

Preparation of Composite Particles Made of Biodegradable Polymer and a Few Additives with Phase Separation Followed by Drying-in-Liquid

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Abstract

It was tried to prepare the biodegradable composite particles by the phase separation method followed by the drying-in-liquid method. The composite particles were made of poly- ϵ -caprolactone, quaternary ammonium, carbon black and wax. In the experiment, acetone and water were selected as a good solvent and a poor solvent for poly- ϵ -caprolactone, quaternary ammonium and wax, respectively. The composite particles were prepared by changing the surfactant species and their concentration, the feeding velocity of water and the weight ratio of poly- ϵ -caprolactone with larger molecular weight to one with smaller molecular weight. The composite particles with the inner structure in which carbon black, quaternary ammonium and wax were coated well with poly- ϵ -caprolactone could be prepared by the preparation method presented in this study. The structure and the mean diameter of composite particles were strongly affected by the feeding velocity of water. The higher the feeding velocity of water, the larger the mean diameter of composite particles. The mean diameter was drastically decreased with the surfactant concentration and increased with the added amount of poly- ϵ -caprolactant with larger molecular weight.

Keywords

Biodegradable Composite Particles, Phase Separation, Drying-in-Liquid, Poly- ϵ -Caprolactone, Microencapsulation

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1. Introduction

Many kinds of composite particles have been prepared by various preparation methods and applied in many fields such as information recording materials, paintings, writing materials, adhesive, cosmetics, food industry, medicine and so on [1] [2]. These composite particles could be prepared by using inorganic, organic and polymeric materials and by combining these elementary materials. We can give a single composite particle of several functions by selection and combination of materials used to prepare [1] [2].

However, on a few practical application fields of these composite particles, it is strongly desired that the composite particles are prepared by using biodegradable materials [3]-[6]. For an example, it has been tried to prepare microcapsules or composite particles, which contain agricultural medicine or pheromone for noxious insects, by biodegradable materials based on natural elemental materials, because it may be expected that the biodegradable shell materials should vanish after complete release of core material and environmental pollution could be prevented [7]-[9].

Furthermore, the composite particles containing various drugs and physiological active materials dosed into the human body are inevitably required to be biodegradable [10]-[12]. For these demands, the various composite particles have been prepared by using edible and biodegradable materials. Similarly, it has been tried to develop the preparation method of toner used on the copying press with the green preparing process by using biodegradable materials [13]-[15].

In these works stated above, the most important purpose is to develop the simple preparing methods without much energy and noxious volatile solvents. However, it is well known that there are many important things required to be solved in these works. For examples, the noxious solvents have been used as the solvent for biodegradable polymers and the complicated preparation processes have been developed.

In this study, taking these into consideration, we have tried to develop the simple preparation method without any noxious solvents. For this purpose, we have adopted the phase separation method followed by the drying-in-liquid method to prepare the biodegradable composite particles, in which poly- ϵ -caprolactone was used as the biodegradable polymer, because poly- ϵ -caprolactone with lower melting point (ca. 60°C) is pliable and easily dissolved in acetone of an innocuous solvent.

The purposes of this study are to investigate whether the biodegradable composite particles could be prepared by the phase separation method [16]-[18] followed by the drying-in-liquid method [1] [19] or not, to establish the optimum operational conditions for preparing the biodegradable composite particles, to characterize the composite particles prepared and to get the fundamental information for application to toner particles.

2. Experiment

2.1. Materials

Two kinds of biodegradable poly- ϵ -caprolactone (PCL) (Tokyo Kasei Co., Ltd.) were used as matrix polymer of composite particles. One of them is p- ϵ -caprolactone (RPCL) with molecular weight of 10,000 and the other p- ϵ -caprolactone (HPCL) with molecular weight of $7 \times 10^4 - 10^5$. Acetone (Junsei Chemical Co., Ltd.) was used as the good solvent for poly- ϵ -caprolactone. As additive materials, quaternary ammonium (QA) as a charge controlling agent (Oki Data Co., Ltd.), wax with the melting point of $M_T = 69^\circ\text{C}$ and carbon black (CB) (Mitsubishi Chemical Co., Ltd.) were added. Polyoxyethylenesorbitanmonolaurate (Tween20), Polyoxyethylenesorbitantristearate (Tween65) and Polyoxyethylenesorbitanmonooleate (Tween80) (Tokyo Kasei Co., Ltd.) were used as water soluble surfactants.

