

# Development of Deep-Sea Resonant Sandwich Linear Ultrasonic Motor

Shaopeng He, Shengjun Shi, Weishan Chen

State Key Laboratory of Robotics and System, Harbin Institute of Technology, Harbin, China

Email: hsp@stu.hit.edu.cn

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## Abstract

A deep-sea resonant sandwich linear ultrasonic motor is proposed and designed. We determine the parameter of its structure by finite-element analysis. The piezoelectric actuator adopts compound vibration mode of fifth order bending vibration and second order longitudinal. The mode degeneracy of that is completed. We manufacture the prototype to measure the performance of it. We measure its vibration mode and resonant frequency. The velocity of prototype can reach 264.5 mm/s while the water pressure is 8 MPa and the voltage signal with frequency of 30.30 kHz and voltage amplitude of 150 V.

## Keywords

Piezoelectric Actuator, Finite-Element Analysis, Hybrid Mode, Fluid-Solid Coupling

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## 1. Introduction

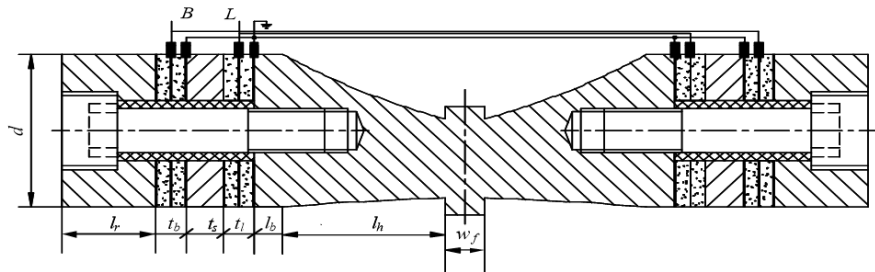
Piezoelectric actuator is a kind of new motor which using inverse piezoelectric effect of piezoelectric ceramics [1] [2] [3]. Piezoelectric actuators have advantages of compact structure, high power with small weight, without electromagnetic interference and self-locking by frictional. Piezoelectric actuators are classified into two types: single vibration mode and compound vibration mode [3] [4] [5]. Piezoelectric actuators of compound vibration mode have higher performance than single vibration mode. At present, piezoelectric actuators have been studied by researchers, and they have been applied into many fields of spaceflight, automation and so on [6] [7] [8] [9]. We study the compound vibration mode piezoelectric motor working in deep-sea environment.

In this study, we design a deep-sea resonant sandwich linear ultrasonic motor and manufacture the prototype to measure its performance. The piezoelectric actuator adopts compound vibration mode of fifth order bending vibration and

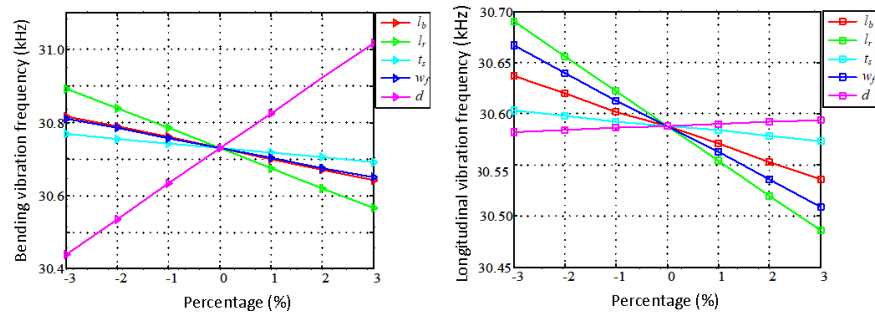
second order longitudinal. We complete the mode degeneracy by finite element analysis. We design and set up the experimental platform to measure the performance of prototype. The velocity of prototype can reach 264.5 mm/s while the water pressure is 8 MPa and the voltage signal with frequency of 30.30 kHz and voltage amplitude of 150 V. It verifies the simulation result and reaches the experiment objective.

## 2. Finite Element Analysis

We select a configuration to build finite element model as show in **Figure 1**. This configuration adopts compound vibration mode of five order bending vibration and second order longitudinal vibration. High order bending vibrations and longitudinal vibrations are small affected by deep-sea environment. We complete the mode degeneracy by adjust the parameter of piezoelectric actuator. We obtain the sensitivity of main parameters about resonant frequency as shown in **Figure 2**. We determine the final parameters of structure as show in **Table 1**.



**Figure 1.** Structure of piezoelectric actuator.



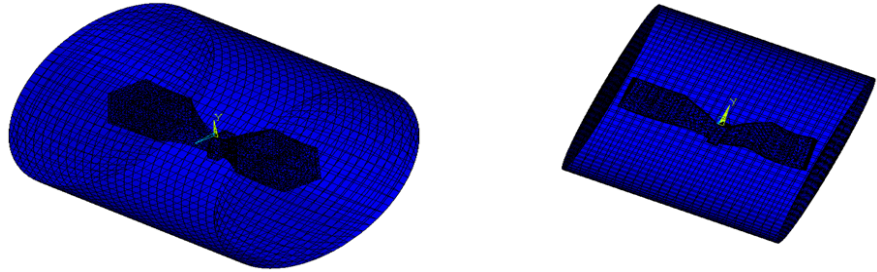
**Figure 2.** Sensitivity of main parameters.

