

Safety Assessment of Ionic Liquid-Based Lithium-Ion Battery Prototypes

J. Kalhoff¹, G.-T. Kim², S. Passerini^{2*}, G. B. Appetecchi^{3*}

¹Institute of Physical Chemistry, University of Muenster, Muenster, Germany

²Helmholtz Institute Ulm-Karlsruhe Institute of Technology, Ulm, Germany

³ENEA, Agency for New Technologies, Energy and Sustainable Economic Development, SSPT-PROMAS-MATPRO, Rome, Italy

Email: *stefano.passerini@kit.edu, *gianni.appetecchi@enea.it

Received 26 December 2015; accepted 15 March 2016; published 18 March 2016

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Abstract

In this paper we report the results of combined cycle- and life-aging and abuse tests carried out under severe conditions on $\text{Li}_4\text{Ti}_5\text{O}_{12}/\text{LiFePO}_4$ lithium-ion stacked prototypes using a PYR_{14} FSI-LiTFSI ionic liquid electrolyte. No relevant degradation phenomena took place within ionic liquid electrolyte during prolonged inactivity period or overcharging. No fire/explosion or venting event as well as no gas development occurred during abuse tests, which led only to modest raise in temperature. Therefore, electrodes based on $\text{Li}_4\text{Ti}_5\text{O}_{12}$ and LiFePO_4 active materials can be favorably combined with non-volatile and non-flammable pyrrolidinium FSI ionic liquid electrolytes to realize highly safe lithium-ion battery systems.

Keywords

Ionic Liquids, Lithium-Ion Battery Prototype, Abuse Tests

1. Introduction

Present lithium battery systems use electrolytes based on organic solvents, which represent a major safety problem [1]-[4]. In fact, the presence of flammable and volatile organics can lead to dangerous events such as heat generation, thermal runaway, cell venting, fire and, therefore, rapid cell disassembly. For instance, uncontrolled heat development might cause combustion of the vaporized organic electrolyte with oxygen becoming available from the decomposition of the positive electrode [5] [6], leading to catastrophic events (explosion). In addition, the electrolyte burning causes decomposition of the lithium salt, LiPF_6 , and the PVdF-based electrode binder [7],

*Corresponding author.

leading to development of highly toxic HF gas [8].

Battery manufacturers design systems to deliver specified performance characteristics in safe manner under anticipated usage conditions. However, failure can be caused by poor execution of design, abuse of system usage and unanticipated abuse conditions [9] [10]. Passive and active safeguards [11] have been designed to mitigate or prevent some failures. Major challenges in performance and safety are thermal stability of battery active materials and occurrence of internal short circuits [11]. Therefore, standards and testing protocols have been developed as guidelines on how to assess the safety of lithium-ion batteries [11]-[14].

A very promising approach to overcome the lithium battery safety limitation is represented by the replacement of organic hazardous solvents with non-volatile, non-flammable, thermally stable fluids known as ionic liquids (ILs), e.g., organic/inorganic salts generally molten at room temperature or below [15] [16]. Particularly, ILs based on pyrrolidinium cations and bis(trifluoromethanesulfonyl)imide (TFSI) or bis(fluoromethanesulfonyl)imide (FSI) anions have been successfully proposed for use in lithium batteries [16]-[26].

In the frame of the European project ILLIBATT, we scaled up $\text{Li}_4\text{Ti}_5\text{O}_{12}/\text{LiFePO}_4$ lithium-ion cells using a PYR_{14} FSI-LiTFSI electrolyte mixture, aiming to realize greener and safer prototypes. The latter, having a nominal capacity of 0.8 A h, were developed for low to mid-rate applications such as renewable energy storage [27]. The safety level results further enhanced by the use of $\text{Li}_4\text{Ti}_5\text{O}_{12}$, which does not require any passive layer (SEI) at the anode/electrolyte interface [28], and LiFePO_4 , because of its resistance to release oxygen (above 225°C) due to the strong bonding to phosphorous [29]. In addition, it should be pointed that the electrodes were made using the fluorine-free, economically viable, natural binder carboxymethylcellulose sodium salt (CMC), this involving the use of water as the only solvent and allowing easier recycle of the battery components at the end of life [25] [26]. In the present paper we report the results obtained from abuse tests on two of these innovative, ionic liquid-based, $\text{Li}_4\text{Ti}_5\text{O}_{12}/\text{LiFePO}_4$ stacked battery prototypes.