2.2. Preparation of Composite Particles

Figure 1 shows the flow chart for preparing the composite particles made of biodegradable polymer and a few additives.

At first, PCL, Wax, QA and surfactant of a given amount were added into acetone and completely dissolved to form the uniform solution by stirring for 30 min with the six bladed disc type impeller. Next, the CB slurry with 5 wt% concentration was prepared by adding CB of a given weight into water.

After the CB slurry was poured into the acetone solution, the mixture was homogenized for 3 min with the ultrasonic homogenizer in order to untie bloc of CB and then, homogenized further for 3 min with the rotor stator homogenizer to completely disperse CB in the solution. Here, it was confirmed that PCL, QA and wax dissolved

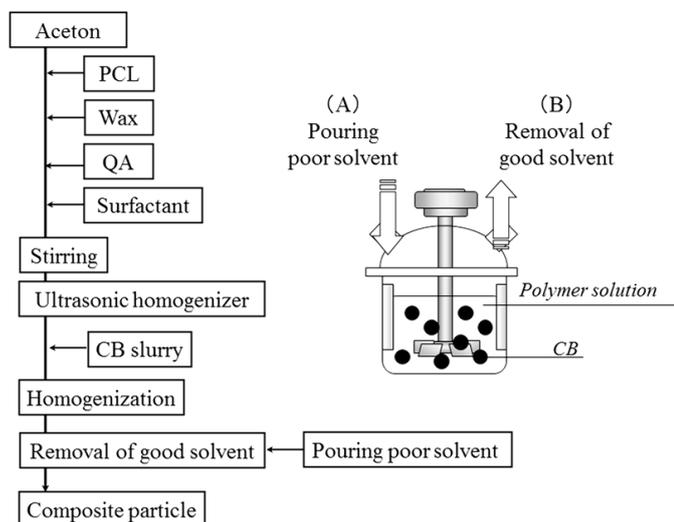


Figure 1. Flow chart for preparing composite particles.

in the acetone solution were not reduced by addition of the CB slurry because of small quantity of slurry water (3.5 cm^3).

Then, water as the poor solvent was added at the constant feeding velocity by the microfeeder. Then, acetone was removed under the conditions of $T = 30^\circ\text{C}$ and low vacuum due to aspirator (drying-in-liquid operation) on pouring water of the poor solvent for PCL. With elapsing time, PCL, wax and QA dissolved in the acetone solution were gradually separated to form coagulums in which CB was contained and to finally form the composite particles.

The drying-in-liquid operation was continued for 3 h to completely remove acetone. Accordingly, the diameters of composite particles were kept constant at the complete removal of acetone. The composite particles thus formed were separated with the filtration paper and dried under room temperature.

In this operation, the concentration of surfactant (C_E), the feeding velocity (V_p) of poor solvent (water) and the weight ratio ($R = W_H/W_L$) of HPCL to RPCL were mainly changed, where W_H and W_L were the weights of HPCL and RPCL, respectively. **Table 1** shows the experimental conditions adopted in this study.

2.3. Characterization

Thermal visco-elasticity

Thermal visco-elasticity of matrix polymer of composite particles is one of the important characteristics of the composite particles. Especially, when the composite particles are planned to apply to toner particles, it is necessary to obtain the fundamental informations about thermal visco-elasticity of matrix polymer. Thermal visco-elasticity of composite particles was measured by Thermal Visco-Elasticity Instrument (SII Nano Technology Co., Ltd., Japan). Namely, thermal visco-elasticity was measured by changing the weight ratio of HPCL to RPCL.

Observation

The composite particles formed were observed by optical microscope (OLYMPUS Co., Ltd., Japan) and scanning electron microscope (SEM: Nihon Densi Co., Ltd., Japan), respectively. The inner structure of a composite particle was observed by transmission electron microscope (TEM: Nihon Densi Co., Ltd, Japan). In this observation, the cross section was colored by Lutonium dye.

Diameter distribution and mean diameter

The diameter distributions and mean diameters of composite particles were measured by Particle Size Analyzer (ELSZ-2; OTSUKA ELECTRONICS Co., Ltd., Japan). Here, the mean diameters were the Sauter mean diameters.

