

Design and Parametric Simulation of a Bi-Band Miniaturized PIFA Antenna for the GSM900 and DCS1800 Bands

Abdelhakim Elouadih¹, Ahmed Oulad-Said¹, Moha Mrabet Hassani²

¹Department of Electrical and Telecommunications Engineering, Royal Air Academy (ERA), Marrakesh, Morocco; ²Department of Physics, Semlalia University of Sciences (FSSM), Marrakesh, Morocco.
Email: elouadih@gmail.com, a_ouladsaid@hotmail.com, hassani@ucam.ac.ma

Received February 26th, 2013; revised March 28th, 2013; accepted April 11th, 2013

Copyright © 2013 Abdelhakim Elouadih *et al.* This is an open access article distributed under the Creative Commons Attribution License, which permits unrestricted use, distribution, and reproduction in any medium, provided the original work is properly cited.

ABSTRACT

This paper describes the design and simulation by HFSS simulator of a probe-fed Planar Inverted-F Antenna (PIFA) for the use in GSM900 band [890 MHz - 960 MHz] and DCS1800 band [1710 MHz - 1880 MHz]. A methodology based on parametric simulations (parameters are ground plan length, height of radiating plate, feeding point position, shorting plate width and position) was used to design optimized antenna. The simulation allowed the characterization of the designed antenna and the computing of different antenna parameters like S_{11} parameter, resonant frequency, VSWR, bandwidth, impedance in feeding point, gain, diagram pattern and Fields distribution. The results were very interesting and respect the GSM requirements.

Keywords: GSM; DCS; HFSS; PIFA; Patch Antenna; Parametric; Simulation

1. Introduction

Wireless communications have progressed very rapidly in recent years, and many mobile units are becoming smaller and smaller. To meet the miniaturization requirement, the antennas employed in mobile terminals must have their dimensions reduced accordingly. Planar antennas, such as microstrip and printed antennas have the attractive features of low profile, small size, and conformability to mounting hosts and are very promising candidates for satisfying this design consideration. Planar antennas are also very attractive for applications in communication devices for wide mobile telecommunications like GSM, wireless local area network, aeronautics and embedded systems [1].

For optimum system performance, the antennas must have high radiation efficiency, small volume, isotropic radiation characteristics, small backward radiation, simple and low-loss impedance matching to patches. The major types of configurations of low-profile antennas with enhanced bandwidth performance include planar inverted F Antennas.

The PIFA consists in general of a ground plane, a top plate element, a feed wire attached between the ground plane and the top plate, and a shorting wire or strip that is

connected between the ground plane and the top plate.

The antenna is fed at the base of the feed wire at the point where the wire connects to the ground plane. The PIFA is an attractive antenna for wireless systems where the space volume of the antenna for wireless systems where the space volume of the antenna is quite limited. It requires simple manufacturing, since the radiator must only be printed. The addition of a shorting strip allows good impedance match to be achieved with a top plate that is typically less than $\lambda/4$ long. The resulting PIFA is more compact than a conventional half-wavelength probe-fed patch antenna [2].

The miniaturization can affect radiation characteristics, bandwidth, gain, radiation efficiency and polarization purity. The miniaturization approaches are based on either geometric manipulation (the use of bend forms, meandered lines, PIFA shape, varying distance between feeder and short plate [3]) or material manipulation (Loading with a high-dielectric material, lumped elements, conductors, capacitors, short plate [4]) or the environment characteristics (ground plane dimensions, coupling, measurement and fabrication errors [3]). In this case, the bi-band designed antenna is shorted to the ground plane by a plate, uses regular shapes and uses a

high dielectric thin substrate under the radiating plate not above the ground plane).

If all precedent works are concentrated on studying the effects of these elements (material, geometry, environment), the choice of a PIFA element was so improvised in the design. In this paper, a methodology based on parametric simulation is used to choose simultaneously or independently different PIFA elements and the results should be compliant for both bands.

In the next section, the author presents the methodology and detailed parametric simulations to optimize the antenna design. After, the dimensions and parameters are then chosen. The author exposes in the third section the characteristics of the designed antenna.

