

A Practical Framework for Reliability and Quality Assessment of Power Systems

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Abstract

This paper presents a new practical framework for evaluating reliability levels associated with power system supply-demand balance. The framework has been developed as part of a recent major industry-supported research and development study. The novel framework is based on three metaphors (dimensions) representing the relationship between available generation capacities and required demand levels. The first metaphor defines whether or not the capacity exists, the second metaphor defines whether or not the capacity is needed, and the last metaphor defines whether or not the capacity can reach (delivered to) the demand. The eight possible combinations associated with the 0/1 (Yes/No) values of the three metaphors would, in turn, define a set of powerful system-wide performance quality measures relating to generation deficiency, redundancy, bottling, etc. Practical applications to a portion of the Saudi power grid are also presented for demonstration purposes. The work of the paper constitutes a new line of research in system reliability assessment where the derived system-wide performance quality indices are capable of addressing and revealing areas of deficiencies and bottlenecks as well as redundancies in the composite generation-demand structure of large-scale power grids. In addition, the sensitivities of the performance quality indices with respect to variations in the system operating parameters represent powerful information, which can be used to assess the level of degradation in the reliability measure or the performance quality index under consideration.

Keywords: Power Systems, Reliability, Quality Assessment, Linear Programming

1. Introduction

Electric power utilities have a key mandate to maintain a continuous and sufficient power supply to the customers at a reasonable cost. Power system cost-effectiveness, security, adequacy and reliability analyses have evolved over the years from mere theoretical topics of limited interest, during the era of generous economy and abundant supply and facilities, to a vital branch in today's highly-competitive business environment of power utility planning and operations [1-4]. In response to the growing interest in system security and reliability by power utilities, several schools of thought have evolved with the associated pioneering research aimed at conducting the security and reliability assessment in an efficient, accurate manner and with as much realization of the business nature and practical circumstances of the power utility as possible. As has happened with many power system disciplines, the prime interest in system security, adequacy and reliability has gradually shifted from completing and refining the theoretical basis, through developing suitable

computational tools for demonstrating the capability and practicality of the methodologies, to upgrading the computational tools to handle the large-scale nature of present power systems and, finally, to relate various security, quality and reliability indices to the practical concerns of utility engineers and executives regarding supply and/or transmission deficiencies as well as the risk associated with ignoring such deficiencies [5,6].

This paper summarizes the results of a recent major industry-supported research and development study in which a novel framework was developed for evaluating performance quality indices associated with power system generation-demand balance. The novel technique utilizes a basic linear programming formulation, which offers a general and comprehensive framework to assess the harmony and compatibility of generation and demand in a power system. Using the method proposed in this paper, integrated system reliability evaluation and quality assessment can be performed globally on the whole system or locally on portions in the power grid. It can be applied to the system under normal operation or subject

to contingencies with certain or random occurrences [7-10]. The methodology presented in this paper has been implemented in an efficient computerized algorithm which analyzes the network structure, generation and load balance and evaluates various composite system performance quality indices. Practical application to a portion of the Saudi power grid is also presented in the paper for demonstration purposes.

2. Problem Formulation

2.1. Network Model

Let n_B = number of buses in the power network, where $n_B = n_L + n_G$, n_L and n_G = number of load and generator buses, respectively. Also, in the network model used, n_T = number of transmission branches (lines and transformers). In order to facilitate subsequent formulation, it is assumed, without loss of generality, that the load buses are numbered as $1, 2, \dots, n_L$ followed by generator buses as $n_L + 1, \dots, n_L + n_G$, where $n_L + n_G = n_B$. For example, the sample power system shown in **Figure 1** has $n_B = 4$, $n_G = 2$, $n_L = 2$ and $n_T = 5$.

Now, let $\mathbf{A} = (n_B \times n_T)$ be the bus incidence matrix representing the connectivity pattern between buses and lines. The entries of \mathbf{A} are either 0, 1 or -1. Therefore, an element $A_{bt} = 1$ if bus b is feeding a transmission branch t ; $A_{bt} = -1$ if bus b is fed from a branch t , otherwise $A_{bt} = 0$. In the current analysis, the \mathbf{A} -Matrix is partitioned row-wise into \mathbf{A}_L and \mathbf{A}_G associated, respectively, with load and generator buses. The rows of \mathbf{A} (or columns of \mathbf{A}^T) represent groups of buses while the columns of \mathbf{A} (or rows of \mathbf{A}^T) represent groups of transmission links. We also note that for practical large-scale networks, the matrix \mathbf{A} is extremely sparse.