Zeta potential

As zeta potential of each component in the solution is the important factor to determine whether the composite particles could be prepared or not, zeta potential was measured with Particle Size Analyzer (ELSZ-2: OTSUKA ELECTRONICS Co., Ltd., Japan).

Table 1. Experimental conditions.

Acetone (good solvent)	220 g
Water (poor solvent)	250 g
PCL	2 g
Pigment 5 wt% (CB slurry)	4 g (3.5 ml H ₂ O)
Quaternary ammonium (QA)	0.02 g
Wax	0.1 g
Surfactant (Tween20, 65, 80)	C _E = 2.5 - 5.5 wt%
Feeding velocity of water	V _P = 2 - 6.5 [ml/min]
Weight ratio of HPCL to RPCL	R(W _H /W _L) = 0% - 100%
Homogenization with ultrasonic	3 min
Homogenization with rotor stator	3 min, 10,000 rpm
Temperature of drying-in-liquid process	T = 30°C
Time of drying-in-liquid operation	3 h
Revolution velocity in drying-in-liquid	250 rpm

3. Results and Discussion

3.1. Effects of Surfactant Species and Concentration of Them

Figure 2 shows the SEM photographs of composite particles prepared with Tween20, Tween65, Tween80. The composite particles prepared with Tween20 and Tween65 coagulated each other to form the irregular particles. However, the composite particles prepared with Tween80 were the spherical sound particles.

As Tween20 (HLB 16.7) is more hydrophilic and Tween65 (HLB 10.5) is more hydrophobic, the stabilizing effect for the (O/W) emulsion may be lower due to insufficient adsorption amounts of them. Meanwhile, as Tween80 (HLB 15.0) has the optimum HLB, the stabilizing effect for the (O/W) emulsion may be stronger. However, it is necessary to investigate the stabilizing effect of surfactant species in detail. Taking the results obtained above into consideration, Tween80 was used to prepare the composite particles hereafter.

Figure 3 shows the effect of concentration of surfactant on the mean diameters of composite particles. From this figure, it was found that the mean diameters decreased with the concentration of surfactant and become almost constant ($D_p = 8.32 \mu\text{m}$) at $C_E = 3.7 \text{ wt}\%$. With increasing the concentration of surfactant, the stability of CB and composite particles may be increased to form the smaller sound composite particles.

The SEM photograph of composite particles prepared under the conditions of $C_E = 3.7 \text{ wt}\%$ and $V_P = 2.0 \text{ ml/min}$ is also shown in **Figure 3**. It was found that the composite particles with the mean diameter of about $8.32 \mu\text{m}$ and the dispersion degree (σ/D_p) of 0.38 could be prepared, where σ was the standard deviation of diameter distribution.

3.2. Effect of Feeding Velocity of Poor Solvent

Figure 4 shows the effect of feeding velocity of poor solvent on the mean diameter and the morphology of composite particles under the conditions of $C_E = 3.7 \text{ wt}\%$ and $R = 0$ (only with RPCL) together with the microscopic photographs. It was found that with increasing the feeding velocity, the mean diameter increases from $30 \mu\text{m}$ ($V_P = 2.0 \text{ ml/min}$) to $290 \mu\text{m}$ ($V_P = 6.5 \text{ ml/min}$) and larger coagulated particles come to be formed. Furthermore, CB was found to be coated well with PCL separated by pouring the poor solvent and to form the composite particles. However, wax is not observed well in these photographs. The microscopic photographs in **Figure 4** were taken in the slurry. Accordingly, PCL adsorbed on the surface of CB was swollen. For this reason, the diameters shown in **Figure 4** become larger than those in **Figure 3**.

From these results, it was found that the feeding velocity was an important factor to determine the diameter and structure of composite particles. Furthermore, the feeding velocity slower than 4.0 ml/min was found to be the optimum feeding velocity to prevent from coagulating and to prepare the composite particles with the desired structure.