2. Design Methodology

2.1. The Description of the Studied Antenna

As shown in **Figure 1**, the designed antenna has a rectangular radiating patch length $L_p = 29.3$ mm and width $W_p = 64$ mm. the patch is placed at a height h from the ground plan. The patch has a length L_g and a width W_g equal to W_p . The patch is matched to the ground plan via a rectangular shorting plate. The shorting plate has a width W_s and a length h . The shorting post of usual PIFA types is a good method for reducing the antenna size, but results in narrow impedance bandwidth. It is placed in the (yz) plan at a distance D from the edge centre. The the feeding point is situated at p from the rear edge of the patch. The patch is fed by a 50Ω wire, a semi-rigid coax with centre conductor that extends beyond the end of the outer conductor is used to form the PIFA feed wire. The outer conductor of the coax is soldered to the edge of a small hole drilled in the ground plane at the feed point. The volume between the radiating plate and the ground plan is filled by air except a thin region 0.8 mm under the radiating patch who is composed of FR4 epoxy ($\epsilon_r = 4.4$).

2.2. The Choice of the Patch Dimensions

It is very important for simulation by HFSS to estimate the resonant frequency that help the simulator to make a refinement mesh in a band around the resonant frequency and then give more precise values. The resonant frequency of a PIFA is approximated by the Equation (1) [5] where F_r is the resonant frequency, C is the light velocity.

$$F_r = \frac{C}{4(L_p + W_p - W_s)} \tag{1}$$

If there is another substrate different from Air, C will be $C_0/\sqrt{\epsilon_r}$ where $C_0 = 3 \times 10^8$ m/s. For our case, the space between the patch and the ground plan is essentially air minus a 0.8 mm FR4 epoxy layer.

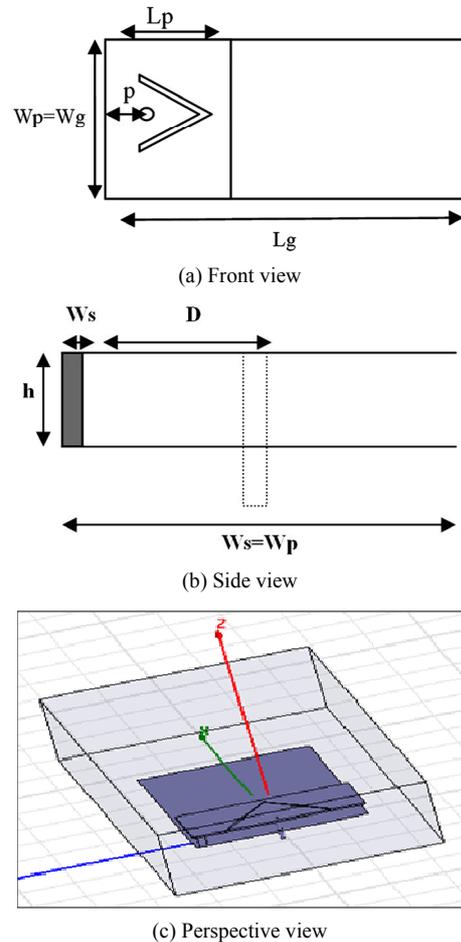


Figure 1. Different view of the designed antenna.

To compute the resonant frequency, we have the following values: $L_p = 29.3$ mm, $W_p = 64$ mm, $W_{S_{max}} = 3$ mm. The theoretical F_r is 830 MHz. The obtained frequency is then not far from 1920 MHz the central frequency of GSM900 band. In fact, there is no equation to determine the resonant frequency for a PIFA that contains not only the patch dimensions but also the other parameters that can affect the antenna characteristics. For this, the author will make constant the patch dimensions that are the mean parameters can furnish the resonant frequency and he will vary undependably the other parameters (ground plan dimensions L_g , height of radiating plate h , feeding point position p , shorting plate Width W_s and position D).

2.3. The Choice of the Simulator

HFSS (High Frequency Simulator Structure) is a high performance full wave electromagnetic (EM) field simulator for arbitrary 3D volumetric passive device modeling that takes advantage of the familiar Microsoft Windows graphical user interface. It integrates simulation, visualization, solid modeling, and automation in an easy to

learn environment where solutions to 3D EM problems are quickly and accurate obtained. Ansoft HFSS employs the Finite Element Method (FEM), adaptive meshing, and brilliant graphics to give unparalleled performance and insight to all of 3D EM problems. Ansoft HFSS can be used to calculate parameters such as S-Parameters, Resonant Frequency and Fields. Typical uses include Package Modeling, PCB Board Modeling, Mobile Communications (Patches, Dipoles, Horns, and Conformal Cell Phone Antennas), Specific Absorption Rate (SAR), Infinite Arrays, Radar Section (RCS), Frequency Selective Surface (FSS) and filters such Cavity Filters, Microstrip, Dielectric. HFSS is an interactive simulation system whose basic mesh element is a tetrahedron T. In industry, Ansoft HFSS is the tool of choice for High productivity research, development, and virtual prototyping [6].

