

# Stabilization of Wind Farm by Using PMSG Based Wind Generator Taking Grid Codes into Consideration

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## Abstract

This paper presents a new operational strategy for a large-scale wind farm (WF) which is composed of both fixed speed wind turbines with squirrel cage induction generators (FSWT-SCIGs) and variable speed wind turbines with permanent magnet synchronous generators (VSWT-PMSGs). FSWT-SCIGs suffer greatly from meeting the requirements of fault ride through (FRT), because they are largely dependent on reactive power. Integration of flexible ac transmission system (FACTS) devices is a solution to overcome that problem, though it definitely increases the overall cost. Therefore, in this paper, a new method is proposed to stabilize FSWT-SCIGs by using VSWT-PMSGs in a WF. This is achieved by injecting the reactive power to the grid during fault condition by controlling the grid side converter (GSC) of PMSG. The conventional proportional-integral (PI)-based cascaded controller is usually used for GSC which can inject small amount of reactive power during fault period. Thus, it cannot stabilize larger rating of SCIG. In this paper, a suitable fuzzy logic controller (FLC) is proposed in the cascaded controller of GSC of PMSG in order to increase reactive power injection and thus improve the FRT capability of WF during voltage dip situation due to severe network fault. To evaluate the proposed controller performance, simulation analyses are performed on a modified IEEE nine-bus system. Simulation results clearly show that the proposed method can be a cost-effective solution which can effectively stabilize the larger rating of SCIG compared to conventional PI based control strategy.

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## Keywords

Wind Turbine Generator, Fuzzy Logic Controller, Power System Stability, Power Converter, PI Controller

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## 1. Introduction

Global warming is one of the serious problems that the world faces recently due to the use of fossil fuel-based power plants to generate electricity [1]. Owing to the drawbacks of conventional power plants, clean energy has grown significantly since the last decade. Wind power (WP) is one of the clean energy sources which grow significantly since the last decade. According to the global wind energy council (GWEC), the cumulative installation size of WP was 539.1 GW at the end of 2017 and it will reach 840.9 GW by 2022 [2]. This huge installation of WP into the power system has serious impacts on system stability. In order to continue the smooth operation of power grid including WP, FRT necessities have been executed all over the world. It demands that the WF must remain connected to the power grid during a fault event and support the system in a similar way as conventional synchronous generators (SGs) [3].

Most of the WFs are constructed using FSWT-SCIG due to their superior characteristics, e.g., brushless operation, robust construction, operational simplicity and low cost [4]. However, the SCIG is directly coupled with the grid system and does not have FRT capability during network disturbance situation [4]. In addition, the SCIG necessitates large reactive power during fault situations to recover air gap flux. If sufficient reactive power is not injected, the developed electromagnetic torque drops significantly. Usually, a capacitor bank is placed near the SCIG terminal to inject the reactive power. However, the SCIG requires large amount of reactive power during transient period than steady state condition and the capacitor bank is unable to inject this high amount of reactive power during transient period.

In order to improve the FRT capability during network fault situation, some supplementary devices, for example, an energy capacitor system (ECS) [5], superconducting magnetic energy storage (SMES) [6], and a static synchronous compensator (STATCOM) [7] are installed in WFs with FSWT-SCIGs. However, the overall system cost increases.

On the other hand, the VSWT-PMSG is a smart kind of wind turbine system in which both active and reactive power output can be controlled effectively [8]. The advantages of VSWT-PMSG configurations are [9] [10]: 1) No brushes and gearbox, thus higher reliability and lower maintenance are required; 2) The full power converter totally decouples the generator from the grid, therefore power system disturbances have no direct impact on the generator; 3) No supplementary power supply for magnetic field excitation is required as permanent magnet is used in the rotor; 4) The converter allows very flexible control of active and

