

A Full Dynamic Voltage Stability Research Based on Time-domain Simulation^{*}

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ABSTRACT

The voltage stability is substantially a dynamic stability, but the primary method which is more mature and engineering practical to analyze the stability of voltage is still static analysis. The time-domain simulation is an important measure in research of complex power grid. With the development of full dynamic simulation technology, the research of dynamic voltage stability by using full dynamic simulation program which is based on time-domain simulation can be carried out. This paper uses full dynamic simulation program in dynamic voltage stability research, lays special stress on research in how generator over-excitation limiter functioned and influence in dynamic voltage stability research, and raise 2 methods and steps to figure out dynamic stable voltage in both over-excitation counted and not counted. The simulation results of examples indicate the correctness and effectiveness of these methods, and also fully verify the function and influence of generator over-excitation limiter in full dynamic voltage stability research.

Keywords: Dynamic Voltage Stability; Generator Over-excitation Limiter; Time-domain Simulation

1. Introduction

The voltage stability refers to the ability that all the buses' voltage was sustained in an acceptable range by power system when it runs in normal or disturbance circumstances. Voltage instability stems from the unbalance between power requirements of load and supply of the system[1,2]. The voltage stability analysis falls into two major categories: static and dynamic voltage stability analysis. Static voltage stability analysis is more mature than dynamic one. But with deeper research in voltage instability, it's gradually becomes more recognized that the voltage stability is substantially a dynamic stability and, the results of static analysis need to be verified by dynamic methods. The main dynamic voltage stability analysis methods are: small signal stability analysis, dynamic power flow analysis, time-domain simulation, direct method analysis and bifurcation theory analysis[3-8]. The time-domain simulation is one of the best tools in system planning, management, running and research of electric power system, also in dynamic voltage stability study. Full dynamic simulation of the power system that based on time-domain simulation is such a method in which the electro-mechanical transient, mid-term and long-term dynamic phenomena are unified[9-11].

But voltage instability is a slow process, which means the simulation would frequently last a few minutes, sometimes even tens of minutes. It is a typical rigid nonlinear system that the time constant in simulation model vary a lot and also combine with fast and slow dynamic process. And considering of stability of integration by parts and convergence of iteration, a long time step should not be used. Hence, a large amount of calculation is needed in time-domain simulation. Furthermore, the simulation may result unreliable because of the cumulative error of integration by parts with an improper time step length.

By analyzing the features of solving rigid nonlinear system and the key problem in existing numerical integration algorithm of power system dynamic simulation, Literature [12] raise a new composite numerical integration algorithm applying to full dynamic simulation which can overcome the shortages of existing algorithm that inefficient calculation and complicated intermittent processing in electro-mechanical transient process.

By using full dynamic simulation program with the new algorithm in dynamic voltage stability research, this paper lays special stress on how generator over-excitation limiter functioned and influence in dynamic voltage stability research, and raise methods and steps to figure out dynamic stable voltage in both over-excitation

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counted and not counted.

2. Dynamic Voltage Stability and Its Influencing Factors

Dynamic voltage stability research refers to the distance between current operating point and voltage collapse point when the load of power system rises gradually by certain rate. Influences of those dynamic components such as dynamic load model, ULTC, generator over-excitation limiter and others have been considered, which means the distance can be reported more precisely even in complicated system. Therefore, the margin information can be more valuable to operating crew.

Take many factors in consideration, load characteristic is the most critical and direct factor in voltage stability. It determines, to a large extent, the process of voltage instability and collapse. Hence, load modeling occupies a vital important place in voltage stability research. Load model is the key factor to the veracity and reliability of research results of voltage stability[13,14].

Generator excitation system's condition and its limiter are important factors that influence system voltage stability. Excitation regulator is the main method of voltage control in power system, but its regulating range is restricted by excitation winding thermal capacity. When excitation capacity of the engine set reaches its maximum limit, the over-excitation limiter will restrict the exciting current to rated value. This process may cause active power drop suddenly and then the system voltage drop correspondingly. Additionally, when the system get close to its limit state, a sudden excitation reduction of a single generator may results in chain reaction among other generators. This situation would leads to system voltage instability or accelerates the instability. In 2 blackouts in USA in 1996 and 2003, excitation protection functioned in the last moment when the grid black-out. Therefore, the influence of generator over-exciting limiter should be fully considered when trying to figure out the extreme value of system voltage stability [2,15,16].