The HFSS is then used in our simulation; the author proposes after exposing the results of the HFSS simulations.

2.4. The Choice of the Height h

The height h is the distance between the top plate and the ground plane. In order to eliminate the effects of the ground plane, the patched is placed on the edge of an infinite ground plane (in HFSS, the choice the infinite ground plan can made during defininig boundaries) at a height varying from 6 mm to 13 mm. From the simulation result shown by **Figure 2** for GSM900 band, the heights 10 and 11 mm present important S_{11} values and closer to central frequency. It is then necessary to look if they are adequate to DCS band also. From result shown in **Figure 3**, $h = 11$ mm is a very interesting height (it will be nearly the handset thickness).

2.5. The Choice of the Ground Plan Length L_g

The height h is taken equal to 11 mm. Then, a variation of the ground plane length L_g is made from 70 mm to 120 mm. This sweep is taken because the designed antenna will be mounted on a GSM handset. The **Figures 4** and **5** show the result of the parametric simulation. The curve corresponding to the length 80 mm is the most adapted (the closest to DCS central frequency and is a S_{11} peak for GSM900). In reality, the simulation shows close results for the lengths 80 mm, 90 mm and 100 mm. Also, 120 mm and over can be considered not interesting values for a ground plane in a handset. Then, $L_g = 80$ mm. In the following, the other parameters effects are discussed.

2.6. The Choice the Shorting Plate Position D , Width W_s and Feeding Point Position

The three parameters D , W_s and p have approximately comparable effect intensity. Theses parameters will vary simultaneously. The shorting plate position D from 28

mm to 31 mm, the width W_s from 1 to 3 mm, the feeding point p from 3 to 7 mm from the patch edge. The number of possible configuration is $4 \times 3 \times 5 = 60$. The intervall sweep must be chosen correctly if not the simulation can be costly in computing and memories ressources. The **Figure 4** shows the results of the tri-parametric simulation for GSM900 band. From **Figure 4**, there is a curve

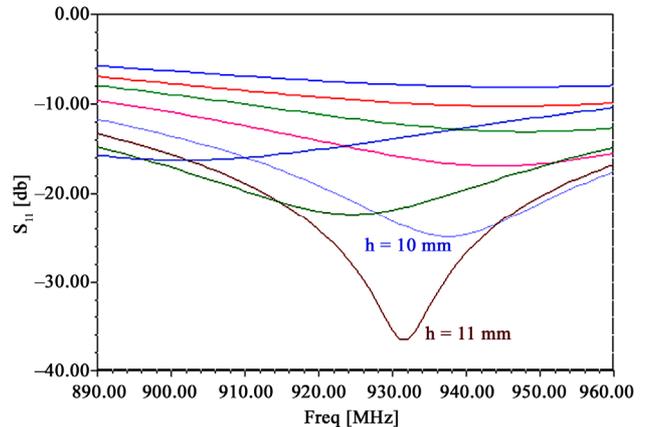


Figure 2. h -parametric simulation for GSM band.

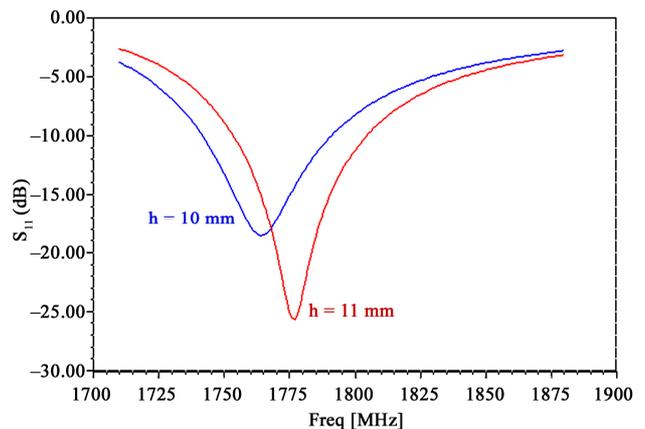


Figure 3. h -parametric simulation for DCS.