reactive power in all grid conditions (normal or disturbed); 5) The converter can fully control the amplitude and frequency of the generator voltage. However, the only drawbacks of VSWT-PMSG are expensive cost due to use of full rating power electronic AC/DC/AC converter. Thus, combined installation of small-scale VSWT-PMSG along with large-scale FSWT-SCIG could be an effective solution. The VSWT-PMSG system can supply additional amount of reactive power during transient period to the FSWT-SCIG. Therefore, the FRT capability of SCIG can be ensured at lower cost. The power converters of PMSG consist of machine side converter (MSC) and GSC. The GSC is responsible to inject reactive power to the grid system [11]. Thus, the designing of GSC control strategy is very crucial and equally important. Normally, cascaded control strategy based on four conventional PI controllers is used in the inner and outer loops of GSC controller [11]. But the accomplishment of the conventional PI controller is insufficient during transient period and it cannot provide effective amount of reactive power [12]. This is because, for example, conventional PI controller cannot deal with the system non-linearity due to parameter changes in the grid system. According to the deviation of the grid system impedances, gain margin and phase margin of the control system should be changed.

On the other hand, the FLC can handle nonlinear systems very effectively because it offers variable gain during transient conditions. Compared with conventional PI controller, FLC has the potential to provide an improved method even in the wide parameter variations. The FLC can take the place of conventional PI controller.

Thus, using an FLC in the inner loop of GSC controller to provide efficient amount of reactive power to stabilize SCIG-based WF during fault periods is convenient. Therefore, the main contribution of this paper is the design of a novel FLC-based GSC controller of PMSG to improve the FRT capability and stabilize the grid-connected SCIG-based WF. Detailed design procedure and control strategies of the overall system are presented in this paper. The effectiveness of the proposed control strategy is verified by both transient and dynamic simulation analyses. Real wind speed data measured in Hokkaido Island, Japan, are used for dynamic study.

The transient performance of the overall system composed of proposed GSC controller controlled PMSG, SCIG, and conventional SGs is compared with that composed of a PMSG controlled by conventional PI-based cascaded controller presented in [11]. Finally, it is found that the proposed FLC-based GSC controller is very effective to improve the FRT capability of SCIG-based WF.

The rest of the paper is organized as follows. Section 2 presents the description of power system model. Section 3 describes the wind turbine model, and the design procedure of the PMSG control system with proposed GSC controller is introduced in Section 4. The simulation results and a discussion of the performance of the proposed and conventional methods are presented in Section 5. Finally, Section 6 summarizes the findings and concludes the paper.

## 2. Description of Power System Model

This study employed the power system model illustrated in **Figure 1** for transient stability and dynamic performance analyses. It is composed of IEEE nine-bus main model and a WF. The main system consists of three conventional SGs (SG1 rating: 150 MVA, SG2 rating: 250 MVA and SG3 rating: 200 MVA). IEEE type AC4A exciter model presented in [13] is considered for all SGs. The SG1 and SG2 are thermal power plants whereas SG3 is a hydro power plant. The models and parameters of thermal and hydro governor systems are taken from [13]. The WF is connected to bus 5 through double circuit transmission lines, transformers, and it consists of one SCIG (rated capacity: 35 MW) and one PMSG (rated capacity: 15 MW) as shown in **Figure 1**. The total capacity of WF is 50 MW. Each PMSG and SCIG are denoted by an aggregated equivalent single generator to decrease computational time [14] [15]. The parameters of conventional SGs, SCIG, and PMSG are presented in **Appendix**.

## 3. Wind Turbine Model

The extracted mechanical power from a wind turbine can be expressed as [8]:

$$P_w = 0.5\rho\pi R^2 V_w^3 C_p(\lambda, \beta) \tag{1}$$

where,

$$C_p(\lambda, \beta) = c_1 \left( \frac{c_2}{\lambda_i} - c_3\beta - c_4 \right) e^{\frac{-c_5}{\lambda_i}} + c_6\lambda \tag{2}$$

$$\frac{1}{\lambda_i} = \frac{1}{\lambda - 0.08\beta} - \frac{0.035}{\beta^3 + 1} \tag{3}$$

$$\lambda = \frac{\omega_r R}{V_w} \tag{4}$$

where,  $P_w$  = Captured wind power,  $\rho$  = Air density (KG/m<sup>3</sup>),  $R$  = Radius of the

