

# Experimental Investigation of Surface Plasmon Resonance Using Tapered Cylindrical Light Guides with Metal-Dielectric Interface

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## ABSTRACT

In this paper we report an experimental investigation on the observation of surface plasmon resonance at the metal-dielectric interface of silver coated tapered light guiding glass rods of different dimensions. Chemical deposition technique has been used for metallic deposition of silver on the Tapered glass rod. Angular interrogation in Kretschmann-like configuration of this non-planar (cylindrical) structure is used to locate the resonance dip in the reflectance measurement. Fabrication simplicity, in addition to the inherent advantage of using different types of tapered structures, makes this study important in the development of nanoplasmonics. The experimental study is accompanied by some interesting results.

**Keywords:** Glass Waveguides; Thin Films; Plasmonics; Surface Plasmons

## 1. Introduction

The Surface plasmon resonance (SPR) phenomenon is one of the most useful areas of research in the field of Nanotechnology/Nanophotonics. Surface plasmons are the collective charge oscillations at metal-dielectric interface [1]. Surface plasmon resonance phenomena has lots of applications in medicine, Nanobiotechnology, environmental monitoring etc [2]. The earlier studies relating to SPR phenomenon employed either Kretschmann [3] or Otto configuration [4]. Surface plasmon resonance phenomenon is an important tool used for developing sensors. The first SPR sensor was developed for gas detection and biosensing [5,6]. Many researchers have reported their work on SPR-based fiber optic sensor [7-13].

Almost all the methodology used in above literature involve sophisticated instrumentation as far as fabrication of the actual nano-thickness multilayered structure is concerned. In most of the methods complex planar structures are used, which are though simpler to analyze mathematically but need a high level of accuracy in fabrication and measurements. Earlier, Ray *et al.* have published the SPR based theoretical [14-16] as well as experimental work [17,18] where main focus was on the development of novel methodology as well as reduction of complexity in the structure.

In the present work we have investigated surface plasmon resonance phenomenon experimentally using two

different kind of tapered glass rods made of fused silica material. A thin layer of silver having thickness of the order of 50 nm has been chemically deposited over a specified length of the external surface of these rods. Effect of varying the sensing length has also been investigated.

## 2. Theory

### 2.1. Basic Theory of Surface Plasmon Resonance

The excitation of surface plasmons at metal/dielectric interface results in the transfer of energy from incident light to surface plasmons, which reduces the intensity of the reflected light. Surface plasmons are coherent electron oscillations at the interface between any two materials (like metal/dielectric) where real part of dielectric function changes sign across the interface. A medium of large negative dielectric constant is a good selection to observe surface plasmon resonance phenomenon. As a result, most noble metals such as aluminium, gold and silver can exhibit resonant absorption by surface plasmon excitation. When a p-polarized light beam (having direction of vibration parallel to the plane of incidence) is incident from a light coupling device like glass/epoxy to a noble metal having large negative dielectric constant and as light is going from a higher refractive index medium (glass/epoxy) to a lower refractive index medium

(metal), an evanescent wave is created at the glass-metal interface due to the slight penetration of the incoming light wave into the metal layer having thickness of the order of nanometer. As a result, there will be energy coupling between evanescent wave and surface plasmon wave at the glass-metal interface. These surface plasmon waves are created due to surface electrons on the glass metal interface. When the wave vector of the evanescent wave ( $k_{ev}$ ) and surface plasmon wave ( $k_{SP}$ ) matches then entire amount of evanescent wave energy is transferred to the surface plasmon wave and due to resonance the reflected light intensity from the output beam will be minimized. Now the phase matching condition needed for surface plasmon resonance is given by [3]

$$(k_{ev}) = (k_{SP}) \quad (1)$$

where

$$k_{ev} = \frac{\omega}{c} \sqrt{\varepsilon_p} \sin \theta \quad (2)$$

$$k_{SP} = \frac{\omega}{c} \left( \frac{\varepsilon_m \varepsilon_s}{\varepsilon_m + \varepsilon_s} \right)^{1/2} \quad (3)$$

where  $\varepsilon_p$  represents the dielectric constant of the material of the coupling device like (glass/epoxy),  $\varepsilon_m$  represents the dielectric constant of the metal layer,  $\varepsilon_s$  represents dielectric constant of the sensing layer,  $\theta$  is the angle of incidence of the beam,  $\omega$  is the frequency of the incident light beam and  $c$  is the velocity of light.