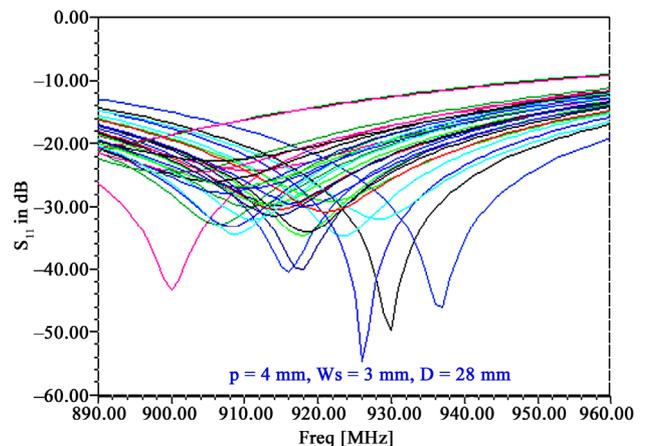


Figure 4. Tri-parametric simulation for GSM900 band.

that present minimal S_{11} values and very close to the central frequency 926 MHz. The corresponding configuration is ($p = 4$ mm, $D = 28$ mm, $W_s = 3$ mm). It's now important to check the simulation result for DCS band. The result is shown in **Figure 5**. Except of some values, the effect of different parameters are very close in this band. It is then easy to verify that our chosen configuration for GSM is also adequate for DCS band. The result shown by **Figure 6** is interesting because it presents a S_{11} peak near 1800 MHz.

3. The Designed Antenna Characterization

The dimensions of the designed bi-band antenna are summarized in the **Table 1**. We will now present the antenna characteristics.

3.1. The Reflection Loss

The **Figure 7** shows the S_{11} parameter function of frequency in [0 - 2.4 GHz].

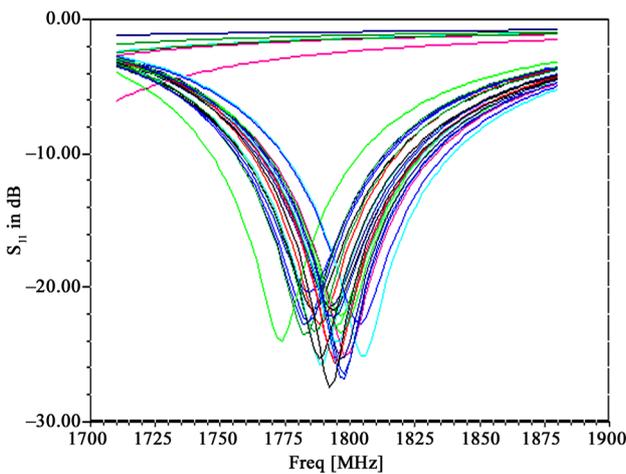


Figure 5. Tri-parametric simulation for DCS band.

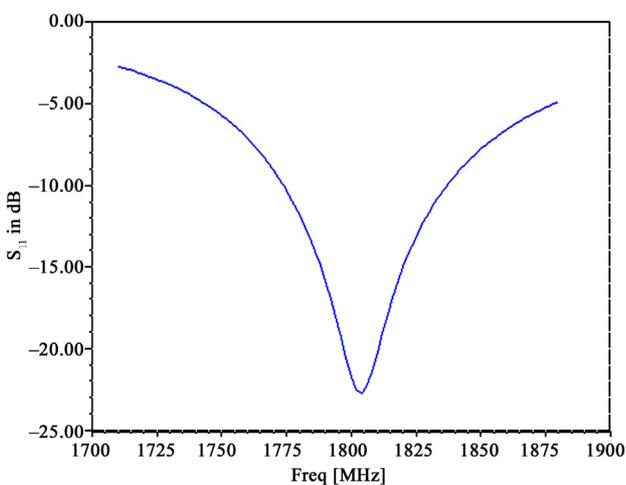


Figure 6. The chosen configuration in DCS band.

Table 1. The designed antenna dimensions.