2.2. Performance Quality Assessment

Although the basic definitions pertaining to system performance quality are simple to state and often seem

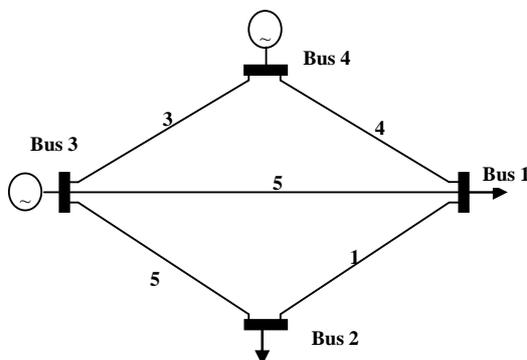


Figure 1. A sample power system.

intuitive at first glance, a great deal of care should be exercised in order to recognize some subtle differences in the definition and formulation of the composite performance quality indices. Let,

$\bar{\mathbf{P}}_T$ =vector of n_T elements representing transmission branch capacities

$\bar{\mathbf{P}}_L$ =vector of n_L elements of peak bus loads

$\bar{\mathbf{P}}_G$ =vector of n_G elements representing generator capacities \bar{P}_g

For simplicity of notation, we shall use \bar{P}_t to denote a general element t of the vector $\bar{\mathbf{P}}_T$ (rather than the more strict notation of $\bar{\mathbf{P}}_{Tt}$). Similarly, we shall use \bar{P}_l and \bar{P}_g to denote general elements of $\bar{\mathbf{P}}_L$ and $\bar{\mathbf{P}}_G$ respectively. However, when confusion may occur, we will use the strict notation of $\bar{\mathbf{P}}_{Tt}$, $\bar{\mathbf{P}}_{Ll}$ and $\bar{\mathbf{P}}_{Gg}$. Now consider the schematic configurations of **Figure 2** which depicts the transfer connectivity between generation through transmission to load.

If, for example the local generation capacity \bar{P}_g at bus g exceeds the corresponding transmission capability $\sum_{t \in T_g} \bar{P}_t$ in **Figure 2(b)**, where T_g denotes the set of transmission branches connected to generator bus g , then using the terminology introduced in the previous section,

we may say that a positive amount of $\left(\bar{P}_g - \sum_{t \in T_g} \bar{P}_t \right)$ of

generation beyond bus g has been bottled (blocked from usage). We should note that such a definition applies to a specific scenario of system configuration (the \mathbf{A} -matrix) and loading conditions. For example, in the above discussion, we assumed that the set T_g does not represent any of pre-defined contingency scenarios. That is, T_g represents the full transmission capacity at bus g .

In addition to the above definitions, we also define – using similar notation—the following vector for later use $\bar{\mathbf{P}}_G$ = Vector of generation *site* capacities, which represents the maximum future expanded generation capacity that could be available at the same generation site.

2.3. Master Linear Program

In the proposed scheme, the integrated system quality

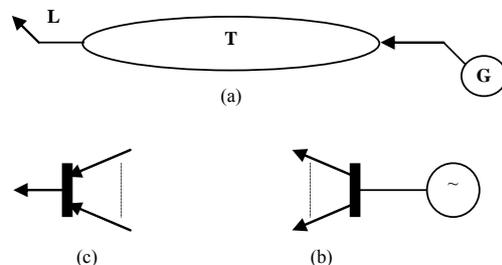


Figure 2. G-T-L transfer connectivity.

