

Modeling and Experiments of the Gain and Noise Figure for an Irradiated Erbium-Ytterbium Co-Doped Fiber Amplifier

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Abstract

It is crucial to study the effect of radiation on the fiber amplifier devices. In the present paper, the Erbium-ytterbium co-doped fiber amplifier (EYDFA) has been irradiated by a neutron beam of different doses for various exposure times from an Am-241/Be-9 neutron source. The gain and noise figure of the EYDFA have been calculated theoretically and recorded after and before the irradiation to test its performance under the effect of irradiation. In order to show the enhancement in the gain of the fiber amplifier devices, a comparison between the gain of the irradiated EYDFA and Erbium doped Fiber amplifier (EDFA) has been carried out. The calculated results by the proposed model are in good agreement with the experimental ones. It indicates that the gain of EYDFA deteriorates after being irradiated by a neutron dose. Moreover, the gain of irradiated EYDFA has been reduced to 13.8 dB at a dose of 720 Gy.

Keywords

Erbium-Ytterbium Co-Doped Fiber Amplifier, Americium/Beryllium-Neutron Source, Gain Deterioration

1. Introduction

Erbium doped fiber amplifiers (EDFAs) are well suited for long haul systems, however they are still too bulky

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and costly to be used in local areas [1]. In these amplifiers, a concentration of Erbium (Er) exceeding 10^{26} ion/m³ is needed. Unfortunately, such high concentration may cause concentration quenching resulting from ion-ion interactions by cooperative up conversion and cross relation, which may reduce the pump efficiency [2].

On other hand the ion-ion interactions which causes pair-induced up-conversion depletes the erbium meta stable level. It lowers the pump efficiency for concentration above few hundred parts per million of Er [3]. This issue has been addressed by co-doping the Er fiber by ytterbium (Yb). The presence of Yb reduces the formation of Er clusters and reduces the up-conversion rate from the upper level of Er (${}^{4}I_{13/2}$ level) significantly. This allows high erbium doping level needed for high gain amplifier. Moreover, an efficient indirect pumping mechanism of Er ions is provided by an energy transfer from Yb to Er [4].

In the EYDF system, the ytterbium ions are first pumped at the absorption wavelength of 800 - 1100 nm to the ${}^{2}F_{5/2}$ state. The energy of the Yb ions is then transferred to the erbium ions, which are excited to the ${}^{4}I_{11/2}$ state. These excited Er ions undergo a nonradioactive transition to the ${}^{4}I_{13/2}$ meta stable state and form a population inversion with the ${}^{4}I_{15/2}$. An incident optical signal travelling through the fiber is amplified via stimulated emission between these two states [5].

Many researchers addressed the deterioration of the gain of the optical amplifiers that carried out by natural radiation [6] [7]. Nuclear radiations may produce similar defects in the optical fiber as well as the optical amplifier [8]-[12]. Therefore, the exposure of the optical amplifier to the ionizing radiation may result in a change of the refractive index along the whole fiber [13] [14].

In the present paper, we will study the effect of irradiating the EYDFA to a neutron beam of 4.5 MeV mean energy on its refractive index. A theoretical modeling for the gain and the noise figure will be reported here. The calculated gain of the EYDFA will be compared to the measured one. Moreover, it will be compared to the reported one for a single doped fiber amplifier EDFA for low neutron dose irradiation in [5].

2. Experimental Setup

The EYDFA is pumped by a pump laser diode (wavelength 980 nm). The input power is varied from -40 dB to 5 dB. The pump light and signal light are launched into the inputs of a wavelength division multiplexing (WDM) coupler as shown in **Figure 1**. The EYDFA is exposed to a neutron beam emitted from a 5 Ci Americium/ Beryllium (Am-241/Be-9) neutron source for different exposure times 1, 10, 20, and 30 days. The neutron source was calibrated by Amersham Ind., UK on 1987. The neutron spectrum in **Figure 2** indicates that Am-241/Be-9 neutron energies range from about 2 MeV to 10 MeV and that approximately 23% of neutrons are of energies below 1 MeV [6]. The average neutron energy was taken to be 4.5 MeV from the spectrum in **Figure 2** as in [7]. The characteristics and the composition of the Am-241/Be-9 neutron source are listed in **Table 1**.

Fine powder of AmO₂ is mechanically mixed with powdered Be (initial cluster size of 50 pmm) and compressed into cylindrical pellet (density 1.3 g/cm³). The source is embedded in a Plexiglas and Lucite: $C_5H_8O_2$; density = 1.18 g/cm³; A = 100.117 [10].

The measurements were carried out at the nuclear radiation laboratory at the physics department, King Abdulaziz University, Jeddah, Saudi Arabia. The EYDFA was positioned at 5 cm from the center of the neutron source. The emitted gamma rays from the neutron source has been shielded by 10 cm thickness lead bricks surrounded the source from all sides [10]. The container, the shielded well inside which the Am-Be neutron source is placed and are shown in **Figure 3**.