2. Experimental

2.1. Battery Prototype Manufacturing

The $\text{Li}_4\text{Ti}_5\text{O}_{12}/\text{LiFePO}_4$ cell components, namely the ionic liquid electrolyte and composite electrodes, were prepared according to procedure routes reported in details elsewhere [25]-[27] [30]. The stacked prototypes were manufactured within a dry-room (relative moisture content $< 0.2\%$ at 20°C), housed in soft packages, evacuated for about 1 h and, finally, heat-sealed under vacuum.

2.2. Abuse Test

Upon manufacturing, two 0.8 A h class $\text{Li}_4\text{Ti}_5\text{O}_{12}/\text{LiFePO}_4$ stacked prototypes were subjected to two hundreds consecutive charge/discharge full cycles within the 1.0 - 2.5 voltage range at 0.1C current rate, corresponding to 80 mA. The electric tests were performed at $20^\circ\text{C} \pm 2^\circ\text{C}$ using a Maccor 4000 battery tester. Successively, the fully charged prototypes were stored on a shelf in uncontrolled environment for three years. After this aging period, the batteries were again subjected to 100 full cycles (0.1C at $20^\circ\text{C} \pm 2^\circ\text{C}$). Finally, the two cells were fully charged at 0.1C and, then, subjected to different abuse test types.

The first prototype (ILLIBATT #1) underwent the nail penetration test (**Figure 1**, panel A) using a custom designed Abuse Test Chamber (hereinafter called ATC). The abuse test was performed using a 3 mm diameter steel nail, penetrating the pouch cells perpendicularly with a plunge speed of $80 \text{ mm}\cdot\text{s}^{-1}$. The electric data on the test prototype were collected by a modified 540-R 30 A potentiostat/galvanostat. Additionally, the cell deformation was logged by a high speed camera. IR images referred to internal prototype bulk were taken by Allied Vision Technology IRC 320 infrared camera. Moreover, thermal properties were documented by thermocouples.

The second prototype (ILLIBATT #2) was overcharged (**Figure 1(b)**) up to 50% of the nominal capacity, or 100% of the capacity (0.4 A h) measured at the 300th charge/discharge full cycle, under a current rate equal to 1C (0.4 A). Therefore, the cell was subjected to an overall charge of 0.8 A h (200% SOC with respect to the capacity value detected at the 300th full cycle). As well as for the first prototype, the behavior of ILLIBATT #2 under overcharge tests was followed by potentiostat/galvanostat, high speed camera and thermocouples. Upon overcharging the prototype ILLIBATT #2 was discharged down to 1.0 V and, successively undergone to cycling tests at 0.05C current rate (40 mA) and $20^\circ\text{C} \pm 2^\circ\text{C}$. **Table 1** reports the protocol of the overall abuse tests to which the two prototypes were subjected.

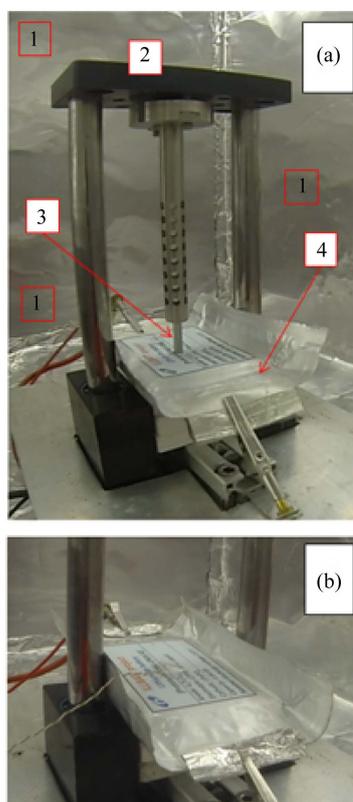


Figure 1. Execution of nail penetration (panel A) and overcharging (panel B) tests on ionic liquid-based, stacked, $\text{Li}_4\text{Ti}_5\text{O}_{12}/\text{LiFePO}_4$ lithium-ion ILLIBATT prototypes. Legend in panel A: 1) abuse test chamber (ATC); 2) abuse test equipment; 3) steel nail; 4) prototype under test.