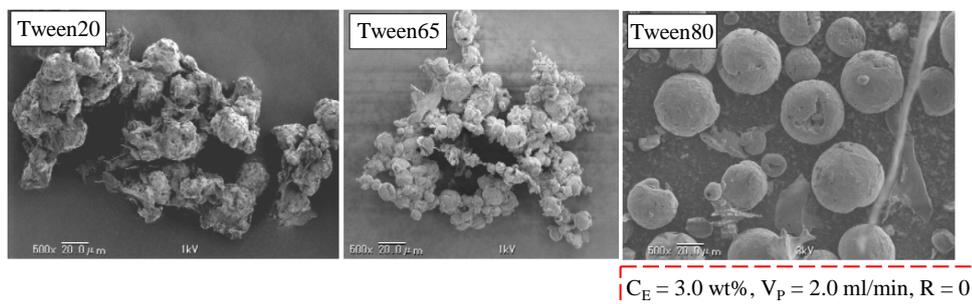


Figure 2. SEM photographs of composite particles (effect of surfactant species).

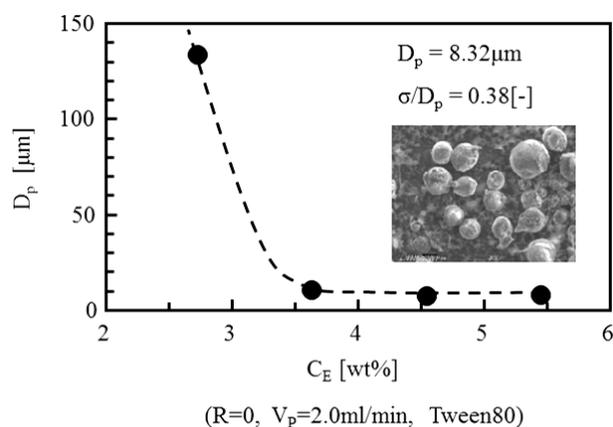


Figure 3. Effect of concentration of surfactant on diameter of composite particle.

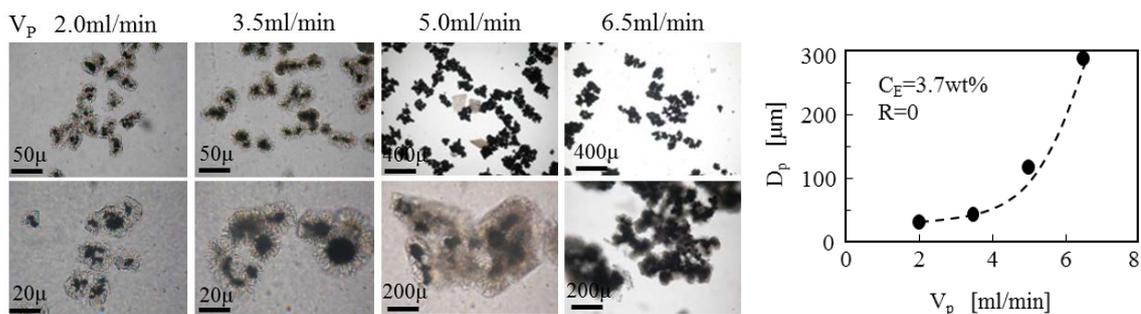


Figure 4. Effect of feeding velocity of poor solvent on formation of composite particles.

3.3. Effect of Weight Ratio of HPCL to RPCL

Figure 5 shows the dependence of the mean diameters of composite particles on the weight ratio (R) at each concentration of surfactant. In **Figure 5**, the mean diameters drastically decreased with the concentration of surfactant even at any ratio. The larger the ratio, the larger the mean diameter. When HPCL dissolved in the oil phase was reduced, the larger nuclei were formed and then, the larger particles were formed due to coagulation each other. However, in order to prepare the composite particles with the mean diameter of ca. 10 μm , it was found that there was the critical concentration of surfactant at each ratio.

For an example, the critical concentrations were 3.5 wt% ($D_p = 10.5 \mu\text{m}$) at $R = 0$ and $R = 10\%$, 7 wt% ($D_p = 10.3 \mu\text{m}$) at $R = 50\%$, 8.2 wt% ($D_p = 10.5 \mu\text{m}$) at $R = 100\%$, respectively.

Figure 6 shows the SEM photographs and diameter distributions of composite particles prepared under each experimental condition in which both the number distributions and the volume distributions of diameters are also shown. The composite particles are found to be spherical particles. Furthermore, the diameter distributions at $R = 10\%$ and 100% were more uniform compared with that at $R = 50\%$.