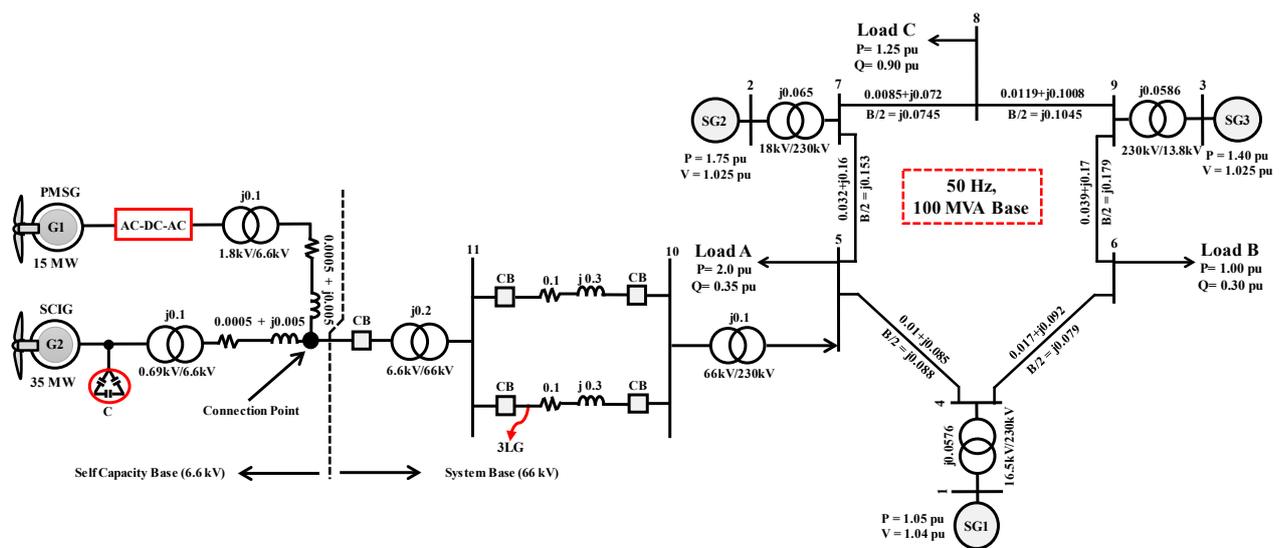


Figure 1. Power system model.

rotor blade (m),  $V_w$  = Wind speed (m/s),  $C_p$  = Power coefficient,  $\beta$  = Pitch angle, and  $\lambda$  = Tip speed ratio. In addition,  $c_1$  to  $c_6$  are characteristic coefficients of wind turbine [16], and  $\omega_r$  = rotational speed of wind turbine (rad/s).

The maximum power point tracking (MPPT) technique shown in Equation (5) is adopted in this work [8].

$$P_{MPPT} = 0.5\rho\pi R^2 \left(\omega_r / \lambda_{opt}\right)^2 C_{p\_opt} \tag{5}$$

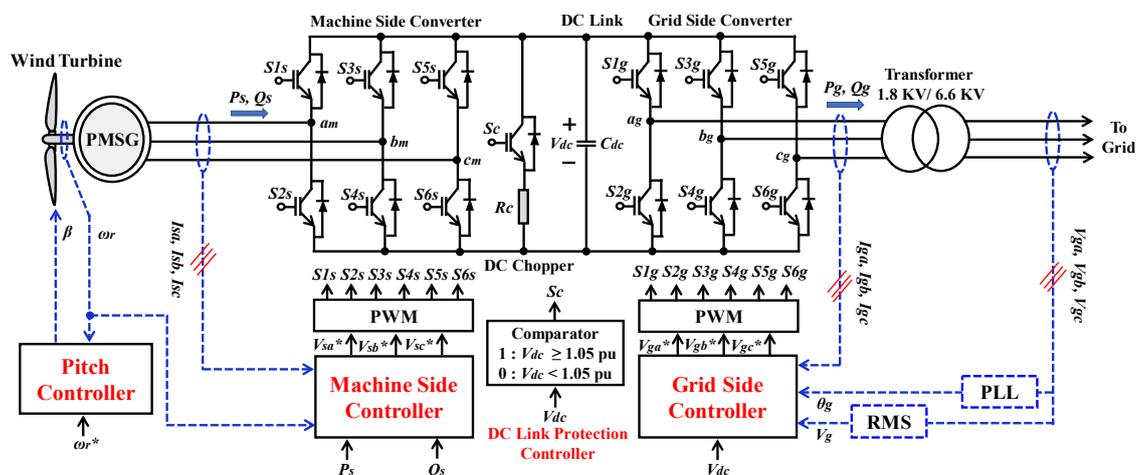
The rotating mass of variable speed wind turbine is composed of rotor hub with blades and generator shaft. The two-mass drive train model is considered in this work [11] [17].