assessment is performed via solving a master linear programming problem [11] in which a feasible power flow is established which minimizes the total system non-served load subject to capacity limits and flow equations. The master linear program, which utilizes the network bus incidence matrix \mathbf{A} , is formulated as

$$\begin{aligned} \text{Minimize } f &= \sum_{l=1}^{n_l} (-p_l) \\ \text{with respect to } &\mathbf{P}_L, \mathbf{P}_G \text{ and } \mathbf{P}_T \\ \text{such that } &\mathbf{A}\mathbf{P}_T = \begin{bmatrix} -\mathbf{P}_L \\ \mathbf{P}_G \end{bmatrix} \\ &\mathbf{P}_L \leq \bar{\mathbf{P}}_L, -\mathbf{P}_L \leq \mathbf{0} \\ &\mathbf{P}_G \leq \bar{\mathbf{P}}_G, -\mathbf{P}_G \leq \mathbf{0} \\ &\mathbf{P}_T \leq \bar{\mathbf{P}}_T, -\mathbf{P}_T \leq \bar{\mathbf{P}}_T \end{aligned} \quad (1)$$

In the master linear program, \mathbf{P}_L , \mathbf{P}_G , and \mathbf{P}_T are n_L , n_G and n_T column vectors representing the actual load bus powers (measured outward), generator bus powers (measured inwards) and transmission line powers (measured as per the network bus incidence matrix \mathbf{A}), respectively. The solution of the above linear program provides a more realistic (less conservative) flow pattern in view of the fact that when load curtailments are anticipated, all system generation resources would be re-dispatched in such a way which minimizes such load cuts. The feasible flow pattern established from the Master Linear Program is then used to evaluate various integrated system quality indices through a set of closely related sub-problems. For example, a sub-problem may be defined to evaluate the total system loss of load subject to a given contingency scenario. In this case, the sum of all elements of the \mathbf{P}_L vector is subtracted from the total nominal system load. The resulting amount, if positive, would constitute the total system loss of load (Load Not-Served).

3. Quality Metaphors

3.1. Conceptual Framework

As was indicated before, the novel framework presented in this paper is based on three metaphors (dimensions) representing the relationship between certain system generation capacity and the demand. These metaphors are illustrated in **Table 1**, and relate to the following demand fulfillment issues:

- 1) Need of capacity for demand fulfillment.
- 2) Existence of capacity (availability for demand fulfillment).
- 3) Ability of capacity to reach the demand.

The first metaphor defines whether or not the capacity is needed, the second metaphor defines whether or not the capacity exists, and the last metaphor defines whether

Table 1. Illustration of quality assessment metaphors.

#	Quality Measure	Quality State			Quality Metaphor of a Capacity		
		<i>N</i>	<i>E</i>	<i>R</i>	(<i>N</i>) <i>Needed?</i>	(<i>E</i>) <i>Exists?</i>	(<i>R</i>) <i>Can Reach?</i>
1	Utilized	1	1	1	Yes	Yes	Yes
2	Bottled	1	1	0	Yes	Yes	No
3	Shortfall	1	0	1	Yes	No	Yes
4	Deficit	1	0	0	Yes	No	No
5	Surplus	0	1	1	No	Yes	Yes
6	Redundant	0	1	0	No	Yes	No
7	Spared	0	0	1	No	No	Yes
8	Saved	0	0	0	No	No	No

or not the capacity can reach (delivered to) the demand. The eight possible combinations associated with the 0/1 (Yes/No) values of the three metaphors would, in turn, define a set of powerful system-wide performance quality measures, namely:

1) **Utilized:** A given capacity is said to be **utilized** if it is *needed* (for demand fulfillment), *exists*, and *can reach* the demand.

2) **Bottled:** A given capacity is said to be **bottled** if it is *needed* (for demand fulfillment) and *exists*, but *cannot reach* the demand.

3) **Shortfall:** A given capacity is said to be **shortfall** if it is *needed* (for demand fulfillment) and, anyhow, *does not exist* and *can reach* the demand.

4) **Deficit:** A given capacity is said to be **deficit** if it is *needed* (for demand fulfillment) but, however, *does not exist* and *cannot reach* the demand.

5) **Surplus:** A given capacity is said to be **surplus** if it is *not needed* (for demand fulfillment) although *exists* and *can reach* the demand.

6) **Redundant:** A given capacity is said to be **redundant** if it is *not needed* (for Demand fulfillment) although *exists* but, anyhow, *cannot reach* the demand.

7) **Spared:** A given capacity is said to be **spared** if it is *not needed* (for demand fulfillment) and, anyhow, *does not exist* although *can reach* the demand.