The excitation of surface plasmons occurs when the wave vector of evanescent wave exactly matches with that of surface plasmons of similar frequency. This occurs at a particular angle of incidence  $\theta_{res}$ , which is known as SPR angle. Thus the resonance condition for surface plasmon resonance is given by

$$\frac{\omega}{c} \sqrt{\varepsilon_p} \sin \theta_{res} = \frac{\omega}{c} \left( \frac{\varepsilon_m \varepsilon_s}{\varepsilon_m + \varepsilon_s} \right)^{1/2} \quad (4)$$

## 2.2. Reflectance for a 3-Layer Kretschmann Configuration

Fresnel reflection formulae for 3-layer model of conventional Kretschmann configuration of the prism (subscript-pr)/metal (subscript-1)/air (subscript-2) system can be summarized as follows. These formulae have been generally used for theoretical simulation of planar geometry and we have made necessary modifications for the non-planar structures under consideration.

The reflectance  $R$ , for p-polarization is given by

$$R = |r_{pr12}^p|^2 = \left| \frac{(r_{pr1}^p + r_{12}^p \exp(2ikz_1 d_1))}{(1 + r_{pr1}^p r_{12}^p \exp(2ikz_1 d_1))} \right|^2 \quad (5)$$

where

$$r_{ik}^p = \frac{(n_k \cos \theta_i - n_i \cos \theta_k)}{(n_k \cos \theta_i + n_i \cos \theta_k)} \quad (6)$$

$$r_{12}^p = \frac{\left[ \left( \sqrt{\varepsilon_1 - n_{pr}^2 \sin^2 \theta_{pr} / \varepsilon_1} \right) - \left( \sqrt{n_2^2 - n_{pr}^2 \sin^2 \theta_{pr} / n_2^2} \right) \right]}{\left[ \left( \sqrt{\varepsilon_1 - n_{pr}^2 \sin^2 \theta_{pr} / \varepsilon_1} \right) + \left( \sqrt{n_2^2 - n_{pr}^2 \sin^2 \theta_{pr} / n_2^2} \right) \right]} \quad (7)$$

$$\text{phase factor} = kz_1 d_1 = k_1 d_1 \cos \theta_1$$

$$= \left( \frac{2\pi}{\lambda} \right) d_1 \left( \sqrt{\varepsilon_1 - n_{pr}^2 \sin^2 \theta_{pr}} \right) \quad (8)$$

## 2.3. Mathematical Formulation for Taper Light Guide

**Figure 1** depicts the typical ray path within a taper light guide under attenuated total internal reflection (ATIR) mode. For linear tapering,  $\rho(z)$  is the taper radius at a distance “ $z$ ” from input end of the taper. Angle of incidence  $\theta_i$  of the ray at input end of the taper will be transformed into incident angle  $\varphi(z)$  at the taper sensing region located at a distance  $z$  from the input end.

If  $n_{air}$  is the refractive index of air and  $n_g$  is the refractive index of the taper light guide material (*i.e.* glass), then using Snell’s law,

$$n_{air} \sin \theta_i = n_g \sin \theta_r \quad (9)$$

$\theta_i$  is the angle of incidence controlled by the rotating table. By knowing  $\theta_i$  and using Equation (9), we can determine the value of  $\theta_r$ . Assuming  $\theta = (90 - \theta_r)$ , the angle  $\varphi(z)$  can be calculated as

$$\varphi(z) = \cos^{-1} \left[ \frac{\rho_i \cos \theta}{\rho(z)} \right] - \tan^{-1} \left( \frac{\rho_i - \rho_o}{L} \right) \quad (10)$$

where

$$\rho(z) = \rho_i - \frac{z}{L} (\rho_i - \rho_o). \quad (11)$$

And  $\tan^{-1} \left( \frac{\rho_i - \rho_o}{L} \right) = \Omega$  represents the taper angle.  $\theta_r$  is the angle of refraction at the input end,  $\rho_i$  and  $\rho_o$  denote the radii at input and output end of the taper respectively and  $L$  is the length of the taper [10]. As depicted schematically in **Figure 1**, we can easily visualize that as the light propagates through the tapered glass rod, the angle of incidence decreases along the glass-air interface of taper outer surface where there is no coating. It is to be noted that when the light beam reaches the sensing area, SPR occurs only at the first reflection on the glass-metal interface of the tapered glass rod provided the phase matching condition of Equation (1) is satisfied.