### 4. PMSG Model and Control System

An arrangement of VSWT-PMSG and control scheme is illustrated in **Figure 2**. The complete system comprises wind turbine with drive train models, PMSG without gearbox, MSC, GSC, and pitch angle controller. The both converters are built by using two levels of insulated gate bipolar transistor (IGBT), and the machine side controller and the grid side controller are responsible for controlling them. The MSC is directly associated to the stator terminal of PMSG whereas the GSC is attached to the grid system through step up transformers. PMSG model available in PSCAD library is used in this work [18]. A DC chopper is located in the DC-Link circuit. It is controlled by the comparator block. When the DC-link voltage ( $V_{dc}$ )  $\geq 1.05$  pu, the comparator activates the DC chopper and protect the DC-Link circuit. The pulse width modulation (PWM) method is used in this work and the carrier frequency is taken 3.0 kHz for both converters. The rated  $V_{dc}$  is 3.0 kV.

#### 4.1. Machine Side Controller

The MSC transforms the three phase AC voltage generated by PMSG to DC voltage. The controller for MSC is composed of four conventional PI controllers as depicted in **Figure 3**. The controller is consisting of two loops; upper loop is for



**Figure 2.** Arrangement of PMSG system.

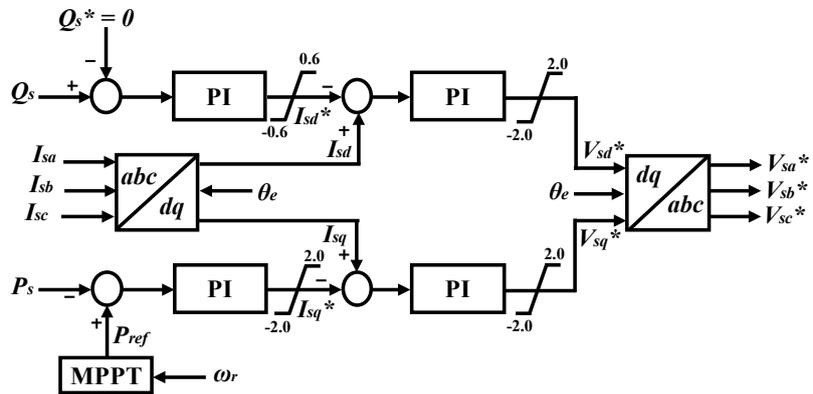


Figure 3. Machine side controller.

reactive power whereas lower one is for active power. The q-axis current ( $I_{sq}$ ) and the d-axis ( $I_{sd}$ ) current control the active power ( $P_s$ ) and reactive power ( $Q_s$ ) of the PMSG system, respectively. The reference active power ( $P_{ref}$ ) is obtained by the MPPT algorithm described in Section 3. The unity power factor operation is performed by setting the reference reactive power ( $Q_s^*$ ) to zero.

## 4.2. Grid Side Controller

This chapter describes the proposed controller of GSC and detail design procedure of FLC.

### 4.2.1. Proposed Grid Side Controller Operation

The GSC transforms the DC voltage into three phase AC voltage of the grid frequency. Figure 4 depicts the proposed controller for GSC. It is composed of three PI controllers and one FLC. The controller is used to control the reactive power ( $Q_g$ ) delivered to the grid and keep the  $V_{dc}$  constant by using the d-axis ( $I_{gd}$ ) and q-axis ( $I_{gq}$ ) currents of GSC. The FLC is used in the inner loop of the GSC controller to supply reactive power more efficiently during fault condition. Based on the system parameters, the FLC can provide variable gain. Therefore, it is possible to inject effective amount of reactive power during transient period. Thus, the terminal voltage can quickly be going back to the pre-fault value. In addition, the proposed control strategy can effectively stabilize the SCIG-based WF compared to conventional PI based cascaded GSC controller of PMSG.