8) **Saved:** A given capacity is said to be **saved** if it is *no needed* (for demand fulfillment) and, anyhow, *does not exist* and *cannot reach* the demand.

We note here that the above performance quality measures are associated with different combinations (topples) of the three quality metaphors, namely, “existence”, “need” and “ability to reach the demand”. The corresponding quality state of a given capacity can be represented, as demonstrated in **Table 1**, by a three-value expression of either a “Yes/No” or “1/0” type indicating

the true/false value associated with each quality metaphor.

As will be demonstrated later, the evaluation of the above quality indices requires the knowledge of the following data types for the demand and various system facilities:

- 1) The value of demand required to be supplied.
- 2) The value of generation capacity as well as the maximum site capacity (the limit of potential increase in existing generation capacity).
- 3) The value of transmission capacity.

3.2. Illustrative Example of Quality Metaphors

As a simple illustrative example, consider the sample 2-bus system of **Figure 3**, where a demand (load) of 50 (per-unit) is supplied by a generating facility having an available capacity of 70 (per-unit) and a site capacity of 90 (per-unit). The load is supplied through a transmission facility having an available capacity of 40 (per-unit) and a route capacity of 100 (per-unit). For this simple system, the quality indices can be easily evaluated by inspection as shown in **Table 2**. In order to facilitate understanding of the meaning of the different quality indices and ensure correct interpretation of their definitions, Appendix I contains a complete list of the quality indices for many case scenarios involving different values of required load supply level as well as generation and generation capacities.

3.3. Large-Scale Implementation

For real life power systems with practical sizes, the quality indices cannot be evaluated by inspection as was done in the previous illustrative example. An appropriate computerized scheme is needed in order to properly evaluate various quality indices according to their stated definitions. The master linear program presented before

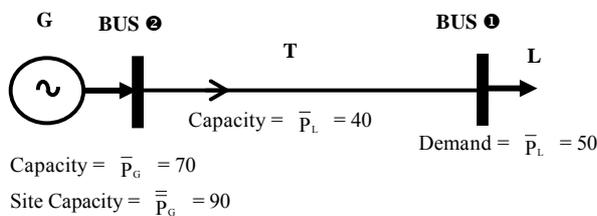


Figure 3. A 2-Bus sample power system.

Table 2. Quality indices for 2-Bus sample system.

\bar{P}_G	\bar{P}_T	\bar{P}_L	$\bar{\bar{P}}_G$	$\bar{\bar{P}}_T$	LNS	<i>(Needed, Exists, Can-reach)</i>							
						000	001	010	011	100	101	110	111
70	40	50	90	100	10	40	10	0	0	0	20	0	20

forms the bases for analyzing and evaluating the quality indices. For example, the *Load Supply Reliability* can be evaluated as follows:

$$LNS_l = \text{Load Not-Served at Load Bus } (l) = (\bar{P}_l - P_l^{(1)})$$

$$LNS = \text{Total System Load Not-Served} = \sum_{l=1}^{n_L} (\bar{P}_l - P_l^{(1)})$$

where the bus loads at the solution of the master linear program are termed as $P_l^{(1)}$, and P_l denotes the solution load value at bus (l).

On the other hand, generation quality indices are defined in terms of the previously defined “1/0” states indicating the (Needed, Exists, Can-reach) true/false values associated with each quality metaphor. We shall use the symbol Q_{gijk} to indicate the generation quality index state. Also, in the following expressions, we shall use $\min\{x, y, \dots, z\}$ to indicate the minimum of x, y, \dots, z . The notation $\langle x \rangle$ will be used to denote $\max\{0, x\}$, that is the maximum of x and zero ($=x$ if $x > 0$, or 0 otherwise). For example, the generation *Utilized Capacity* index is given by

$$\begin{aligned}
 Q_{g111} &= \text{Utilized Capacity} \\
 &\equiv \{needed, exists, can reach\} = \sum_{l=1}^{n_L} (P_l^{(1)})
 \end{aligned}$$

Similarly, the generation *Bottled Capacity* index is given by

$$\begin{aligned}
 Q_{g110} &= \text{Bottled Capacity} \\
 &\equiv \{needed, exists, cannotreach\} \\
 &= \min \left\{ \left[\sum_{l=1}^{n_L} \bar{P}_l - \sum_{g=1}^{n_G} \bar{P}_g^{(1)} \right], \left[\sum_{g=1}^{n_G} \max \left\{ 0, \left(\bar{P}_g - \bar{P}_g^{(1)} \right) \right\} \right] \right\}
 \end{aligned}$$

4. Practical Application

4.1. SEC Quality Indices

The newly developed methodology for power system performance quality assessment has been applied to a practical power system comprising a portion of the interconnected Saudi power grid. The power system consists of two main regions, namely the Central region and the Eastern region.