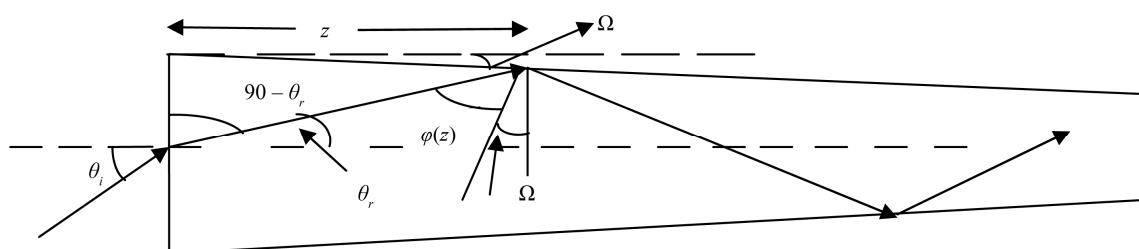


Figure 1. Taper structure used as the light coupling device for SPR sensing.

Consequently, for other successive reflection of the glass-metal interface finally result in the decrease of light intensity measured at the exit end face of the tapered glass rod and one will get the minimum intensity in the output beam. Here the output beam power is measured at the exit end of the taper, which is further normalized by the highest value of the power measured at the output end. As normalized reflectance value at the glass-metal interface is directly proportional to this, we have plotted our results in terms of reflectance vs. angle of incidence.

### 3. Sample Preparation

As shown in **Figure 2** and **Figure 3**, two types of tapers are used for our experimental purpose and corresponding specifications are as shown in **Table 1**. Main purpose of using different sensing layer length and location is to investigate their effect on the observed SPR. Sensing region is located at 3 cm from larger diameter and 1.3 cm from the smaller diameter for Taper-1 whereas it is located at 3.9 cm from larger diameter and 2.4 cm from the smaller diameter for Taper-2.

#### 3.1. Deposition of Silver Film Using Chemical Deposition Technique

Chemical deposition technique that we have used for the purpose of coating is described in the self-explanatory **Figure 4**. It is to be noted that before all the samples are dipped in this mixture of stock solution A and B, the samples are dipped in 5%  $\text{SnCl}_2$  solution prepared with 2.5 gm  $\text{SnCl}_2$  and 50 cc distilled water. Here  $\text{Sn}^{2+}$  ion act as binding agent for deposited  $\text{Ag}^{2+}$  ion on the samples. Moreover, by controlling the time of deposition we can control the thickness of the deposited silver film over the samples. Here the time of deposition within the solution is of the order of 120 seconds for both Taper-1 and Taper-2. For this time of deposition the thickness of coated silver film was found to vary within the range of 35 nm to 38.3 nm [19]. For simulation of Fresnel's reflection equation with non-planar structures using Equation (10) and Equation (11) it was found that thickness of the silver film of the order of 35 nm is necessary to obtain surface plasmon resonance with non-planar structures for the Attenuated Total Internal reflection (ATIR) at a particular



Figure 2. Taper-1.



Figure 3. Taper-2.

Table 1. Specifications of two tapers.

Sample	Length	Sensing region length	Entrance diameter	Exit diameter
Taper-1	8.2 cm	3.9 cm	3.0 mm	2.0 mm
Taper-2	7.9 cm	1.6 cm	3.0 mm	2.0 mm

location within the taper. Finally all the samples are dipped in distilled water for 30 minutes and then dried to ensure that the surface is free from any water mark.

