

# ICI Performance Analysis for All Phase OFDM Systems

Renhua Ge<sup>1</sup>, Shanlin Sun<sup>1,2</sup>

<sup>1</sup>Guilin College of Aerospace Technology, Guilin, 541004, China; <sup>2</sup>Tianjin University, Tianjin, 300072, China.  
Email: grh1962@163.com

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## ABSTRACT

Orthogonal frequency division multiplexing (OFDM) is a strong candidate for the next generation wireless communication. But the frequency offset between the local oscillators at the transmitter and receiver causes a single frequency offset in the signal, while a time-varying channel can cause a spread of frequency offsets known as the Doppler spread. Frequency offsets ruin the orthogonal of OFDM sub-carriers and cause inter-carrier interference (ICI), therefore, quickly diminishing the performance of the system. A novel all phase OFDM (AP-OFDM) system is established. APFFT is introduced for the first time to overcome ICI aroused by carrier frequency offset (CFO) in OFDM systems. This scheme makes use of APFFT in time domain and zero inserting in frequency domain to reduce the amount of ICI generated as a result of frequency offset, with little additional computational complexity. At the same time, the proposed system has zero phase error. It is proved to be correct and effective in mathematics. The simulation results indicate that AP-OFDM system has a better performance than conventional OFDM system.

**Keywords:** All Phase Orthogonal Frequency-division Multiplexing (APOFDM), Carrier Frequency Offset (CFO), Inter-carrier Interference (ICI)

## 1. Introduction

Orthogonal frequency-division multiplexing (OFDM) communication systems require precise frequency synchronization [1-4], since otherwise inter-carrier interference (ICI) will occur. Currently, three different approaches for reducing ICI have been developed in the literature. One is to estimate and remove the frequency offset [3-7]. While many methods exist that can estimate and remove the frequency offset quite accurately, they often have considerable computational complexity. Another approach is to use signal processing and/or coding to reduce the sensitivity of the OFDM system to the frequency offset [8]. These methods can either be used as low complexity alternatives to fine frequency-offset estimation techniques or they can be used together with a somewhat accurate oscillator. Windowing has been used in [9] and [10] to reduce the ICI created as a result of frequency offset. A simple and effective method known as ICI self-cancellation scheme [11,12] has been proposed by Zhao and Haggman. Other frequency-domain coding methods have been proposed in [13,14] that do not reduce the data rate. However, these methods produce less reduction in ICI. A new self-cancellation scheme has been proposed by Alireza, Seyedi and Saulnier [15]. This method has better performance with more computational complexity.

This paper concentrates on the further development of the ICI cancellation method and APFFT is proposed for ICI cancellation. The advantages of APFFT are zero phase error and less ICI. It improves the OFDM system's ability to resist frequency offset with the cost of limited additional computational complexity.

## 2. The Model of APOFDM System

In conventional FFT system, the spectrum of the receiver signal can expressed as [16].

$$X(k) = \frac{1}{N} \frac{\sin(\pi(k+\varepsilon))}{\sin(\pi(k+\varepsilon)/N)} e^{-j(N-1)(k+\varepsilon)\pi/N} \cdot e^{j\varphi_0} \quad (1)$$

where  $\varepsilon$  is the normalization frequency offset. Thus, the amplitude spectrum is:

$$|X(k)| = \left| \frac{1}{N} \frac{\sin(\pi(k+\varepsilon))}{\sin(\pi(k+\varepsilon)/N)} \right| \quad (2)$$

And the phase spectrum is:

$$\varphi_1 = -\frac{N-1}{N}(k+\varepsilon)\pi + \varphi_0 \quad (3)$$

Frequency offset can introduce ICI and phase noise and diminish the performance of the system Figure 1

shows the block of APOFDM. Figure 2 is the N-all phase FFT circuit [16,17].