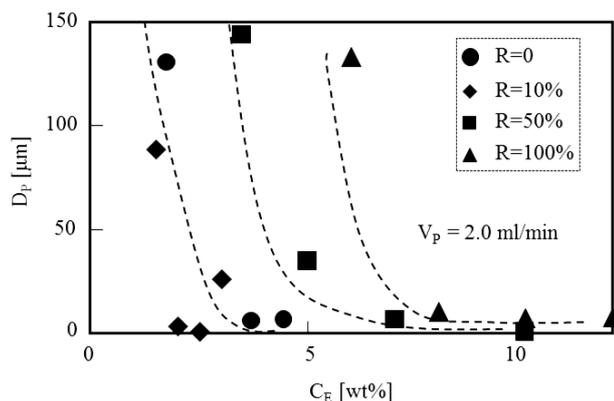


Figure 5. Dependence of mean diameter on concentration of surfactant and weight ratio.

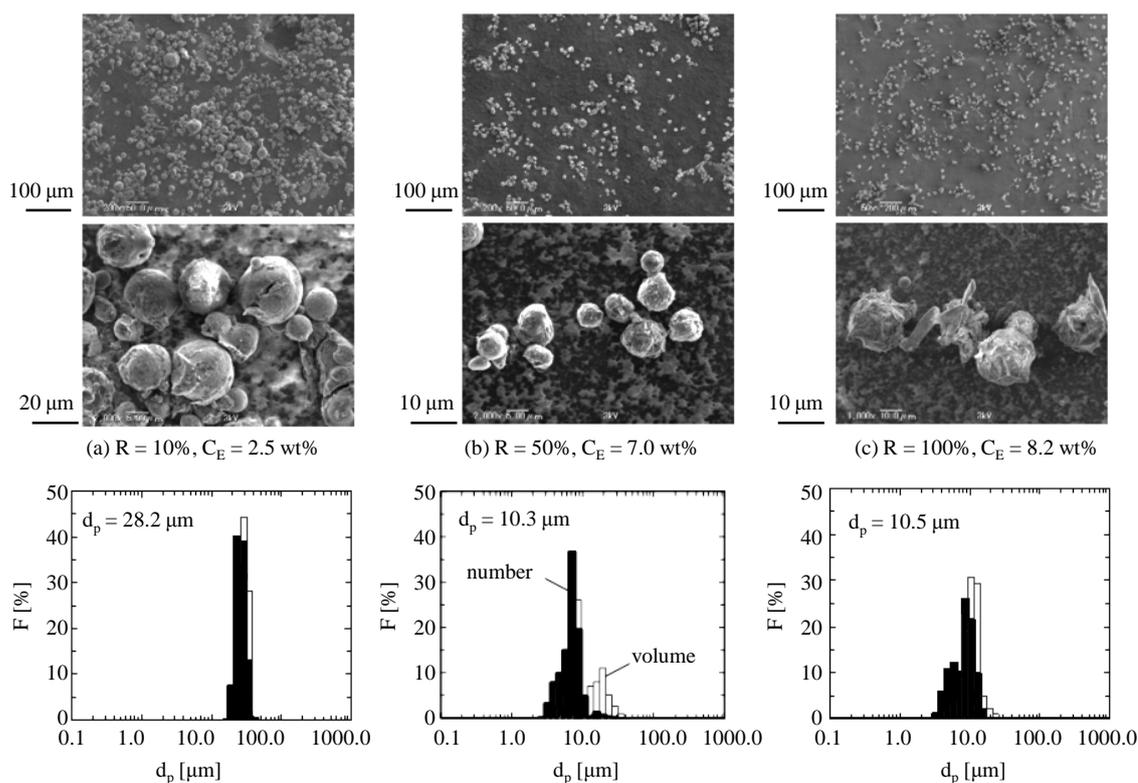


Figure 6. Effect of molecular weight of polymer ($V_p = 2.0$ ml/min).

3.4. Thermal Visco-Elasticity

Figure 7 shows the results of the thermal visco-elasticity of composite particles prepared with RPCL and HPCL together with that of toner particles used on the hard copy for reference. In **Figure 7**, the curve 1, the curve 2 and the curve 3 are the results for RPCL, HPCL and toner particles, respectively.

