.C. and Burke, M. (2000) Antennas with Magneto-Dielectrics. *Microwave and Optical Technology Letters*, **26**, 75-78. [http://dx.doi.org/10.1002/1098-2760\(20000720\)26:2<75::AID-MOP3>3.0.CO;2-W](http://dx.doi.org/10.1002/1098-2760(20000720)26:2<75::AID-MOP3>3.0.CO;2-W)
- [16] Kong, L.B., Li, Z.W., Lin, G.Q. and Gan, Y.B. (2007) Ni-Zn Ferrite Composite with Almost Equal Values of Permeability and Permittivity for Low-Frequency Antenna Design. *IEEE Transactions on Magnetics*, **43**, 6-10. <http://dx.doi.org/10.1109/TMAG.2006.886321>
- [17] Kim, I., Bae, S. and Kim, J. (2008) Effect of Ferrite Substrates on Antenna Miniaturization. *Journal of Korean Physical Society*, **52**, 127-131. <http://dx.doi.org/10.3938/jkps.52.127>
- [18] Bae, S., Hong, Y.K. and Lyle, A. (2008) Effect of Ni-Zn Ferrite on Bandwidth and Radiation Efficiency of Embedded

Antenna for Mobile Phone. *Journal of Applied Physics*, **103**, Article ID: 07E929.

- [19] Liew, X.T., Chan, K.C. and Kong, L.B. (2009) Magnetodielectric Ni Ferrite Ceramics with Bi₂O₃ Additive for Potential Antenna Miniaturizations. *Journal of Materials Research*, **24**, 324-332. <http://dx.doi.org/10.1557/JMR.2009.0057>
- [20] Now submitting to *Journal of Magnetism and Magnetic Materials*.
- [21] Bai, Y., Zhou, J., Gui, Z.L. and Li, L.T. (2004) Frequency Dispersion of Complex Permeability of Y-Type Hexagonal Ferrites. *Materials Letters*, **58**, 1602-1606. <http://dx.doi.org/10.1016/j.matlet.2003.09.049>
- [22] Bai, Y., Zhou, J., Gui, Z.L. and Li, L.T. (2002) An Investigation of the Magnetic Properties of Co₂Y Hexaferrite. *Materials Letters*, **57**, 807-811. [http://dx.doi.org/10.1016/S0167-577X\(02\)00877-7](http://dx.doi.org/10.1016/S0167-577X(02)00877-7)
- [23] Nicolson, A.M. and Ross, G.F. (1970) Measurement of the Intrinsic Properties of Materials by Time Domain Techniques. *IEEE Transactions on Instrumentation and Measurement*, **19**, 377-382. <http://dx.doi.org/10.1109/TIM.1970.4313932>
- [24] van der Zaag, P.J., van der Valk, P.J. and Rekveldt, M.Th. (1966) A Domain Size Effect in the Magnetic Hysteresis of NiZn-Ferrites. *Applied Physics Letters*, **69**, 2927-2929. <http://dx.doi.org/10.1063/1.117326>

Scientific Research Publishing (SCIRP) is one of the largest Open Access journal publishers. It is currently publishing more than 200 open access, online, peer-reviewed journals covering a wide range of academic disciplines. SCIRP serves the worldwide academic communities and contributes to the progress and application of science with its publication.

Other selected journals from SCIRP are listed as below. Submit your manuscript to us via either submit@scirp.org or [Online Submission Portal](#).