Antenna parameter	Value of the parameter (mm)
Patch length L_p	29.3
Patch width W_p	64
Ground plan length L_g	80
Ground plan width W_g	64
Height h	11
Short plate width W_s	3
Short plate position D	28
Feeding point position	4

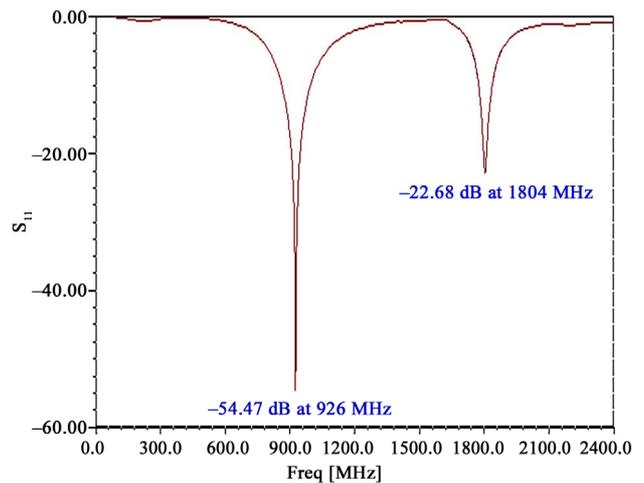


Figure 7. S_{11} depending on frequency for [0 - 2400 MHz].

There are two peaks of S_{11} parameter in the curve of **Figure 7**. The first peak is around 926 MHz (very close to the GSM900 central frequency 925 MHz), and the second peak is around 1804 MHz (very close to the DCS central frequency 1995 MHz). Also, the S_{11} values out of both bands are near 0. That means the designed antenna can't interfere with other radiations. We can also run the simulation by refining the sweep interval for more precision. As given exactly by simulations tables, we note $S_{11} = -14.71$ dB for 890 MHz (the low frequency of the GSM900 band), $S_{11} = -15.68$ dB for 960 MHz (the high frequency of the GSM900 band), $S_{11} = -3$ dB for 1710 MHz (the low frequency of the DCS band), $S_{11} = -5$ dB for 1880 MHz (the high frequency of the DCS band). The designed antenna has a S_{11} litter than -14.71 dB for the first band and better than -3 dB for second band.

3.2. The VSWR and Bandwidth the Diagram Pattern

We obtain as shown in **Figure 8** for GSM900 band a VSWR = 1.45 for 890 MHz (the lowest frequency), VSWR_{min} = 1.003 for 926 MHz (the resonant frequency), VSWR = 1.39 for 960 MHz (the highest frequency). The VSWR is at its minimum. It's a very interesting result. Also, The GSM bandwidth (70 MHz) is for the designed antenna a 1:1.45 VSWR bandwidth and the antenna presents a 1:2 bandwidth equal to 140 MHz. It is considered a very interesting result. Also, we obtain as shown in **Figure 9** for DCS band a VSWR = 6.39 for 1710 MHz (the lowest frequency), VSWR_{min} = 1.15 for 1922 MHz (the resonant frequency), VSWR = 3.62 for 1880 MHz (the highest frequency). The VSWR is at its minimum for the resonant frequency. It's a very interesting result. Also, the antenna presents a 1:2 VSWR bandwidth equal to 70 MHz.

3.3. The Smith Chart

The **Figure 10** shows a regular Smith chart with interesting parameters of reflection, impedance, VSWR, and Q.

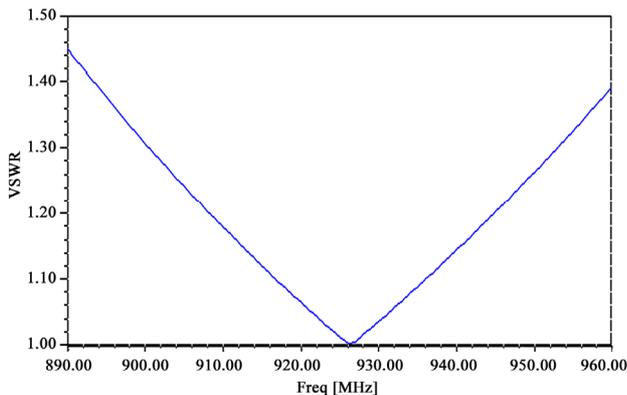


Figure 8. VSWR depending on the frequency for the GSM900 band.