3. Full Dynamic Simulation

3.1. Load Model

This paper takes fully advantages of time-domain simulation, and uses "static load model + introduction motor model" which is frequently used by engineering in full dynamic simulation.

Static load modeling:

$$\begin{cases} P = P_0 \left[P_1 \left(\frac{V}{V_0} \right)^2 + P_2 \left(\frac{V}{V_0} \right) + P_3 \right] (1 + \Delta f \cdot L_{DP}) \\ Q = Q_0 \left[Q_1 \left(\frac{V}{V_0} \right)^2 + Q_2 \left(\frac{V}{V_0} \right) + Q_3 \right] (1 + \Delta f \cdot L_{DP}) \end{cases}$$

In this model, P_0 is Active Load, P_1, P_2, P_3 are Constant Impedance Active Load Ratio, Constant Current Active Load Ratio and Constant Power Active Load Ratio respectively, V is System Actual Voltage, V_0 is System Reference Voltage, Δf is Frequency Variation, L_{DP} is percentage change of active power with every 1% of frequency change, and reactive power load model follow the same naming rule. In the upper formula, $P_1 + P_2 + P_3 = 1, Q_1 + Q_2 + Q_3 = 1$.

Introduction motor load modeling:

Based on known motor stator resistance R_S , motor stator reactance X_S , initiation reactance X_M , rotor resistance R_R , rotor reactance X_R and motor slip frequency S , the mechanical torque ratio A, B and C can be figured out.

3.2. Generator Over-exciting Limitation

The limitation of excitation system including two functions: transient limitation of ceiling current and limitation of inverse time over-excitation[17]. The primary courses of over-excitation are including long-term low system voltage, AVR acting on excitation, or AVR malfunctioning. The system dynamic voltage stability research is focus on the over-excitation limit action during system voltage instability process. In other words, it's a restriction function of inverse time over-excitation in excitation system.

Over-excitation process could be nearly constant, or could be a slow process that takes place and increases over-excitation value gradually. Hence, it's not in general to use over-excitation duration to define whether over-excitation limiter activate or not, but to limit the regulator output by calculate the heating value which generated by excitation set when excitation current exceed long-term operating permissible value. And the generator rotor can be protected by restrict the value of generator rotor current consequently.

Generator over-excitation limitation model, which aims to avoid generator overheated by excitation over current, is determined by its own overheat load capacity. And rotor over current time is connected with excitation current peak value. See **Figure 1** as below.

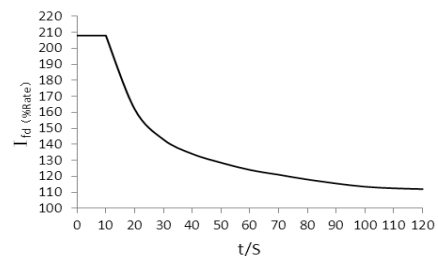


Figure 1. Generator exciting winding current overload capacity.

3.3. Calculation of Dynamic Voltage Stability

Figure 2 shows the steps of full simulation calculation of dynamic voltage stability research. Data preparations include modeling of network parameter, generator, load and other dynamic components. Load increase pattern includes definition of increase range and rate.

In full simulation calculation, the process of system running from stable into instable when it close to critical point may caused by load increase and over-excitation limitation or other automatics like ULTC simultaneously or individually. Therefore, without consideration of other automatics, taking over-excitation limitation into account or not would influence the calculation of dynamic voltage stability margin significantly, its computation steps differs obviously.

With load increase continue, the system is getting close to its critical point. When over-excitation limitation is not taking into account, the key factor that cause system instability is load increase. It's a single causal relationship, its computation steps is convenience. But when taking over-excitation into account, the slow dynamic process before instable is a superimposed effect by load increase and over-excitation limitation. To figure out dynamic voltage stability margin precisely in this situation, the dynamic process of over-excitation limitation caused by load increase continuously should be sufficiently considered.