**Table 1.** Parameter of structure.

$d$	$l_r$	$t_b$	$t_l$	$t_s$	$w_f$	$l_h$	$l_b$
35	20	6	6	8	8.5	37.5	6

After it, the finite element model under water is built to obtain the resonant frequency as shown in **Figure 3**. We compare the resonant frequency under water with normal resonant frequency, as shown in **Table 2**. It shows water have stronger effect on five order bending vibration than second order longitudinal

vibration. We also get many resonant frequencies with different pressure of water as shown in **Table 3**. It shows the pressure almost has no effect on resonant frequency. Finally, we conduct transient analysis to verify feasibility of this piezoelectric actuator.



**Figure 3.** Finite element model.

**Table 2.** Resonant frequency with different environment.

	Resonant frequency in air	Resonant frequency in water	Differentials
bending vibration (kHz)	30.730	30.214	0.516
longitudinal vibration (kHz)	30.588	30.478	0.110

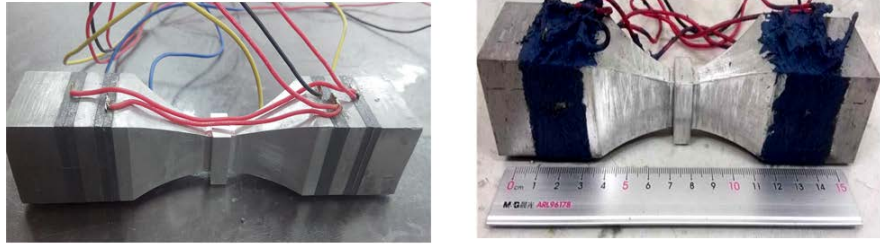
**Table 3.** Resonant frequency with different pressure.

pressure (Mpa)	2	4	8	12	16	20
bending vibration (kHz)	30.201	30.178	30.156	30.132	30.109	30.088
longitudinal vibration (kHz)	30.474	30.470	30.464	30.456	30.450	30.445

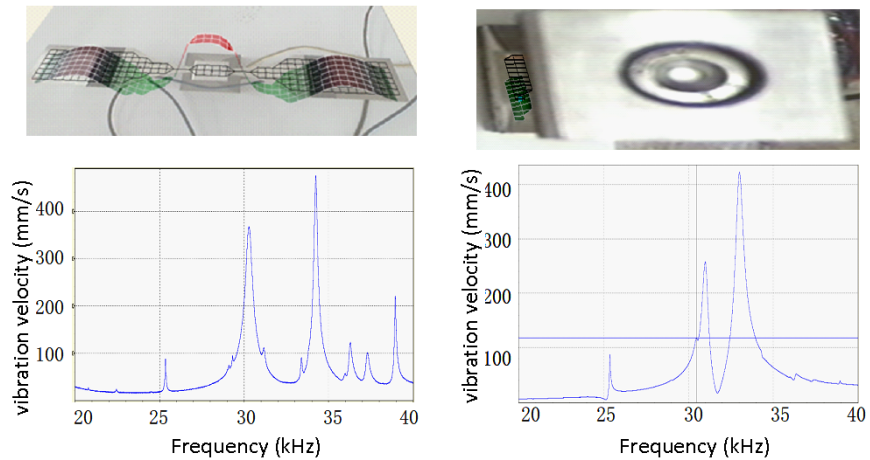
### 3. Experimental Study

We manufacture the prototype to measure the performance of this piezoelectric actuator, as shown in **Figure 4**. After it, we used the scanning laser Doppler vibrometer (PSV-400-M2, Polytec, Germany) to measure its vibration mode and the resonant frequency, as shown in the **Figure 5** and **Figure 6**. We can know the vibration mode and the resonant frequency is almost coincident with the simulation. We think the fabrication error contribute on the little different.

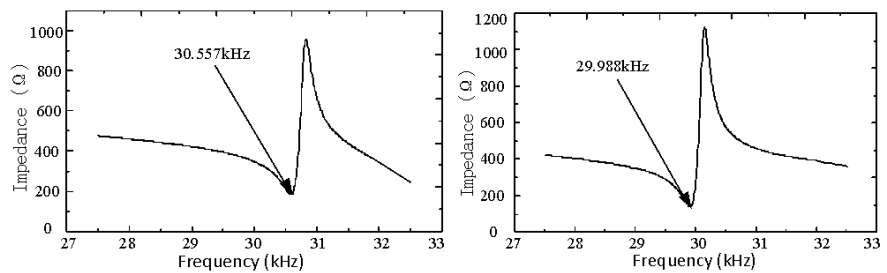
When the prototype is placed in the deep sea high pressure simulation system, we use precision impedance analyzer to measure impedance characteristic of prototype and obtain the resonant frequency, as shown in **Figure 6**. It has a little reducing compare with the normal environment, which shows correspondence with simulation result. Finally, the velocity of prototype reaches 264.5 mm/s while the water pressure is 8 MPa and the voltage signal with frequency of 30.30 kHz and voltage amplitude of 150 V.



**Figure 4.** Prototype and sealed prototype.



**Figure 5.** Vibration mode and vibration velocity of prototype.



**Figure 6.** Impedance analysis result.

## 4. Conclusion

In this study, we design and study a deep-sea resonant sandwich linear piezoelectric actuator. We complete the mode degeneracy of fifth order bending vibration and second order longitudinal vibration. We manufacture the prototype and measure its performance. The measuring result verifies the simulation result. Finally, prototype's velocity reaches 264.5 mm/s while the water pressure is 8 MPa and the voltage signal with frequency of 30.30 kHz and voltage amplitude of 150 V.

## Acknowledgements

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