### 4.2.2. Fuzzy Logic Controller Design

In order to design the proposed FLC, the error of the grid d-axis current ( $eI_{gd}$ ) and rate of change of the  $eI_{gd}$  ( $ceI_{gd}$ ) are considered as the controller inputs. The grid d-axis voltage reference ( $V_{gd}^*$ ) is chosen as the controller output. The main structure of the FLC consists of fuzzification, rule base, fuzzy inference, and defuzzification as illustrated in Figure 5 [19]. For fuzzification, the triangular membership functions with overlap are used for inputs and output as shown in Figure 6, in which the linguistic variables NB, NM, NS, ZO, PS, PM, and PB stand for negative big, negative medium, negative small, zero, positive small,



**Table 1.** Fuzzy rules.

$V_{gd}^*$	$ceI_{gd}$							
	<i>PB</i>	<i>PM</i>	<i>PS</i>	<i>ZO</i>	<i>NS</i>	<i>NM</i>	<i>NB</i>	
<i>PB</i>	PB	PB	PB	PM	PM	PS	ZO	
<i>PM</i>	PB	PB	PM	PM	PS	ZO	NS	
<i>PS</i>	PB	PM	PM	PS	ZO	NS	NM	
$eI_{gd}$	<i>ZO</i>	PM	PM	PS	ZO	NS	NM	NM
<i>NS</i>	PM	PS	ZO	NS	NM	NM	NB	
<i>NM</i>	PS	ZO	NS	NM	NM	NB	NB	
<i>NB</i>	ZO	NS	NM	NM	NB	NB	NB	

the power system model illustrated in **Figure 1**. The FLC was designed using FORTRAN code. For transient stability analysis, three line to ground (3LG) fault near bus 11 was considered as depicted in **Figure 1**. The fault is considered to happen at 0.1 s, the duration of fault is 0.1 s (5 cycles), the circuit breakers (CBs) on the faulty line are opened at 0.2 s in order to isolate the faulty line from the entire power system and reclosed at 1.0 s. The simulation time is 10.0 s with a solution time step of 5  $\mu$ s. The wind speed applied to each wind turbine is kept constant at 11.0 m/s based on the assumption that the wind speed does not change dramatically within this short period. Simulations were performed for two cases in order to validate the effectiveness of the proposed FLC controlled GSC controller of PMSG.

Case 1: with conventional cascaded GSC controller of PMSG presented in [11].

Case 2: with proposed cascaded FLC-based GSC controller of PMSG presented in Section 4.2.

The grid code of FRT requirement for WF which is considered in this study is illustrated in **Figure 7** [3]. Based on the curve, the wind turbine must stay connected with the power system if the voltage dip is within the defined range.

The simulation results of PMSG, SCIG, and SGs are depicted in **Figure 8** and **Figure 9**, respectively. The reactive power injected by PMSG to the SCIG system in Case 2 is greater than that in Case 1 after a severe network fault as shown in **Figure 8(a)**. Thus, the connection point voltage is recovered to the pre-fault value more quickly in Case 2 whereas it fails in Case 1 as depicted in **Figure 8(b)**. Since the connection point voltage does not satisfy the standard FRT graph presented in **Figure 7** for Case 1, the WF is disconnected from the power system by opening the CB near the connection point of wind generators at  $t = 2$  s. **Figure 8(c)** shows the rotor speed response of SCIG. As the reactive power injection by PMSG is insufficient in Case 1, thus, the rotor speed of SCIG becomes unstable. On the other hand, the reactive power injection by PMSG is higher and more effective in Case 2, thus, the rotor speed becomes stable in this case. The DC-Link voltage is returned to the steady-state value more quickly in Case 2, wherein it failed to back to the steady-state value in Case 1 as shown in **Figure 8(d)**.