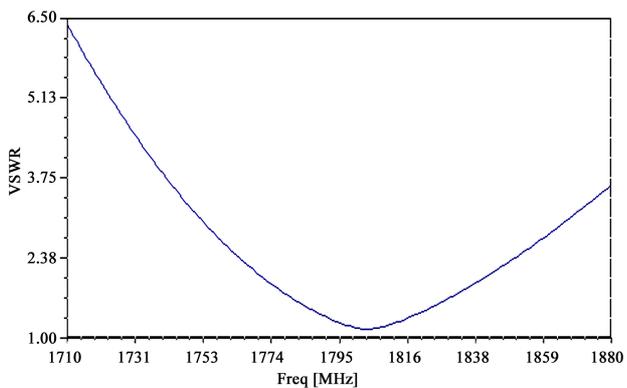


Figure 9. The VSWR depending on the frequency for the DCS1800 band.

3.4. The Impedance in the Feeding Point

From the **Table 2** and **Figure 10**, we can see very close values between the impedances (port impedance Z_0 and feeding point impedance). The feeding point position is then confirmed that is compliant because it presents a very interesting adaptation.

3.5. The Antenna Parameters

The simulations results shown in **Figure 11** give the antenna parameters. The obtained peak gain G is 12.84 dB and peak directivity equal to 15.16 dB; the radiation efficiency is 0.847. We can confirm by the **Figure 12** that (xz) is the E-plane and its maximum is for ($\phi = 0$ deg and $\theta = 0$ deg). Also, the antenna has regular polar diagram as shown in **Figure 13**.

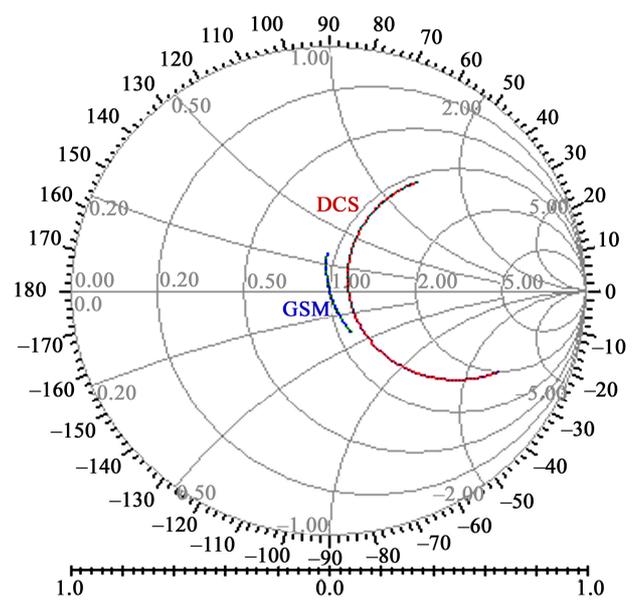


Figure 10. The impedance smith chart for both bands.

Table 2. The impedances table.

Frequency (MHz)	Impedance Z (Magnitude in dB)	Port impedance Z_0 (Magnitude in dB)
890	41.40	35.24
927	35.24	35.24
960	34.64	35.24
1710	7.59	35.24
1809	40.53	35.24
1880	63.07	35.24

Antenna Parameters:			
	Quantity	Value	Units
	Max U	0.81059	W/sr
	Peak Directivity	15.166	
	Peak Gain	12.846	
	Peak Realized Gain	10.186	
	Radiated Power	0.67167	W
	Accepted Power	0.79298	W
	Incident Power	1	W
	Radiation Efficiency	0.84702	
	Decay Factor	0	

Figure 11. Antenna parameters as given by HFSS.

Maximum Field Data:					
	rE Field	Value	Units	At Phi	At Theta
	Total	24.722	V	360deg	0deg
	X	24.722	V	360deg	0deg
	Y	2.4191	V	310deg	40deg
	Z	6.2508	V	10deg	30deg
	Phi	24.722	V	270deg	0deg
	Theta	24.722	V	360deg	0deg
	LHCP	17.481	V	350deg	0deg
	RHCP	17.481	V	330deg	0deg
	Ludwig3/X dominant	24.722	V	360deg	0deg
	Ludwig3/Y dominant	1.3207	V	310deg	40deg

Figure 12. Maximum field data as given by HFSS.