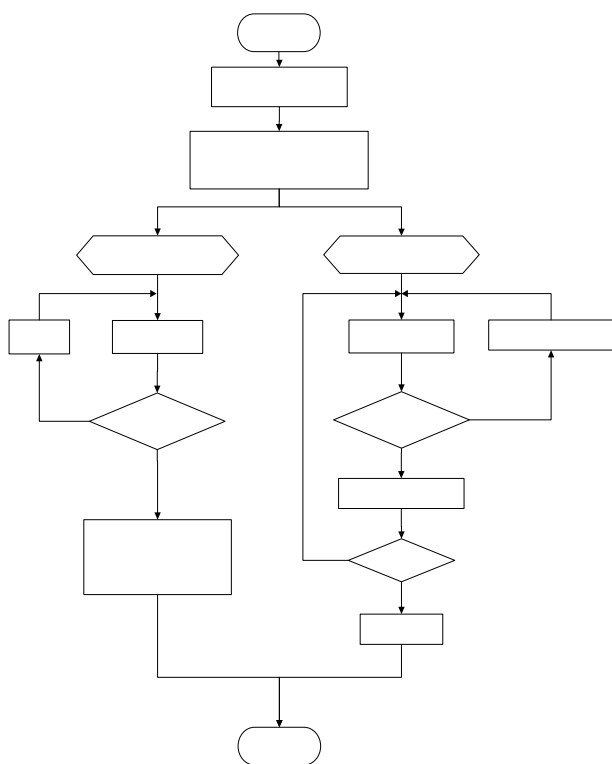


Figure 2. Computation steps of dynamic voltage stability margin full simulation.

In **Figure 2**, T is load increase duration, t_0 is initial value of load increase duration, Δt is changing step of load increase duration, T_{\max} is the maximum length of load increase duration.

When over-excitation limitation is not taking into account, the maximum length of load increase duration T_{\max} under current status and load increase pattern can be figured out by compute one system instability process under load increase continuously, its computation steps are as follows:

- 1) Complete data preparation, confirm load increase pattern, set t_0 value, order $T = t_0$
- 2) Execute full dynamic simulation. With load increase continues, if system runs into instable, execute step 3); if system maintains stable after load increase for T seconds, execute step 4)
- 3) By monitoring system frequency changing, the time point that corresponding to lowest reading frequency is T_{\max} , computation ends.
- 4) Set $T = 2t_0$, repeat step 2).

When over-excitation limitation is taken into account, whether generator over-excitation limitation would cause system instability when load increase for a certain duration should be considered. Hence, load continue increase process should be compute repeatedly, generator over-excitation limit action and system stability situation should be monitored, and searching constantly for value of load increase maximum duration T_{\max} using bisection method. The computation steps are as follows:

- 1) Complete data preparation, confirm load increase pattern, set t_0 value, order $T = t_0$, $\Delta t = \frac{1}{2}t_0$
- 2) Execute full dynamic simulation. With load increase continues, if system runs into instable, execute step 3); if system maintains stable after load increase for T seconds, execute step 4)
- 3) Set $T = T - \Delta t$, $\Delta t = \frac{1}{2}\Delta t$, execute step 5)
- 4) Set $T = T + \Delta t$, $\Delta t = \frac{1}{2}\Delta t$, execute step 6)
- 5) If $\Delta t \leq 0.5$, execute step 6), otherwise repeat step 2)
- 6) Set $T_{\max} = T$, computation ends.

Another caveat here is, full simulation calculation duration must be longer than load continue increase duration T , especially when over-excitation is taking into account. Simulation duration should be long enough to monitor the dynamic process of generator over-excitation limitation and system instability or recovery process after load increase no more.

4. Sample Simulation Analysis

Take certain grid with 280 generators and 2030 nodes to

apply simulation analysis. Use ZM (50% constant impedance + 50% introduction motor) model in load model. And take load frequency factor into account in static parts.

Choose certain receiving grid as load increase sector, set increasing rate to 1%/s, set initial value of load increase duration to $t_0 = 60$ s.

4.1. Without Consideration of Over-excitation Limitation

Without consideration of over-excitation limitation, the result of full dynamic simulation shows: in 60s duration of receiving grid load continuous increase, system gets instable, and load sustainable increase time that corresponding to lowest point of system frequency $T_{max} = 52$ s. See **Figure 3** as below.

In order to verify the result, set load increase duration T to 52s and 53s, and execute simulation respectively. The result of simulation shows when $T = 52$, system runs stably; when $T = 53$, system runs into instability. See **Figure 4** as below.

4.2. With Consideration of Over-excitation Limitation

Taking over-excitation limitation into account, start and repeatedly compute 7 times from $T = t_0 = 60$ s, receiving grid load sustainable increase duration can be figured out: $T_{max} = 23$ s. The result means when $T = 23$, system runs stably; when $T = 24$, system runs into instability. See **Figure 5** as below.