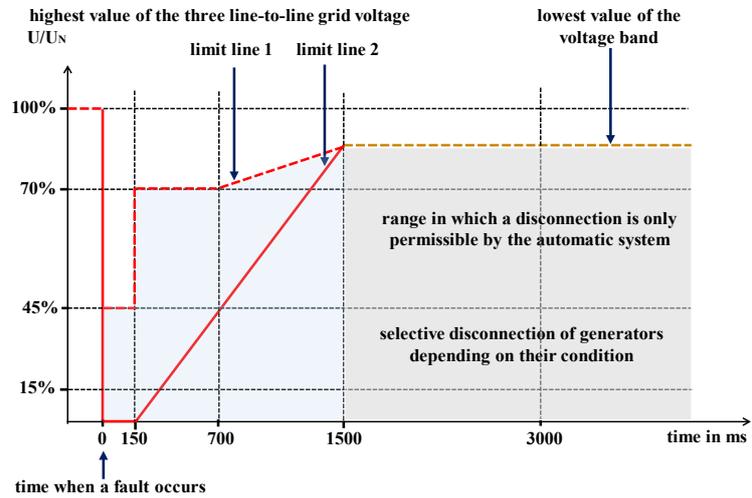


Figure 7. FRT requirement for WF.

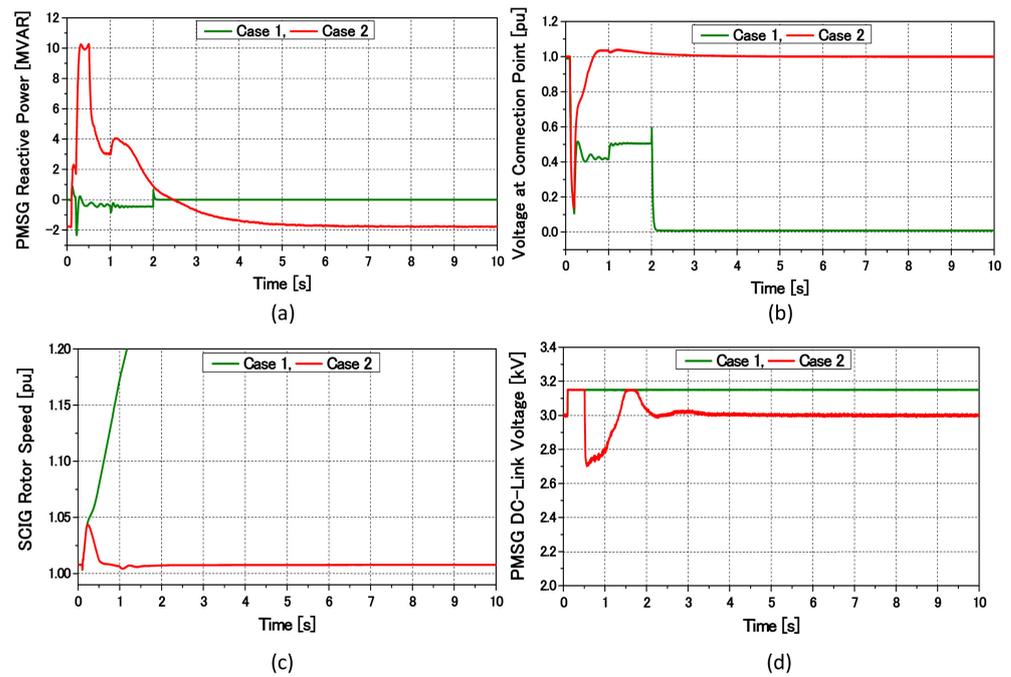


Figure 8. Responses of wind generators: (a) PMSG reactive power, (b) voltage at connection point of wind generators, (c) SCIG rotor speed, and (d) PMSG DC-Link voltage.