Assuming that  $X = \{X(k), k = 0, 1, \dots, N-1\}$  is the complex digital sequence in frequency domain and

$$x(n) = IFFT(X(k)) = \frac{1}{N} \sum_{k=-N/2-1}^{N/2-1} X(k) e^{j\frac{2\pi kn}{N}}. \text{ After zero}$$

interval interpolation, we obtain sequence

$$X' = \{X'(k), k = 0, 1, 2, \dots, 2N-1\} \text{ and}$$

$$X'(k) = \begin{cases} X\left(\frac{k}{2}\right), & k = 0, 2, \dots, 2(N-1) \\ 0, & k = 1, 3, 5, \dots, 2N-1 \end{cases}$$

The number of the point for the new sequence is  $2N$ , so  $2N$ -IFFT should be implemented.

$$x'(n) = \frac{1}{2N} \sum_{k=0}^{2N-1} X'(k) W_{2N}^{-kn} = \frac{1}{2N} \sum_{m=0}^{N-1} X(2m) W_{2N}^{-2mn}, \quad n=0,1,\dots,2N-1 \quad (4)$$

$$x'(n+N) = \frac{1}{2N} \sum_{k=0}^{2N-1} X'(k) W_{2N}^{-2k(n+N)}$$

$$\begin{aligned} &= \frac{1}{2N} \sum_{m=0}^{N-1} X(2m) W_{2N}^{-2mn} \cdot W_{2N}^{-2N} \\ &= \frac{1}{2N} \sum_{m=0}^{N-1} X(2m) W_{2N}^{-2mn} = x'(n), \quad n=0,1,\dots,2N-1 \end{aligned} \quad (5)$$

The purpose of zero interval interpolation in frequency is to obtain the copy of  $N$  subcarriers of OFDM systems and keep the number of subcarriers unchangeable. Therefore, the former  $N$  points are the copy of the last  $N$  points in time domain. These  $2N$  points are indispensable to APFFT. That is to say, in receiver, we only need two times clock sample compared with FFT system to get APFFT sequence in time domain.

To digital sequence with  $2N$  points, the first point  $x(0)$  is removed and the remaining sequence can be expressed as  $x(1), x(2), \dots, x(N-1), x(N), x(N+1), x(N+2), \dots, x(2N-1)$ . In this digital sequence, we can obtain  $N$  sub-sequences and each of them has  $N$  points including  $x(N)$ . Then, every sub-sequence with a recycling style is moved. Finally, the point  $x(N)$  is moved to the first place and then

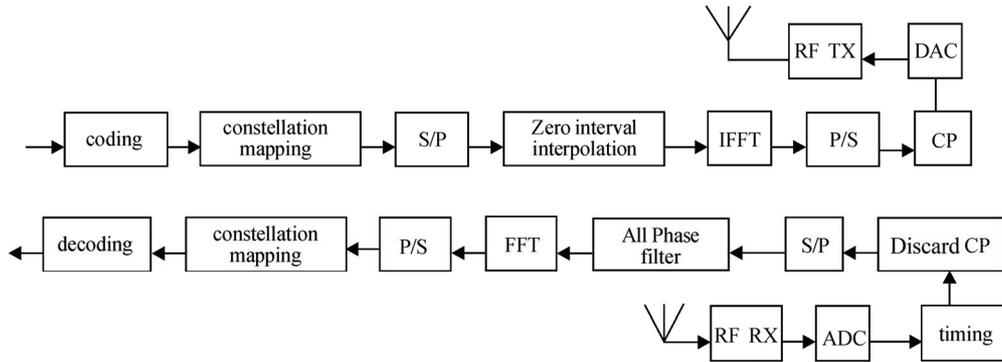


Figure 1. The block of APOFDM system

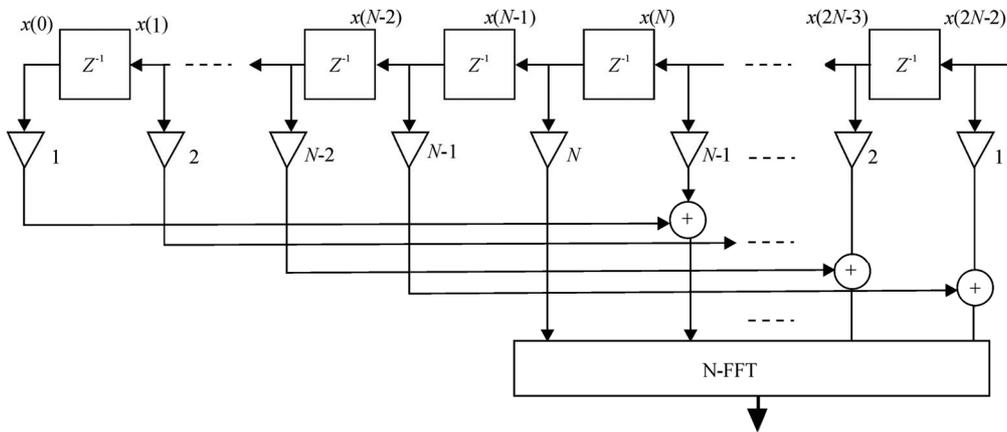


Figure 2. The block of N-step APFFT

get the others  $N$  sub-sequences with  $N$  points. Making them aligned and adding them, a new  $N$  points sequence is obtained, which is called all-phase digital sequence.