Table 1. Abuse test protocol carried out on the ILLIBATT battery prototypes.

Prototype #1			
Step	Mode		Operating conditions
1	Charge/discharge cycling	200 cycles; voltage range: 1.5 - 2.5 V; current: 80 mA (0.1C); T = 20°C	
2	Full charge up to 2.5 V		current: 80 mA (0.1C); T = 20°C
3	Storage in external		3 years; room temperature
4	Charge/discharge cycling	100 cycles; voltage range: 1.5 - 2.5 V; current: 80 mA (0.1C); T = 20°C	
5	Full charge up to 2.5 V		current: 80 mA (0.1C); T = 20°C
6	Nail penetration		steel nail: 3 mm diameter; plunge speed; 80 mm·s ⁻¹
Prototype #2			
Step	Mode		Operating conditions
1	Charge/discharge cycling	200 cycles; voltage range: 1.5 - 2.5 V; current: 80 mA (0.1C); T = 20°C	
2	Full charge up to 2.5 V		current: 80 mA (0.1C); T = 20°C
3	Storage in external		3 years; room temperature
4	Charge/discharge cycling	100 cycles; voltage range: 1.5 - 2.5 V; current: 80 mA (0.1C); T = 20°C	
5	Full charge up to 2.5 V		current: 80 mA (0.1C); T = 20°C
6	Overcharge	up to 100 % capacity detected at 300 th cycle (0.4 A h); current: 0.4 A	
7	Discharge		1.0 V; current: 40 mA; T = 20°C
8	Charge/discharge cycling		voltage range: 1.5 - 2.5 V; current: 40 mA (0.05 C); T = 20°C

3. Results and Discussion

The fresh-manufactured ILLIBATT lithium-ion prototypes were initially subjected to full charge-discharge cycling tests. The results, reported in **Figure 2** as voltage vs discharge capacity profiles, show reproducible flat plateau around 1.8 V, typical of $\text{Li}_4\text{Ti}_5\text{O}_{12}/\text{LiFePO}_4$ cells [25]-[27], with an initial reversible capacity equal or above 0.6 A h, *i.e.*, exceeding 75% of the theoretical value. These values are extremely promising considering that the electrodes and the cells were, respectively, manually produced and assembled with simple laboratory equipment. Regarding the cycling tests, a progressive decrease of delivered capacity is observed, particularly upon 30 cycles, even if no substantial change of the voltage profile was detected, this suggesting no practical variation of the nominal discharge voltage and ohmic drop. Capacity values equal to 0.4 A h (50% of the theoretical value) and 0.46 A h (about 60%) were still delivered after 200 cycles by the ILLIBATT #1 and ILLIBATT #2 prototypes (**Figure 4**), respectively, approaching 68% and 75% of the initial values. Also, a coulombic efficiency levelling 100% upon a few cycles (data not reported) was detected.

The effects resulting from prolonged inactivity periods (e.g., three years) were evaluated by cycling tests. **Figure 3** plots the voltage vs capacity profile of selected charge/discharge cycles, which displayed the expected feature for $\text{Li}_4\text{Ti}_5\text{O}_{12}/\text{LiFePO}_4$ cells even upon prolonged storage in uncontrolled environment. No relevant variation of the ohmic drop and nominal voltage was observed (during cycling tests) with respect to the freshly manufactured prototypes. This indicates that the ionic liquid electrolyte kept its ion transport properties even