#### 3.2. Protection of the Silver Coating from Oxidation

Though silver is a good candidate for observation of SPR, it is prone to oxidation. In order to protect the deposited silver film from getting oxidized, a mixture of 2/3 part 99% pure tetra ethyl orthosilicate  $[\text{Si}(\text{OC}_2\text{H}_5)_4]$  and 1/3 part ethyl alcohol  $[\text{C}_2\text{H}_5\text{OH}]$  can be used. When the samples are dipped in this mixture for a short duration and heated to  $250^\circ\text{C}$  in vacuum oven, a thin layer of  $\text{SiO}_2$  so created will protect the silver film from oxidation. It is to be noted that samples should be dipped within the solution for 1 sec only in order to ensure the thickness of the  $\text{SiO}_2$  protective layer of the order of 1 nm to 5 nm.



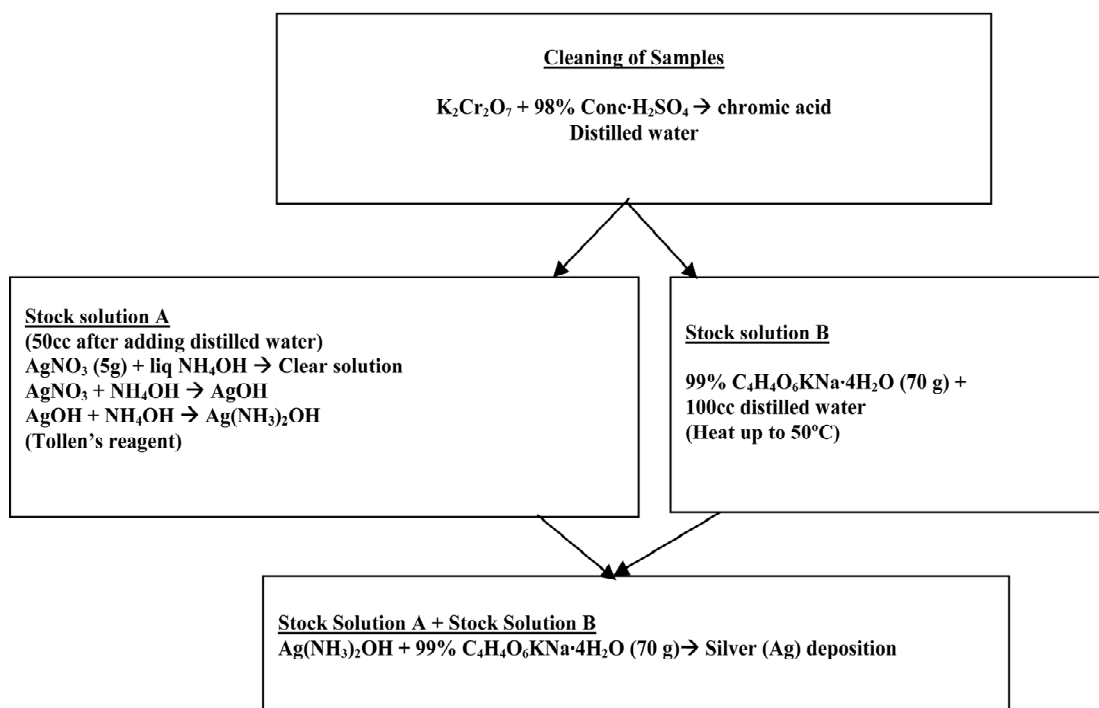


Figure 4. Chemical silver deposition process.

#### 4. Experimental Arrangement

Our basic experimental set-up for the angular interrogation reflectance measurement is shown in **Figures 5(a)** and **(b)**. The He-Ne laser is used as the source of electromagnetic radiation to excite the plasmon. A polarizer is used to make the input beam p-polarized so that its direction of vibration becomes parallel to the plane of incidence to excite the surface electrons of the metal. Angle of interrogation mode is realized by placing the experimental samples on the rotating table in such a manner so as to coincide the input end of the tapered rod with the rotating axis of this table. The output beam from the tapered rod is detected by a photo detector and measured by a power meter.

#### Detail Specification of Experimental Components Used

Laser source: Melles Griot, 5 mw at 632.8 nm. Class 3R laser product IEC.

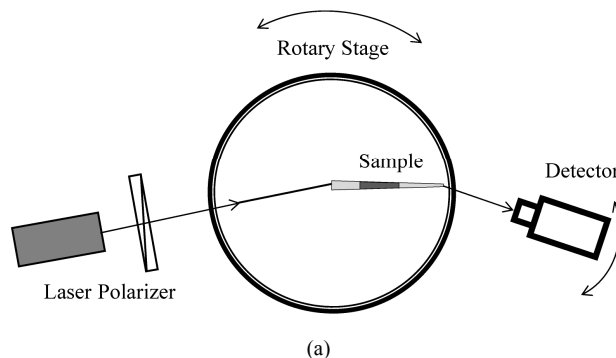
Polarizer: Yolux, India make, sheet polarizer.