The neutron doses from the source were measured by a neutron monitor (Nuclear Enterprise, UK NM2) to be 24, 240, 480 and 720 Gy, respectively. This monitor was provided by the Radiation Safety Committee in King Abdulaziz University.

3. Mathematical Modeling

Er and Yb co-doped fibers acts as a four level laser system. The energy level schemes for these two ions along with the possible transitions are shown in **Figure 4**. The transitions involve both radiative and non-radiative energy transfer processes [3]. The rate equations for Er and Yb population densities can be written as [8] [9]:

$$\frac{\mathrm{d}N_2}{\mathrm{d}t} = -A_{21}N_2 - 2C_{up}N_2^2 + N_1\sigma_{sa}\phi_s - N_2\sigma_{se}\phi_s + \gamma_{32}N_3 \tag{1}$$



Figure 1. A schematic diagram for EYDFA irradiation experimental setup.



Figure 2. The neutron spectrum Am-241/Be-9 [5].

Table	1.	Characteristics and	l composition of	f the A	Am-241/I	Be-9	neutron source.
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Parameter	Definition		
Neutron emission rate	$2.2 \times 10^6 \text{ n s}^{-1} \cdot \text{Ci}^{-1}$		
Neutron emission tolerance	10 %		
Source strength	$1.1 imes 10^7 \mathrm{n} \cdot \mathrm{s}^{-1}$		
Source half life	433 Yr		
Peak thermal neutron flux	10 ⁶ neutrons/sec		
Capsule type	X.14 with 6 M threads		
Source composition	Mixture of Americium oxide with Beryllium metal powder		
Source typical Composition	C (0.004%); Mn (1.59%); P (0.011%); S (0.008%); Si (0.37%); Cr (16.96%); Ni (3.61%); Mo (2.29%); and Fe (65.16)		
Capsule grade	grade AIS1.316		
Moderator type	H_2O		
Source overall diameter	30 mm		
Source overall height	60 mm		
Source wall thickness	1.2 mm		



Figure 3. Am/Be neutron source. (a) The transport container, (b) The shielded well inside which the Am-Be neutron source is placed, and (c) close picture for the circular face of the Am/Be neutron source.



Figure 4. Energy level diagram of Er and Yb system. The dashed lines represent the non-radiative transition, whereas, the solid lines are for the radiative transitions.

$$\frac{\mathrm{d}N_3}{\mathrm{d}t} = -N_3\sigma_{pe}\phi_p + N_1\sigma_{pa}\phi_p + KN_6N_1 - K'N_3N_5 - \gamma_{32}N_3 + \gamma_{43}N_4 \tag{2}$$

$$\frac{\mathrm{d}N_4}{\mathrm{d}t} = C_{up}N_2^2 - \gamma_{43}N_4 \tag{3}$$

$$\sum_{i}^{4} N = N_{Er} \tag{4}$$

$$\frac{\mathrm{d}N_5}{\mathrm{d}t} = KN_6N_1 - K'N_3N_5 - N_5\sigma'_{pa}\phi_p + N_6\sigma'_{pa}\phi_p + N_6\sigma'_{pe}\phi_p + A_{65}N_6$$
(5)

$$N_5 + N_6 = N_{Yb} \tag{6}$$

where, N_1 , N_2 , N_3 and N_4 are the Er³ population densities (m⁻³) of ${}^4I_{15/2}$, ${}^4I_{13/2}$, ${}^4I_{9/2}$ levels, respectively. The quantities N_5 , N_6 are the Yb³ population densities (m⁻³) of the ${}^2F_{7/2}$ and ${}^2F_{5/2}$ levels respectively. Whereas, φ_P , φ_s , σ_{pe} , σ_{pe} , σ'_{pe} , σ'_{pe} , A_{21} , A_{65} , K, K', C_{up} are defined in **Table 2**. The spontaneous emission rates of Er⁺³ and Yb⁺³ can be calculated by:

$$\sigma_a = \frac{h\gamma n}{C} B_{12} g_{12}(\gamma); \sigma_e = \frac{h\gamma n}{C} B_{21} g_{21}(\gamma)$$
(7)

where, $g_{12}(\gamma)$ and $g_{21}(\gamma)$ are the normalized emission and absorption line shape respectively, n is the refractive index of the medium and B_{12} and B_{21} are the coefficients of transition strength from Level 1 to Level 2 and from Level 2 to Level 1, respectively. Then the signal gain G is given by

$$G = \exp\left(\int_{0}^{L} g(z) dz\right),$$
(8)

where g(z) is the gain for Er^{+3} transition per unit length.

$$g(z) = \Gamma_{\rm s} \left[N_2 \sigma_{\rm se} - \sigma_{\rm sa} \left(N_{\rm Er} - N_2 \right) \right]$$
(9)

The total noise figure NF is

$$NF = 10\log_{10}\left[\frac{1}{G} + \frac{P_{ASE}}{Gh\gamma B_o} - \frac{P_{SSE}}{h\gamma B_o}\right]$$
(10)

where, γ is the signal frequency, B_0 is the noise bandwidth, P_{ASE} and P_{SSE} are the power of amplified spontaneous emission, and the power of source spontaneous emission, respectively. Table 3 lists the values for the ion concentrations and absorption cross sections for Er⁺³ and Yb⁺³ that have been used in the present model.