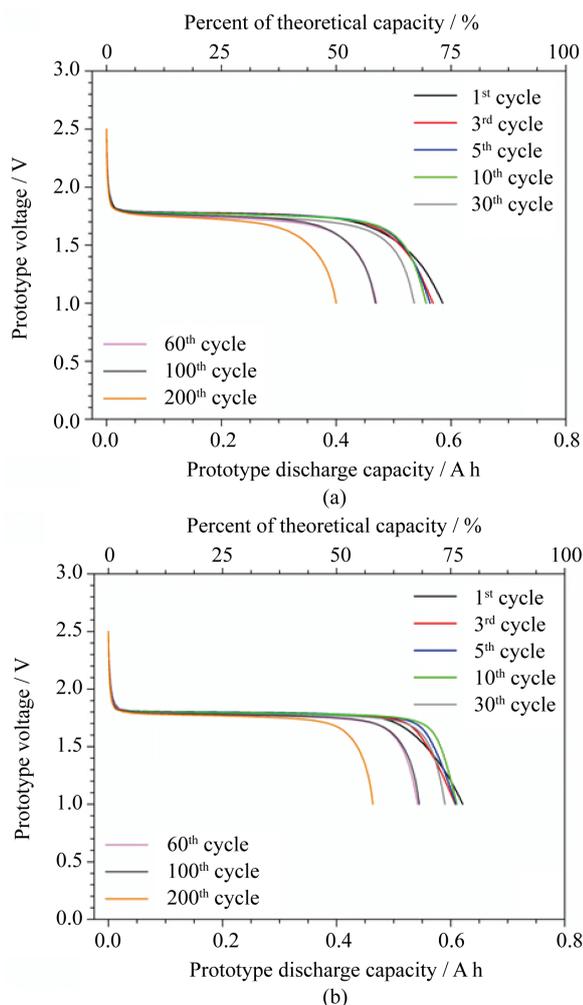
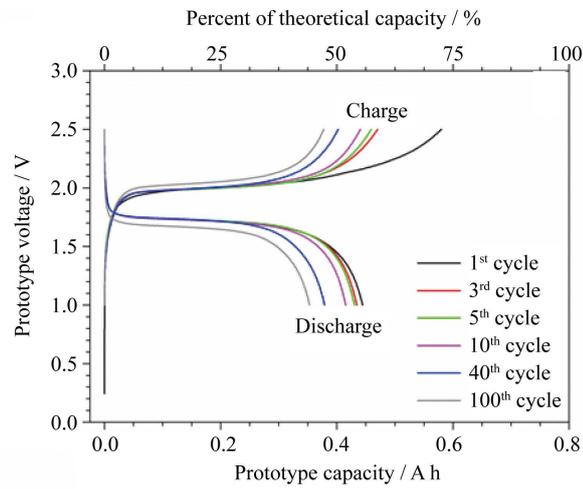
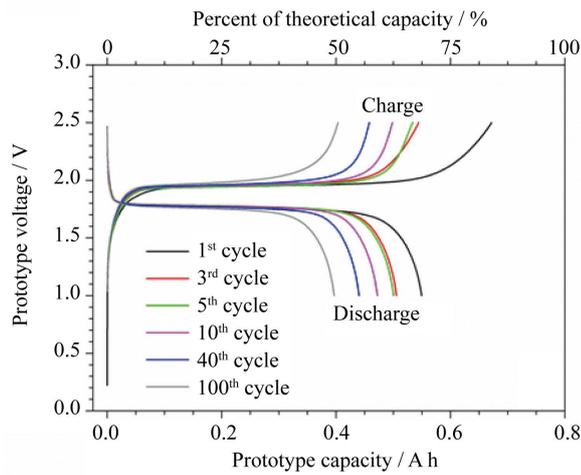


Figure 2. Voltage vs capacity profile of selected discharge cycles performed (0.1C at $20^\circ\text{C} \pm 2^\circ\text{C}$) on fresh-manufactured ILLIBATT #1 (panel A) and ILLIBATT #2 (panel B) prototypes.



(a)



(b)

Figure 3. Voltage vs capacity profile of selected charge/discharge cycles performed (0.1C at $20^{\circ}\text{C} \pm 2^{\circ}\text{C}$) on ILLIBATT #1 (panel A) and ILLIBATT #2 (panel B) prototypes after a three year storage period under rest conditions in uncontrolled environment.