For instance,  $N=4$  and  $2N-1=7$ , we can get the sequence  $x(1), x(2), x(3), x(4), x(5), x(6), x(7)$ . This sequence can be divided into 4 sub-sequences.

1<sup>st</sup> section:  $\{x(1), x(2), x(3), x(4)\}$ , 2<sup>nd</sup> section:

$\{x(2), x(3), x(4), x(5)\}$ , 3<sup>rd</sup> section:  $\{x(3), x(4), x(5), x(6)\}$ ,

4<sup>th</sup> section:  $\{x(4), x(5), x(6), x(7)\}$ . After cycle moving,

we obtain:  $\{x(1), x(2), x(3), x(4)\}$ ,  $\{x(5), x(2), x(3), x(4)\}$ ,

$\{x(5), x(6), x(3), x(4)\}$  and  $\{x(5), x(6), x(7), x(4)\}$ . We

add them together with parallelism principle and normalize them. The AP digital sequence can be expressed as

$$\left\{ \frac{1}{4}(x(1) + 3x(5)), \frac{1}{4}(2x(2) + 2x(6)), \frac{1}{4}(3x(3) + x(7)), \frac{1}{4}(4x(4)) \right\}.$$

Now, we analyze the connection between  $X(k)$  and  $X'(k)$ . According to the character of discrete Fourier transform,  $X'(k)$  is the FFT of sequence  $x(1), x(2), \dots, x(N)$  cycle moving in time domain. Thus

$$X'(k) = X(k) e^{j \frac{2\pi k i}{N}}, \quad i = 0, 1, \dots, N-1 \quad (6)$$

where  $X(k) = \sum_{n=0}^{N-1} x(n) e^{-j 2\pi k n / N}$  ( $k = 0, 1, \dots, N-1$ ). The

spectrum of APFFT is the sum of  $X'(k)$ , thus:

$$X_{AP}(k) = \frac{1}{N} \sum_{i=0}^{N-1} X'(i) = \frac{1}{N} \sum_{i=0}^{N-1} X(i) e^{j 2\pi k i / N} \quad (7)$$

Supposing that  $x(n) = e^{j(\frac{2\pi k_0 n}{N} + \varphi_0)}$ , is a single frequency complex signal, thus,

$$\begin{aligned} X_{AP}(k) &= \frac{1}{N^2} e^{j\varphi_0} \sum_{i=0}^{N-1} \left[ \sum_{m=0}^{N-1} x(m) e^{-j \frac{2\pi k m}{N}} \right] e^{j \frac{2\pi k i}{N}} \\ &= \frac{1}{N^2} e^{j\varphi_0} \cdot \sum_{i=0}^{N-1} e^{-j 2\pi (k_0 - k) i / N} \cdot \sum_{m=0}^{N-1} e^{j 2\pi (k_0 - k) m} \\ &= \frac{1}{N^2} e^{j\varphi_0} \frac{1 - e^{-j 2\pi (k_0 - k) / N}}{1 - e^{-j 2\pi (k_0 - k) / N}} \cdot \frac{1 - e^{j 2\pi (k_0 - k) / N}}{1 - e^{j 2\pi (k_0 - k) / N}} \\ &= \frac{1}{N^2} e^{j\varphi_0} \frac{e^{j\pi (k_0 - k)} - e^{-j\pi (k_0 - k)}}{e^{j\pi (k_0 - k) / N} - e^{-j\pi (k_0 - k) / N}} \cdot \frac{e^{-j\pi (k_0 - k)} - e^{j\pi (k_0 - k)}}{e^{-j\pi (k_0 - k) / N} - e^{j\pi (k_0 - k) / N}} \\ &= \frac{1}{N^2} e^{j\varphi_0} \frac{\sin^2(\pi (k_0 - k))}{\sin^2(\pi (k_0 - k) / N)} \end{aligned} \quad (8)$$

Thus, the normalized spectrum of APFFT is

$$X_{ap}(k) = \frac{1}{N^2} e^{j\varphi_0} \frac{\sin^2(\pi (k + \varepsilon))}{\sin^2(\pi (k + \varepsilon) / N)} \quad (9)$$

Having taken into account all the combinations of  $N$  points sequence including  $x(N)$ , the plus phase error and the minus of  $x(N)$  offset each other, thus the phase error is zero.