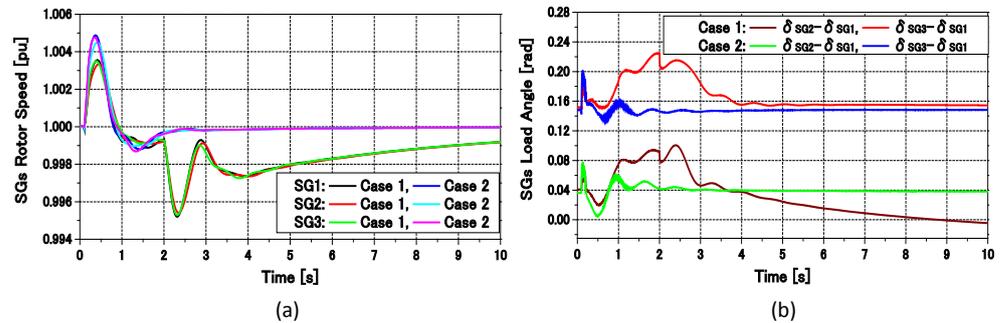


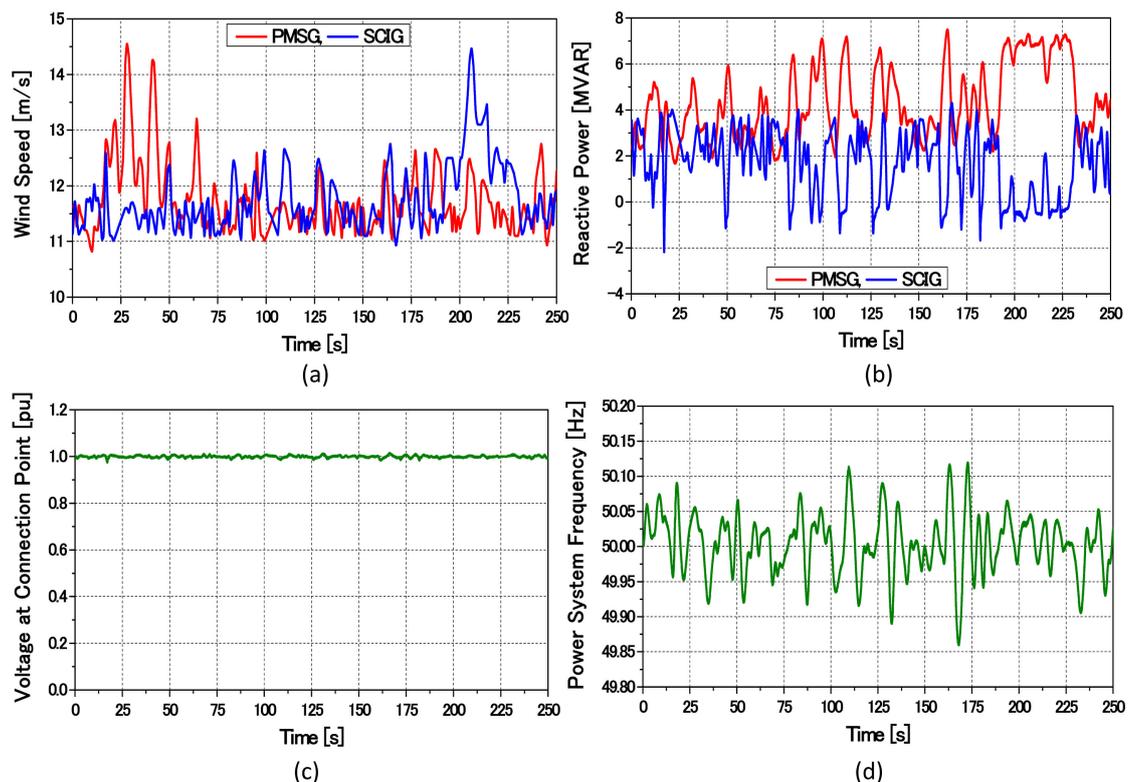
Figure 9. Responses of conventional SGs: (a) SGs rotor speed, and (b) SGs load angle.