Rotating table: Newport rotating table.

Photo detector: PIN photo detector, Sensor oriel Detection system Model 7072, SER NO 412, ORIEL CORPORATION, STANFORD, CONN-06902. I/P, 110 volts, frequency = 50/60 Hz, Current = 0.5 amp.

#### 5. Results and Discussions

For Taper-1, from the **Figure 1** it can be shown that as



(b)

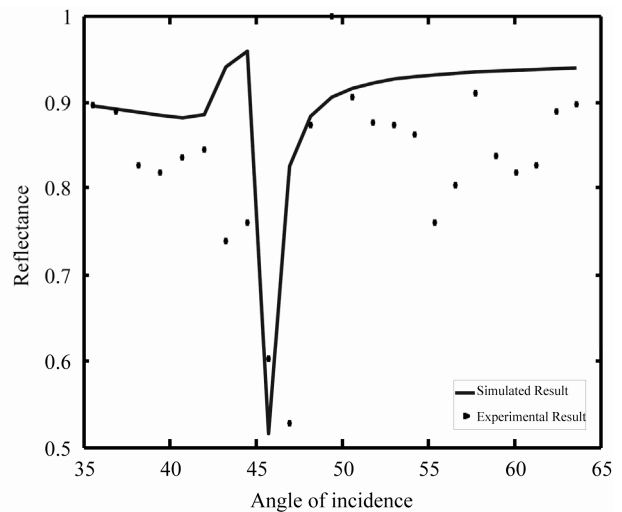
Figure 5. (a) Experimental set-up (schematic); (b) Experimental set-up (laboratory).

the angle of incidence  $\theta_i$  varies at the input end of the taper, angle of incidence  $\varphi(z)$  at the sensing region varies according to the formulae given by Equation (9), Equation (10). Thus, when  $\theta_i = 56^\circ$ ,  $\theta_r = 35^\circ$ ,  $\theta = (90 - \theta_r) = 55^\circ$ . Which gives  $\varphi(3.0) = 45.71^\circ$  which is the SPR angle of fused silica–silver interface having air as the sensing region. Here taper angle for Taper-1 is  $\Omega = 3.489^\circ$  as found from sec 2.3 and at the point of first reflection at the sensing region, taper radius is  $\rho(z) = 1.317$  cm as found from Equation (11). Knowing taper angle  $\Omega$ , taper radius  $\rho(z)$  and angle of incidence  $\varphi(z)$  at the sensing region and using Fresnel's reflection equation we can simulate the angle of incidence vs. reflectance graph considering the first point of reflection of the sensing region of non-planar tapered geometrical structures. Temperature during the experiment was fixed to  $22^\circ$  centigrade.

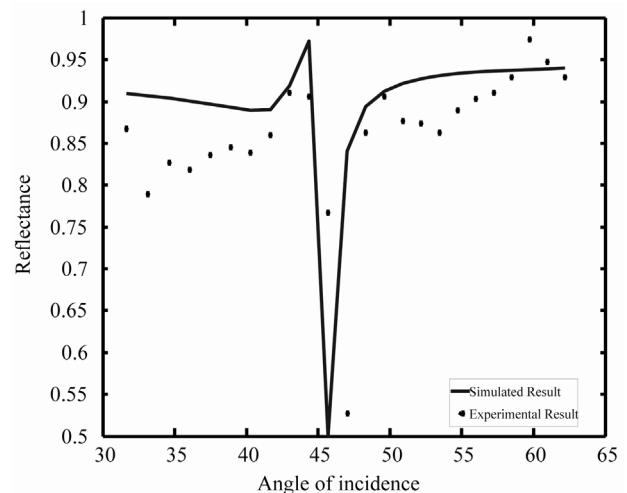
Geometry of **Figure 1** suggests that after few reflections, the light might fall on the reflective surface almost perpendicularly due to the fact that as light propagates along the length of taper, the angle of incidence decreases for each successive reflection on the surface of the glass rod. But we have restricted the length of our sample as shown in **Table 1**, so as to avoid the occurrence of such a situation. Moreover, as 35 nm Ag layer is semi-transparent and act as gray-filter, light may escape the rod sideways. But as the angle of incidence at the taper glass rod is kept greater than the critical angle, total internal reflection (TIR) is ensured, although there is some loss due to refraction at the uncoated glass when wave propagates further.