Figure 5 shows:

- 1) The certain point in time that corresponding to lowest system frequency point is no longer the value of load sustainable increase duration T_{max} .
- 2) A longer dynamic adjusting process takes place after load stop increase. Once the generator over-excitation limitation activated and causing system voltage fall suddenly, then system would led to instability. **Figure 6**

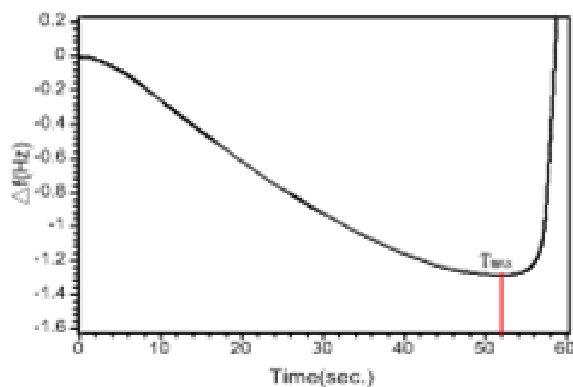


Figure 3. System frequency changing curve without consideration of over-excitation limitation.

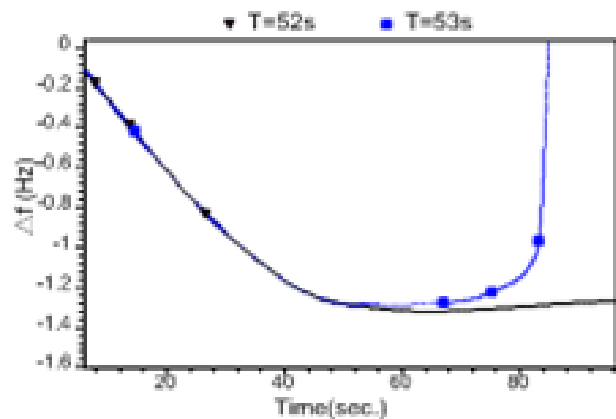


Figure 4. System critical instability frequency changing curve without consideration of over-excitation limitation.

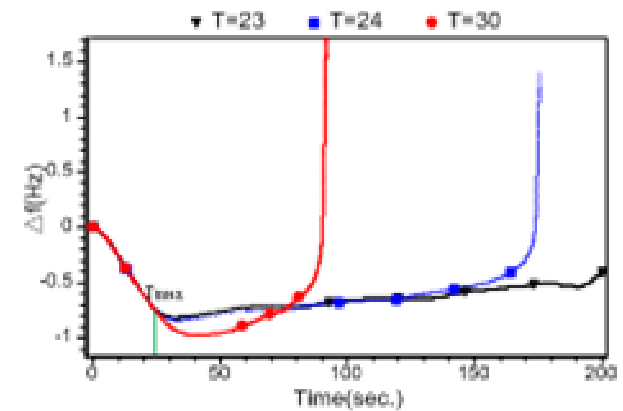


Figure 5. System frequency changing curve with consideration of over-excitation limitation.

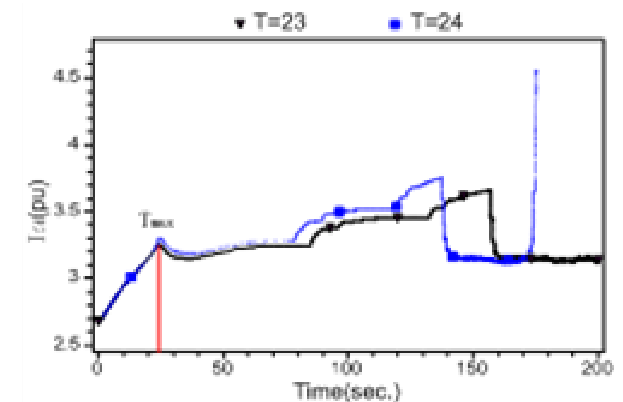


Figure 6. Certain generator excitation current changing curve with consideration of over-excitation limitation

shows certain generator excitation current changing curve in receiving sector.

- 3) The longer the load increases duration last, the faster the system runs into instability. Shown by system frequency changing curve when $T = 30$ s in **Figure 6**.

A final note needs to be mentioned is, load sustainable

increase duration T_{\max} refers to system instability speed under current system situation and load increase pattern. It's not belongs to system dynamic voltage stability margin parameter.

5. Conclusions

This paper uses full dynamic simulation program based on time-domain simulation in dynamic voltage stability research, raise methods and steps to figure out dynamic voltage stability in both with and without consideration of over-excitation limitation, and verifies correctness and effectiveness of methods by sample simulation. The simulation result also fully verifies the effect and influence of generator over-excitation limitation in full dynamic voltage stability research.

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