Parameter	Definition
φ _P	The pump photon flux
$arphi_{ m s}$	The signal photon flux
$\sigma_{_{ m pe}}$	The stimulated emission cross section for Er ⁺³
$\sigma_{_{\mathrm{Pa}}}$	The absorption cross section for Er^{+3}
$\sigma'_{ m pe}$	The stimulated emission cross section for Yb ⁺³
$\sigma'_{\scriptscriptstyle{ extsf{Pa}}}$	The absorption cross section for Yb ⁺³
A ₂₁	The spontaneous emission rate of Er ⁺³
A ₆₅	The spontaneous emission rate Yb ⁺³
K and K	The coefficient of energy transfer $(m^3 \cdot s^{-1})$ for the concentrations of Er^{+3} and Yb^{+3}
$C_{ m up}$	The up conversion coefficient

Table 3. Parameters used in the present	mathematical model	[7]	
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Parameter	Reference value
Er ³ ion concentration N _{ER}	$5.14 \times 10^{25} \mathrm{m}^{-3}$
Yb^3 ion concentration N_{Yb}	$6.20 \times 10^{26} \mathrm{m}^{-3}$
Yb ³ absorption cross section σ_{56}	$0.14 \times 10^{-25} \mathrm{m}^2$
Yb ³ absorption cross section σ_{65}	$2.82 \times 10^{-25} \mathrm{m}^2$
Er^3 ion concentration σ_{12}	$4.82 \times 10^{-25} \mathrm{m}^2$

4. Results and Discussion

Figure 5 shows the variation of the neutron doses (Gy) as a function of the exposure time (days) from an Am-241/Be-9 neutron source at a distance 5 cm from the center of the source. The performance of the EYDFA has been tested before exposure to the neutron irradiation. **Figure 6** shows a comparison between the gain of the suggested co-doped fiber amplifier EYDFA as a function of the input power (mW) with that of the regular fiber amplifier EDFA which has been reported in [5]. The solid line represents the experimental data, whereas, the symbols are for the present calculations for the wavelength in nm. **Figure 6** shows also the variation of the Noise Figure (NF) for all the wavelengths before the irradiation using equation (10). At wavelength 1530, the gain of the EYDFA is maximum at 17 dB and NF is 4 dB for an input power of the 130 mW. These satisfy the tested results of the product before it is used commercially. It is clear that the gain of the EYDFA higher than that of the EDFA by a value of 1.4 dB.

To compare the performance of the reported fiber amplifier EDFA with that of the suggested co-doped fiber amplifier EYDFA under the effect of neutron irradiation, **Figure 7** shows the variation of the signal gain G with the pump power (mW) for the EDFA and EYDFA after exposure to different doses 24, 240, 480 and 720 GY.

The Results in **Figure 7** show that the EYDFA has a higher signal gain than that of the EDFA. Meanwhile, the irradiation with neutron doses deteriorates the gain of the amplifiers. **Figure 8** shows the deterioration percentage in the signal gain for the EDFA and EYDFA fiber amplifiers as a function of the neutron irradiation doses at a pump power 120 mW. Results show that the deterioration percentage in the gain of the EDFA amplifier. It shows also, that the higher the irradiation doses, the higher the deterioration percentages. As a results of the gain drop, the NF increases significantly by values of 21.9 dB for EYDFA at 720 Gy.

5. Conclusion

The performance of the Erbium-ytterbium co-doped fiber amplifier (EYDFA) has been tested against the Erbium doped fiber amplifier (EDFA) under the effect of neutron irradiation. The signal gain of the EYDFA has been measured and calculated theoretically as presented in this work. Results of the performance testing show that the signal gain for the EYDFA is higher than that of the EDFA. In addition, it show that the higher the irradiation doses, the higher the deterioration in the signal gain. Moreover, we can say that the co-doping technique allows the fiber amplifier to be a radiation resistor. As the deterioration percentage for EYDFA is less than that of the EDFA. In other words, the performance of irradiated EYDFA is better than that of the irradiated EDFA by a value of 1.6 dB.



Figure 5. The variation of the neutron doses (GY) of the neutron source with the exposure time (days) at distance 5 cm from the center of the source.



Figure 6. The variation of the signal gain with the input pump power for two amplifiers, EDFA [5] and EYDFA at zero dose, symbols are for the theoretical results whereas, solid lines are experimental data.



Figure 7. The variation of the signal gain and noise figure with the pump power for EDFA and EYDFA irradiated with doses (a) 24 Gy, (b) 240 Gy, (c) 480 Gy and (d) 720 Gy, respectively. Circles are for EYDFA and squares are for EDFA.



Figure 8. The Gain deterioration percentage as a function of the dose (Gy) for EYDFA and EDFA amplifiers.

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