Figure 3 is the spectrum of the same signal with FFT and APFFT respectively. ICI caused by CFO has more difference between them. The ICI of FFT is higher than that of APFFT.

Figure 4 is the phase and amplitude spectrum of OFDM and APOFDM systems with frequency offset 0.05. From Equation (1), (9), Figure 3 and Figure 4, we can indicate that, with APFFT, the phase error of the receiver signal is 0 and the normalized ICI power is the square of that of FFT signal. Therefore, its sensitivity to

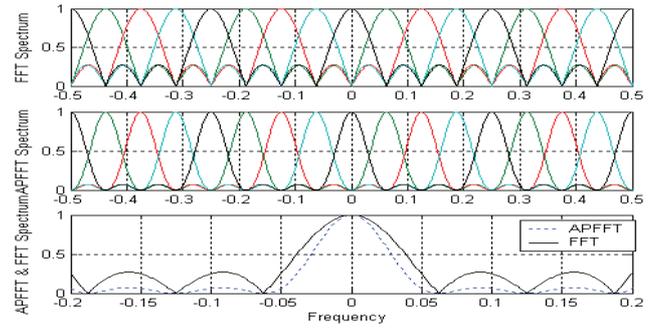


Figure 3. Signal spectrum of APFFT and FFT

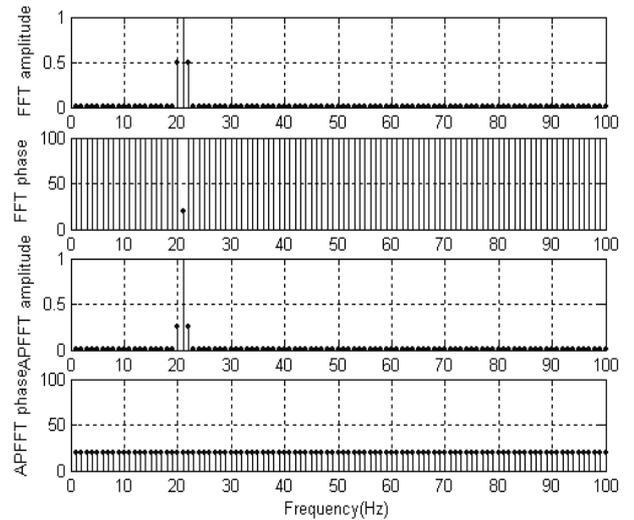


Figure 4. Phase and amplitude spectrum of signal  $s = \exp(j(\omega t \cdot 20/N + 20\pi/180))$  with APFFT and FFT, frequency offset is 0.05

ICI caused by CFO is lower and APFFT is more suitable for OFDM system.

### 3. Performance Analysis for AP-OFDM Systems with CFO

The change of performance duo to CFO is more interested in the research content. In this section we use a method similar to the one used in [16] to calculate the exact BER of the proposed system in the presence of a frequency shift. We assume that the system operates over an AWGN channel and that the data symbols are quaternary phase-shift keying (QPSK) modulated. Similar analysis is possible if a 64-QAM modulation is used [16]. We assume an ideal additive white Gaussian noise (AWGN) channel. The CFO does not change during one OFDM symbol. The sampled signal for the  $k$ th sub-channel after the receiver fast Fourier transform processing can be written as:

$$y_k = X_k S_0 + \sum_{l=0, l \neq k}^{N-1} S_{l-k} X_l + n_k, k = 0, 1, \dots, N-1 \quad (10)$$

where  $X_k \in \left\{ \begin{array}{l} \pm 1 \pm j, \pm 1 \pm 3j, \pm 1 \pm 5j, \pm 1 \pm 7j, \\ \pm 3 \pm j, \pm 3 \pm 3j, \pm 3 \pm 5j, \pm 3 \pm 7j, \\ \pm 5 \pm j, \pm 5 \pm 3j, \pm 5 \pm 5j, \pm 5 \pm 7j, \\ \pm 7 \pm j, \pm 7 \pm 3j, \pm 7 \pm 5j, \pm 7 \pm 7j \end{array} \right\}$  denotes