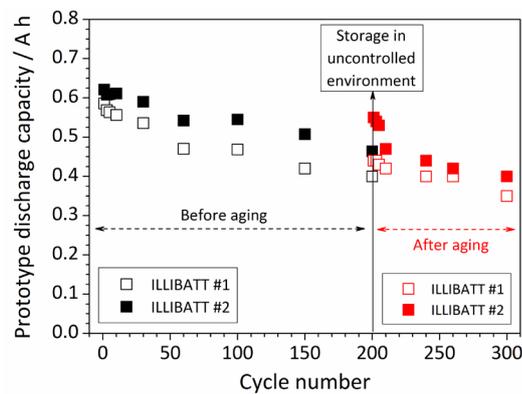


Figure 4. Cycling performance (0.1C at $20^{\circ}\text{C} \pm 2^{\circ}\text{C}$) of the ILLIBATT #1 and ILLIBATT #2 prototypes before (black data markers) and after (red data markers) a three year storage period under rest condition in uncontrolled environment.

upon prolonged storage of the electrochemical devices and, therefore, no relevant degradation process and/or parasitic reaction regarding the electrolyte components (ionic liquids and lithium salt) took place both under current flow and during rest conditions. The aged prototypes have delivered an initial capacity (see 1st cycle in panels A and B of **Figure 3**) equal to 0.44 A h (ILLIBATT #1 in panel A) and 0.55 A h (ILLIBATT #2 in panel B), respectively, which were higher than those delivered at the end of the cycling tests (200th cycle in panels A and B of **Figure 2**) before the three year shelf storage under uncontrolled conditions (**Figure 4**). This is likely due to ion relaxation phenomena occurring (after prolonged full cycling tests) within the electrolyte and electrodes. Successively, the capacity is seen to decrease down to 0.35 A h (ILLIBATT #1) and 0.4 A h (ILLIBATT #2) upon one hundred consecutive full charge-discharge cycles (**Figure 4**). The initial coulombic efficiency was around 77%, but quickly approaching 100%, as already observed for the freshly assembled prototypes. Therefore, the prolonged inactivity period in uncontrolled conditions does not seem to remarkably affect the reversibility of the lithium intercalation process.

Figure 4 summarizes the cycling behavior results, in terms of discharge capacity evolution, obtained before (black data markers) and after (red data markers) the prolonged storage in uncontrolled conditions. The fresh battery prototypes deliver similar initial capacities, e.g., close to 0.6 A h, this is highlighting the more than acceptable reliability of the manual manufacturing procedure. However, ILLIBATT #2 exhibits better cycling performance (higher capacity retention) than ILLIBATT #1, showing the lower capacity fade (0.60 mA h, *i.e.*, 0.097% per cycle, *vs* 0.95 mA h, *i.e.*, 0.16% per cycle) during the initial two hundreds charge-discharge cycles.

After three years shelf-aging, the prototypes initially display an increase of capacity (above 10 %) with respect to that delivered at the end of the cycling test before shelf-aging. This is highlighted by the comparison between the capacity values obtained from the last cycle before storage (black data markers) and the first one after storage (red data markers). However, after the following few cycles, the capacity evolution of the aged prototypes approached the trend exhibited previously, *i.e.*, showing similar fading. This clearly indicates that no appreciable degradation phenomena occurred for the ionic liquid electrolyte and electrodes during the prolonged storage period. Summarizing, very prolonged inactivity periods (up to three years) in uncontrolled environment do not affect the cycling performance of the ionic liquid-based, $\text{Li}_4\text{Ti}_5\text{O}_{12}/\text{LiFePO}_4$ prototypes.

Before abuse tests (and successively to the cycling tests), the ILLIBATT prototypes were fully charged up to 2.5 V (0.1C) as illustrated by the voltage vs time profiles reported in **Figure 5**. The external cell temperature evolution, recorded during the charge step (data not reported), was found to be rather stable around 22°C with a variation lower than 1°C, which might be likely due to lab temperature change.