If we are going to apply the composite particles made of only RPCL or only HPCL to the toner particles, it may be necessary to modify the thermal visco-elasticity of the composite particles.

Figure 8 shows the results of the thermal visco-elasticity measured by changing the weight ratio of HPCL to RPCL and adding wax. From these results, it was found that the thermal visco-elasticity of composite particles was not affected by the weight ratio of HPCL to RPCL (as shown in **Figure 8(a)**) and become almost equal to the desired result when the composite particles were prepared with HPCL and wax of 5 wt% (as shown in **Figure 8(b)**). Here, L in **Figure 7** and **Figure 8** is the moving distance of sensor contacting to the sample.

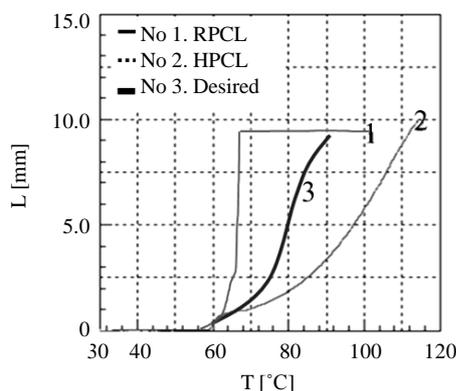


Figure 7. Measured thermal visco-elasticity of PCL.

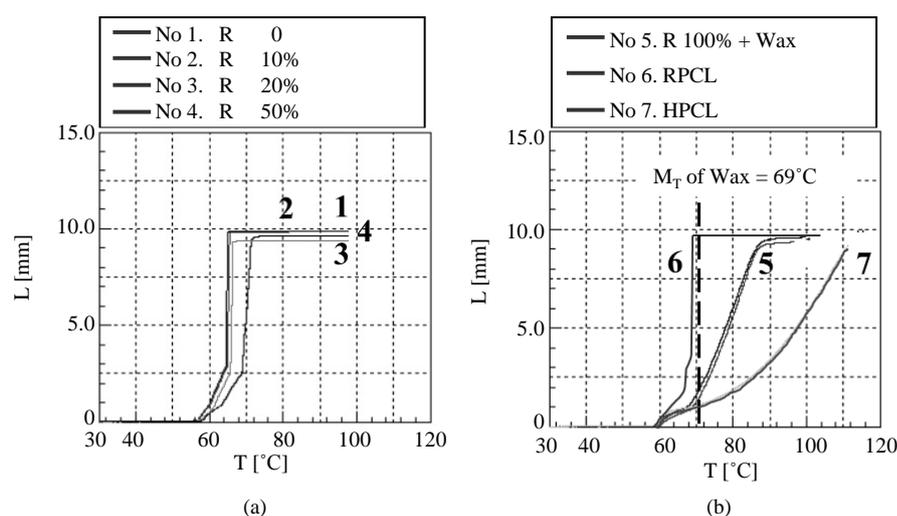


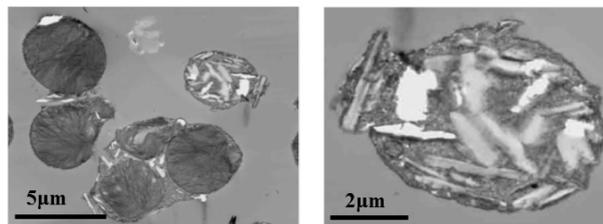
Figure 8. Effect of weight ratio on thermal visco-elasticity of matrix polymer.

3.5. Formation Mechanism of Composite Particles

Figure 9 shows the TEM photographs of the inner structure of composite particles prepared under the conditions as shown in figure, where PCL was colored by lutetium dye. It was found that wax (white color) and CB (black color) were contained well in the matrix polymer. From the results obtained above, the formation mechanism of composite particles may be presented as shown in **Figure 10(a)**. At first, more hydrophobic wax is rapidly separated out and adheres on the hydrophobic surface of CB due to the hydrophilic-hydrophobic interaction and due to attractive force on the basis of zeta potential. The zeta potential of each material measured in the acetone aqueous solution is shown in **Figure 11**. Next, PCL and QA may adhere on the surface of coagulated particles made of wax and CB due to hetero coagulation, because PCL and QA charge positively and wax charges negatively as shown in **Figure 11**. Also, the effect of feeding velocity of poor solvent on the diameter and structure may be explained as follows (in **Figure 10(b)**).