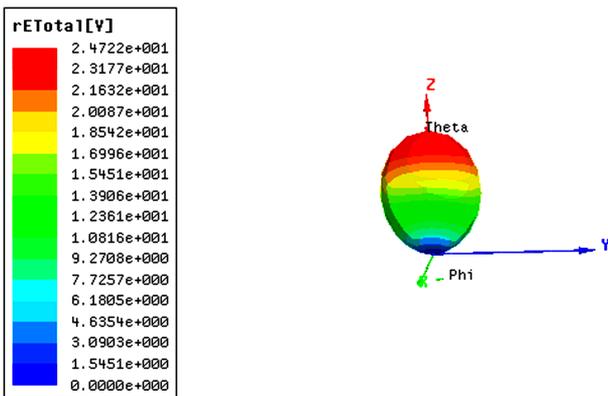


Figure 13. The E-field 3D polar diagram pattern.

4. Conclusions

To design a bi-band PIFA for GSM900/DCS1800 bands, the author adopted a methodology based on parametric simulations. The design process allows the following conclusions:

1) The PIFA characteristics are affected by each of the changed parameter (the height of the radiating plate, the ground plane length, the position and width of the short plate, the position of the feeding point) in compatibility with precedent studies [7].

Table 3. The design antenna parameters and dimensions.

Antenna parameter	Value of the parameter GSM900, DCS1800
Patch Length L_p	29.3 mm
Patch width W_p	64 mm
Ground plan length L_g	80 mm
Ground plan width W_g	64 mm
Height h	11 mm
Short plate width W_s	3 mm
Short plate position D	28 mm
Feeding point position	4 mm
Resonant frequency	926 MHz , 1804 MHz
Peak S_{11}	-54.5 dB, -22.7 dB
1:1.2 VSWR bandwidth	140 MHz, 70 dB
Peak Gain	12.85 dB
Peak Directivity	15.17 dB
Radiation efficiency	85%
E total max	Phi = 0 deg , Theta = 0 deg

2) It's interesting in the design of the PIFA to search an effective solution not the optimal one. In fact, difference will be very little (like for DCS but not GSM) and also, the values of the PIFA dimensions must be practical (one decimal) not theoretical. The Important is the fact that the solution respects the requirements.

3) We must look for a solution compliant simultaneously for both bands. In fact, during simulation, an enhancement in one band affects negatively another band. A trade-off solution was chosen.

4) The designed PIFA for GSM use respects the requirements especially for the resonant frequency, the VSWR, the bandwidth, the reflection coefficient, the anisotropy and the miniaturization. A bandwidth enhancement for DCS band can be handled.

5) In comparison with precedent designed PIFA [3,4] for different frequency bands, the antenna presents a very high gain and directivity and also an interesting radiation efficiency.

The **Table 3** summarizes the characteristics and dimensions of the designed antenna. The analysis of those results makes from our designed antenna a succeeded trade-off that respects GSM requirements.

REFERENCES

- [1] K. L. Wong, "Introduction and Overview," In: K. L. Wong, Ed., *Planar Antennas for Wireless Communications*, J. Willy and Sons, Hoboken, 2003, p. 1
- [2] K. L. Virga and Y. Rahmat-Samii, "Low-Profile Enhanced Bandwidth PIFA for Wireless Communications Packaging," *IEEE Transactions on Microwave Theory and Techniques*, Vol. 45, No. 10, 1997, pp. 1879-1888. [doi:10.1109/22.641786](https://doi.org/10.1109/22.641786)
- [3] W.-J. Liao, T.-M. Liu and S.-Y. Ho, "Miniaturized PIFA Antenna for 2.4 GHz ISM Band Applications," *IEEE Proceedings of the 6th European Conference on Antennas and Propagation (EUCAP)*, Prague, March 2012, pp. 3034-3037.
- [4] A. K. Skrivervik, J.-F. Zürcher, O. Staub and J. R. Mosig, "PCS Antenna Design: The Challenge of Miniaturization," *IEEE Antennas and Propagation Magazine*, Vol. 43, No. 4, 2001, pp. 12-27. [doi:10.1109/74.951556](https://doi.org/10.1109/74.951556)
- [5] PIFA: The Planer Inverted F Antenna. <http://www.antenna-theory.com/antennas/patches/pifa.php>
- [6] Ansoft Corporation, "HFSS 10.0 User's Guide," Ansoft Corporation, Pittsburg, 2005.
- [7] H. T. Chattha, Y. Huang, M. K. Ishfaq and S. J. Boyes, "A Comprehensive Parametric Study of Planar Inverted-F Antenna," *Wireless Engineering and Technology*, Vol. 3, 2012, pp. 1-11. [doi:10.4236/wet.2012.31001](https://doi.org/10.4236/wet.2012.31001)