**Figure 9(a)** and **Figure 9(b)** illustrate the rotor speed and power angle responses of conventional SGs ( $\delta_{SGs}$ ) with respect to SG1 load angle ( $\delta_{SG1}$ ). It is clearly seen from the figures that the rotor speed and power angle responses of SGs are more stable in Case 2 than Case 1. As a result, it can be concluded that the VSWT-PMSG with proposed FLC controlled GSC can enhance the transient stability of SGs as well as the voltage stability of the WF during transient condition.

## 5.2. Dynamic Performance Study

In this chapter, analysis about dynamic performance about the proposed GSC controller of PMSG is presented. The same power system model depicted in **Figure 1** is used in this study. The total simulation time is 250.0 s. The real wind speed data measured at Hokkaido Island, Japan, shown in **Figure 10(a)**, is used in the simulation. **Figure 10(b)** shows the reactive power output of each wind generator. The PMSG supplies the necessary reactive power to the SCIG for voltage regulation. Thus, the connection point voltage is approximately constant, as shown in **Figure 10(c)**. Due to the fluctuations in the wind speed of wind generators, the frequency response of the power system is varying as shown in **Figure 10(d)**. But, the frequency fluctuations lie within the permissible limit in Japan ( $\pm 0.2$  Hz).

The dynamic simulation study confirmed that the proposed FLC-controlled



**Figure 10.** Responses of power system: (a) applied wind speeds to wind generators, (b) reactive power output of wind generators, (c) voltage at connection point of wind generators, and (d) power system frequency response.

PMSG system can effectively supply reactive power and thus maintain the connection point voltage constant under a randomly varying wind speed.

## 6. Conclusions

This study proposes the application of fuzzy logic in GSC controller of PMSG to enhance the FRT capability of SCIG-based WF during transient period. The effectiveness of the proposed controller is tested by considering severe 3LG fault. The transient performance of the overall system composed of the proposed FLC-controlled PMSG, SCIG, and conventional SGs is compared with that of PMSG with the conventional control strategy. It is found that the proposed control strategy can ensure the FRT capability of WF as well as power system transient and steady-state stability. Therefore, it can be concluded that the proposed GSC controller for PMSG can be an effective solution to augment the transient stability of the grid-connected WF.

Application of adaptive neuro-fuzzy inference system (ANFIS) based control strategy of GSC for PMSG is strong candidate for future study.

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## Conflicts of Interest

The authors declare no conflicts of interest regarding the publication of this paper.

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## Appendix

The SGs, PMSG, SCIG, and drive train parameters used in this study are given in **Table A1**.

**Table A1.** Parameters of conventional SGs and wind generators.

Parameters	Synchronous Generators			PMSG		SCIG		
	SG1 (Thermal) (AGC)	SG2 (Thermal) (GF)	SG3 (Hydro) (AGC)	MVA	15	MVA	35	
				$R_s$	0.01 pu	$R_1$	0.01 pu	
				$L_s$	0.1 pu	$X_1$	0.1 pu	
Rated Power	150 MVA	250 MVA	200 MVA	$X_d$	0.9 pu	$X_m$	3.5 pu	
Voltage	16.5 kV	18 kV	13.8 kV	$X_q$	0.7 pu	$R_{21}$	0.035 pu	
	$R_a$	0.003 pu	0.003 pu	0.003 pu	$Flux$	1.4 pu	$R_{22}$	0.014 pu
	$X_l$	0.1 pu	0.1 pu	0.1 pu	$H_l$	5.2 s	$X_{21}$	0.03 pu
	$X_d$	2.11 pu	2.11 pu	1.20 pu	$H_g$	0.8 s	$X_{22}$	0.089 pu
	$X_q$	2.05 pu	2.05 pu	0.700 pu	$D$	1.5	$H$	1.0 s
	$X'_d$	0.25 pu	0.25 pu	0.24 pu	$K$	296		
	$X''_d$	0.21 pu	0.21 pu	0.20 pu				
	$X''_q$	0.21 pu	0.21 pu	0.20 pu				
	$T'_{do}$	6.8 s	7.4 s	7.2 s				
	$T''_{do}$	0.033 s	0.033 s	0.031 s				
	$T''_{qo}$	0.030 s	0.030 s	0.030 s				
	$H$	4.0 s	4.0 s	4.0 s				