Namely, although CB is contained well into the composite particles at the slower feeding velocity of poor solvent, however, CB comes to coagulate each other by the binder action of PCL rapidly separated at the faster feeding velocity of poor solvent. Finally, the composite particles must be prepared by complete removal of good solvent. As a result, the faster the feeding velocity, the larger the diameters of composite particles.

Here, the selection of acetone of the good solvent and water of the poor solvent for PCL must be the optimum combination, because both solvents are innocuous and generate zeta potential in the dispersion. Also, the revolution velocity of impeller in the drying-in-liquid operation must necessarily affect the composite particle diameter, because coalescence and break-up of droplets are affected by the revolution velocity. Accordingly, if the other solvent species and revolution velocity should be used, the different results should be obtained.



($R=100\%$, $C_E=8.2\text{wt}\%$, $V_p=2\text{ml/min}$, wax 5wt%)

Figure 9. TEM photographs of composite particles (colored by lutetium).

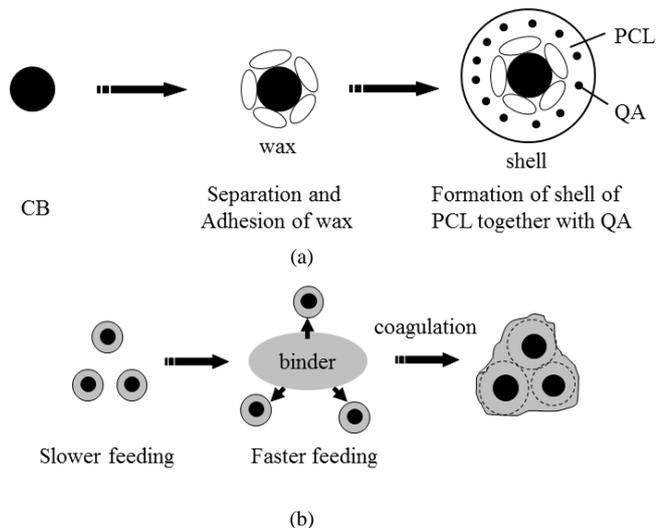


Figure 10. Formation mechanism of composite particles. (a) Formation of composite particles; (b) Effect of feeding velocity.

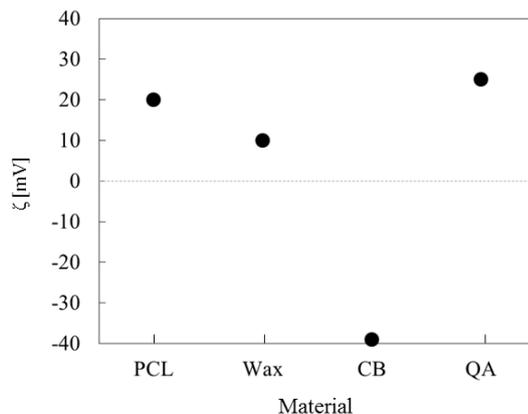


Figure 11. Zeta potential of each material.

4. Conclusions

We have tried to prepare the composite particles made of biodegradable polymer, carbon black, quaternary ammonium and wax by the phase separation method followed by the drying-in-liquid operation. The following fundamental results could be obtained.

- 1) The composite particles could be prepared by the preparation method presented in this study.
- 2) The structure and the mean diameter of composite particles were strongly affected by the feeding velocity of poor solvent for PCL. The larger the feeding velocity of poor solvent, the larger the mean diameter of compo-

site particles.

3) The spherical sound composite particles could be prepared with Tween80.

4) The diameters of composite particles drastically were decreased with the concentration of surfactant and increased with the weight ratio of PCL with larger molecular weight to PCL with smaller molecular weight.

5) Thermal visco-elasticity of composite particles became equal to that of toner particles by adding wax of 5 wt% into PCL with larger molecular weight.

6) Some fundamental information of composite particles required to apply to the toner particles could be obtained. However, it is necessary to investigate how the preparation conditions affect the characteristics of composite particles such as the electric charge density on the surface of composite particles, the printing process and the biodegradability of composite particles.

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