Similarly for Taper-2, taper angle is  $\Omega = 3.621^\circ$  and at the point of first reflection at the sensing region taper radius is  $\rho(z) = 1.253$  cm. When  $\theta_i = 52^\circ$ ,  $\theta_r = 33^\circ$ ,  $\theta = (90 - \theta_r) = 57^\circ$  which gives  $\varphi(3.9) = 45.69^\circ$ , which is the SPR angle of fused silica–silver interface having air as the sensing medium. Here taper angle for Taper-2 is  $\Omega = 3.621^\circ$  as found from sec 2.3 and at the point of first reflection at the sensing region, taper radius is  $\rho(z) = 1.253$  cm as found from Equation (11). Knowing taper angle  $\Omega$ , taper radius  $\rho(z)$  and angle of incidence  $\varphi(z)$  at the sensing region and using Fresnel's reflection equation we can simulate the angle of incidence vs. reflectance graph considering the first point of reflection of the sensing region of non-planar tapered geometrical structures. Temperature during the experiment was fixed to  $22^\circ$  centigrade.

From **Figure 6** and **Figure 7**, it is clear that simulation results have good agreements with that of experimental results. Though Taper-1 and Taper-2 have different sensing region lengths, there is no significant effect on the experimental results for SPR curve, because for these two tapers, SPR is happening only for the first reflection of the glass-metal interface of the tapered glass rod



**Figure 6.** Surface Plasmon Resonance curve showing the variation of reflectance with angle of incidence at the fused silica–silver interface of Taper-1 having air as sensing medium.



**Figure 7.** Surface Plasmon Resonance curve showing the variation of reflectance with angle of incidence at the fused silica–silver interface of Taper-2 having air as sensing medium.

whenever the phase matching condition is satisfied. As the Fresnel reflection formulae are valid for both planar and non-planar structures, here the simulation is done for the first point of reflection on Taper glass rod. Moreover, due to the tapering, there is a possibility of the loss of light due to refraction at the uncoated glass surface whenever the condition for TIR is not satisfied. Hence it decreases the output signal which again leads to lower signal to noise ratio. That is why very few reflections are used to avoid serious light loss. However, from Equation (10), it is clear that using tapered structure it is possible to broaden the angular range because lower value of angle means more spreading of evanescent wave field into

region adjacent to glass-metal interface [10]. Hence coupling between evanescent wave and surface plasmon wave will become stronger.

To quantify the performance of the thin film coating over Taper-1 and Taper-2, a quality factor (Q.F) can be used which is the ratio of depth of surface plasmon resonance and its full width at half maximum. If variation of Q.F with the molar ratio of  $\text{AgNO}_3/\text{KOH}$  is studied then it is clear that coating rate is maximized for optimum molar ratio of  $\text{AgNO}_3/\text{KOH}$ . Highest silver film quality is obtained when deposition rate is maximized. Performing silver coating at room temperature will give best result because as temperature increases there is a tendency of silver film to be oxidized [20]. To prevent the oxidation of silver film over the Tapered glass rods procedure discussed in sec 3.2 has been used in order to improve the result. The small deviation from simulated curve may be attributed to the fact that during wet deposition technique the deposited grain size is smaller (30 ~ 60 nm) and surface produced is rather rougher compared to vacuum deposition technique [19].

## 6. Conclusion

Tapered structure plays an important role for sensing with non-planar metal-dielectric interfaces and particularly for sensing within hollow conical devices in which it is easier to insert a tapered sensing element rather than a planar one. Present work describes the preliminary investigations on the observation of the surface plasmon resonance using such type of non planar taper structures. Further improvement of the results using sophisticated laboratory environment and precise thickness monitoring of the metal coating using vacuum deposition technique is possible and will be our next goal for future communication.

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