the transmitted symbol for the  $k$ th sub-carrier,  $n_k$  is a complex Gaussian noise sample (with its real and imaginary components being independent and identically distributed with variance  $\sigma^2$ ), and  $N$  is the number of sub-carriers. The second term in (12) is the ICI caused by the CFO. The sequence  $S_k$  (ICI coefficients) depends on the CFO and is given by

$$S_k = X_{AP}(k) = A \left| \frac{1}{N} \frac{\sin(\pi(k+\varepsilon))}{\sin(\pi(k+\varepsilon)/N)} \right|^2 e^{j\theta_0} \quad (11)$$

If the ICI assumed to be a Gaussian-distributed random variables (RV) with a zero mean, both the BER and SER can readily be computed for various modulation formats. The approximate error rates then can be expressed in terms of the  $Q(\cdot)$  function and effective SNR for the  $k$ th sub-carrier as

$$\gamma_{eff} = \frac{|S_0|^2 \gamma_s}{1 + \gamma_s \sigma_{APICI}^2} \quad (12)$$

where  $\gamma_s = E|X_k|^2 / \sigma^2$  which is the SNR for the  $k$ th sub-carrier in the absence of a CFO. The variance of the signal constellation  $E|X_k|^2$  will be independent of if all sub-carriers use the same modulation format, which is the normal case. The variance of the ICI on the  $k$ th sub-carrier can be given by

$$\sigma_{APICI}^2 = \sum_{l=0, l \neq k}^{N-1} |S_{l-k}|^2 \quad (13)$$

Compared with FFT-OFDM systems [16], the variance of the ICI of APFFT-OFDM systems can be expressed by

$$\begin{aligned} \hat{\sigma}_{APICI}^2 &= \frac{1}{N} \sum_{n=0}^{N-1} \text{var}[X_{AP}(n)] = \frac{\hat{\sigma}_{ICI}^2}{N} \sum_{n=0}^{N-1} \left[ \left( \frac{N-n}{N} \right)^2 + \left( \frac{n}{N} \right)^2 \right] \\ &= \frac{\hat{\sigma}_{ICI}^2}{N^3} \sum_{n=0}^{N-1} (N^2 + n^2 - 2nN) \\ &= \frac{\hat{\sigma}_{ICI}^2}{N^3} \left[ N^3 + \frac{N(N-1)(2N-1)}{6} - 2N \cdot \frac{N(N-1)}{2} \right] \\ &= \frac{2N^2 + 1}{3N^2} \hat{\sigma}_{ICI}^2 \approx \frac{1}{3} \hat{\sigma}_{ICI}^2 \end{aligned} \quad (14)$$

Equation (14) shows that, after APFFT, the ICI noise to every sub-carrier is the third of that in FFT system. Using the method in [16], the effect caused by CFO can be expressed with the losing of SNR.

$$D = \frac{10}{\ln 10} \frac{1}{3} (\pi \varepsilon)^2 \gamma_s \quad (15)$$

## 4. APOFDM Performance Test with Simulation

### 4.1 The Design Based SIR

According to the method of ICI cancellation in [15], we choose  $N=64$ ,  $L=2$ ,  $M=1$  and  $SIR_{min}=25\text{dB}$  to design a system and compare its performance with FFT system, Zhao-Haggman ( $L=2$ ) system and A-Seyedi system. Figure 5 shows that the performance of APFFT is better than FFT and Zhao-Haggman ( $L=2$ ) systems in low frequency offset, and poorer in high frequency offset. We will only be interested in frequency shifts in the range  $|\varepsilon| \leq 0.5$ .

### 4.2 The Design Based BER

As SIR can not represent the system performance, and the result in Figure 6 obtained before frequency compensation, thus the APFFT-OFDM system SIR can not necessarily better than the other existing systems. The model method in [12] is used and all phase compensation is adopted, BER performances are compared in Figure 6. The parameters are same to the above. Assuming that channel is pilot and the pilot frequency account for 20% of the symbol. The CFO is 0.5. From Figure 6, when  $\text{BER}=10^{-4}$ , APFFT is better than Zhao-Haggman system and A. Seyedi system 1.1 dB and 0.8 dB respectively. This is because of the zero phase error of APFFT with CFO. Equation (14), Figure 3 and Figure 4 can prove it to be correct. That is to say, the simulation and the theory are consistent.