The results of the nail penetration tests performed on the ILLIBATT #1 prototype are depicted in **Figure 6**. The voltage value (panel A) is seen to sharply decay down to 1 V as a result of the nail penetration, and, successively, asymptotically achieve 0 V within a few minutes, indicating short-circuit. It is worthy to point out that no fire (or deflagration) and/or venting as well as no gas development and device deformation/crack were observed during the whole duration of the abuse test (**Figure 1**), witnessing safety levels not detectable in commercial

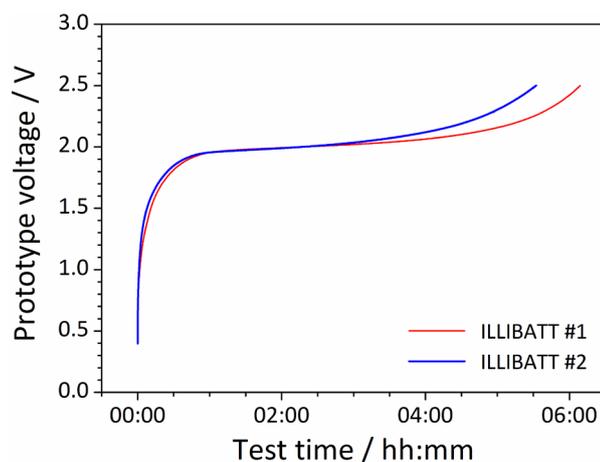


Figure 5. Full charge step run on the ILLIBATT #1 (red trace) and ILLIBATT #2 (blue trace) prototypes at 0.1C (20°C ± 2°C) before abuse tests.

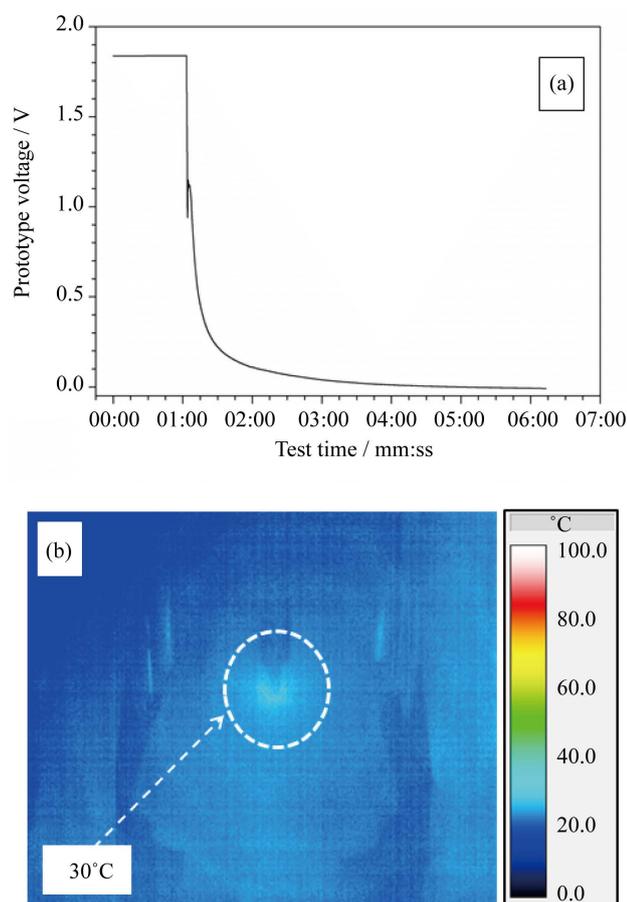


Figure 6. Voltage vs time drop (panel a) recorded on the ILLIBATT #1 prototype during nail penetration test at $20^{\circ}\text{C} \pm 2^{\circ}\text{C}$. The IR camera image (panel b) was taken at the highest temperature after 10 s penetrating into the prototype.

lithium-ion batteries [9]-[14]. The cell external temperature, monitored during the nail penetration by an IR camera, does not exceed 30°C as evidenced by the image depicted in panel B where the warmest zone is highlighted with a dotted circle (it is to note that the IR image was taken at the highest temperature after 10 s penetrating into the cell). This modest temperature raise supports, once more, for the high reliability issues of the ILLIBATT prototypes.