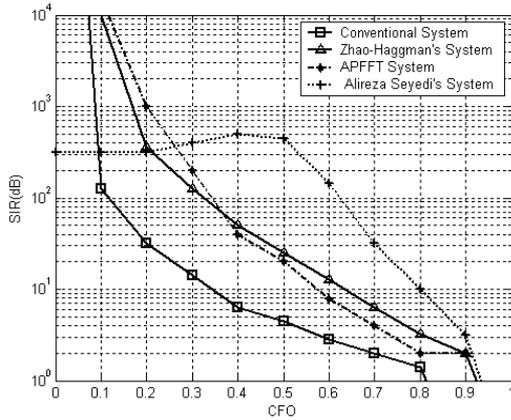


Figure 5. The correction between SIR and normalization frequency offset in ideal AWGN

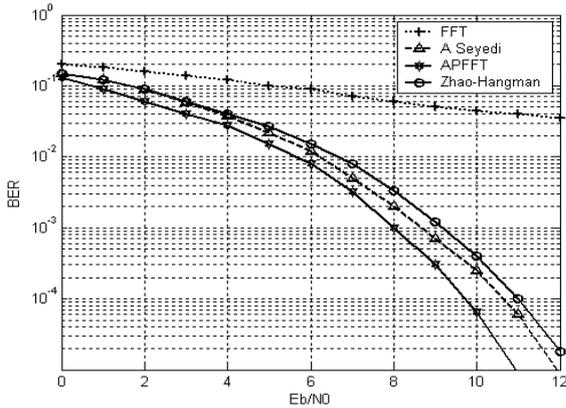


Figure 6. Calculated and simulated BER for the FFT system, Zhao-Haggman system, A. Seyedi system and APFFT system over an AWGN channel with perfect equalization

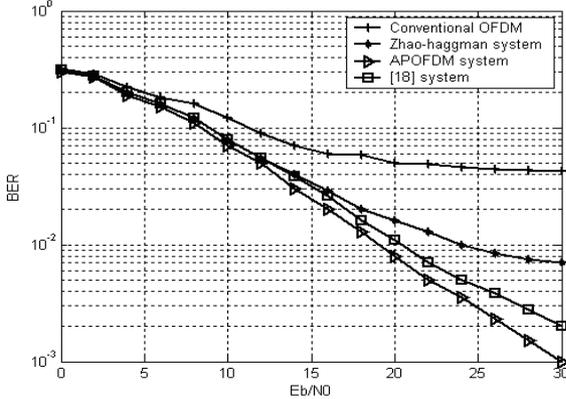


Figure 7. BER of FFT, Zhao-Haggman, A. Seyedi and APFFT-OFDM system over a frequency-selective Channel

4.3 BER of Frequency-Selective System

APFFT can not estimate the CFO but can reduce the sensitivity to CFO. Thus, it is true that APFFT is more suited to the OFDM system. In a frequency-selective channel, 4 sub-paths are chosen to establish channel model and

every sub-path attenuation coefficient accord with Rayleigh distribution. Channel model and Power spectral density are the same with [18]. The cyclic prefix is  $T_{CP} = T/8$ . Figure 7 shows that, when channel is perfect, the lowest BER varies considerably in all the schemes we have mentioned above. The BER of APOFDM is best.

5. Conclusions

The amplitude of FFT has the character of function *sinc* in frequency domain. Moreover, the amplitude spectrum of APFFT is the square of function *sinc*. At the same time, the phase of FFT can change with CFO but APFFT can not. The plus phase error and minus phase error balance out each other, thus, the phase error of APFFT is zero. So, APFFT is more suitable for OFDM system. Compared with conventional OFDM system, APFFT reduce the sensitivity of system to CFO. In this paper, AP-OFDM system is established, the character of ICI cancellation in OFDM system is proved in mathematics, and the methods in [15] are used to analyze the performance of APOFDM system. Through Monte Carlo simulations, we have shown that the proposed system has better performance in the presence of an oscillator frequency offset or when ICI is created as a result of channel fading. Significantly larger gains are achieved when the equalization process is imperfect.

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