Figure 7 reports the results obtained from overcharging tests performed on the already fully charged prototype ILLIBATT #2. Despite the overcharge step, causing cell voltage raise up to 6 V (*i.e.*, more than twice the regular cut-off voltage, 2.5 V), as shown by the voltage vs time profile in **Figure 7**, the external temperature of ILLIBATT #2 (dotted line) is seen to increase from about 23°C (start of overcharge) to 32°C (end) *e.g.*, recording a rise of just 7°C . Apart slight cell inflation, no flame or venting was noticed during the abuse test, as previously observed for ILLIBATT #1, once more confirming the safety of these ionic liquid-based, lithium battery systems. Upon the overcharge step, the prototype voltage asymptotically decays down to 3.5 V in less than 1 hour (likely due to relaxation phenomena) whereas the external cell temperature decreases, following an analogous trend, down to slightly above 25°C . The cycling ability of ILLIBATT #2 was tested even upon the overcharge step. The results, illustrated as voltage vs time profiles in **Figure 8**, show a reversible capacity of 70 mA h and indicate that the prototype can be cycled afterwards, still delivering 15% of the initial capacity.

Summarizing, abuse tests have revealed that combining highly reliable $\text{Li}_4\text{Ti}_5\text{O}_{12}$ and LiFePO_4 active material electrodes with non-volatile and non-flammable pyrrolidinium FSI ionic liquid electrolytes results in highly safe lithium-ion battery systems, keeping their safety assessment even in stacked prototypes.

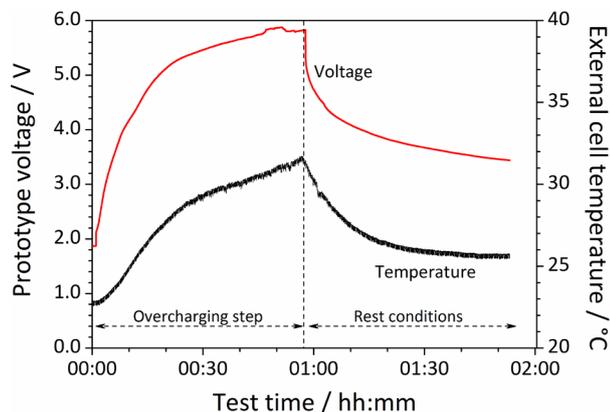


Figure 7. Voltage (red trace) and external temperature (black trace) vs time evolution recorded on the prototype ILLIBATT #2 during and upon overcharging test run up to 200% of the nominal capacity at a current rate equal to 1C (20°C ± 2°C).

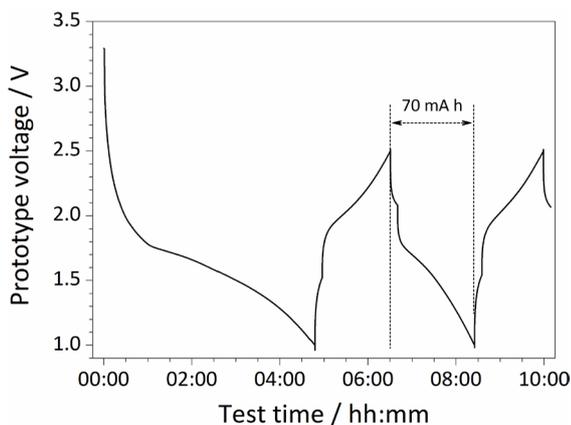


Figure 8. Voltage vs time profile referred to cycling tests run at 0.05C current rate (40 mA) on the prototype ILLIBATT #2 after overcharging test. T = 20°C ± 2°C.

4. Conclusion

Li₄Ti₅O₁₂/LiFePO₄ lithium-ion battery prototypes, manufactured in the frame of an European project using a PYR₁₄ FSI-LiTFSI ionic liquid electrolyte, were subjected to combined three-year storage in uncontrolled environment followed by abuse tests (nail penetration and overcharging). The results have revealed that the ionic liquid electrolyte is able to stand prolonged inactivity periods and high voltages without relevant degradation phenomena. No fire/explosion or venting event as well as no gas development occurred during abuse tests even performed under severe conditions, which led only to modest raise in temperature within the prototypes. Therefore, electrodes based on Li₄Ti₅O₁₂ and LiFePO₄ active materials can be favorably combined with non-volatile and non-flammable pyrrolidinium FSI ionic liquid electrolytes to realize highly safe lithium-ion battery systems.

Acknowledgements

The authors gratefully acknowledge the financial support of the European Commission under Contracts NMP3-CT-2006-033181 (ILLIBATT project).

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