The two systems are interconnected through two 380 kV and one 230 kV double-circuit lines. The system model used in the current application is shown in **Figure 4**. Three zones are identified in the present analysis, two in the Central region (Riyadh and Qassim zones) and one in the Eastern region.

In this application, three reliability and quality indices are considered, namely the system Load Not-Served (*LNS*), Bottled Generation Capacity (Q_{g110}) and Surplus Generation Capacity (Q_{g011}). The Surplus Generation

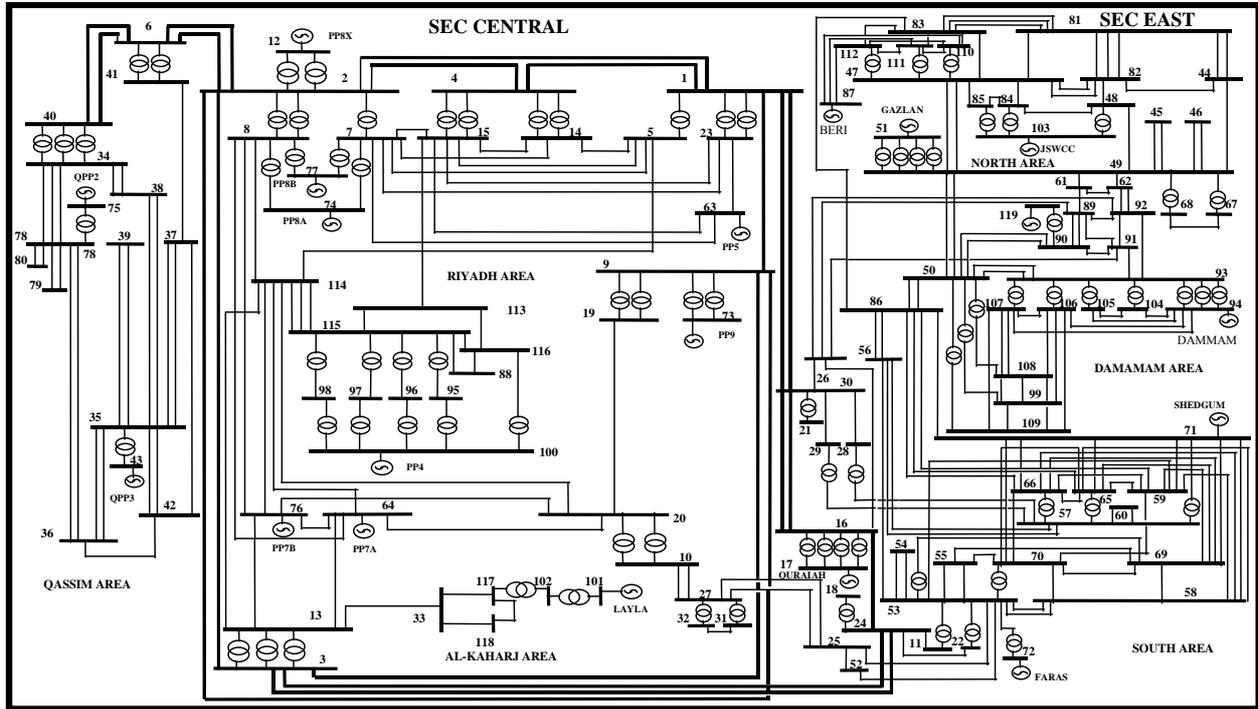


Figure 4. Single-line diagram of study power system.

Capacity (Q_g011) is calculated as

$$\begin{aligned}
 Q_g011 &= \text{Surplus Capacity} \\
 &\equiv \{ \text{not needed, exists, can reach} \} \\
 &= \min \left\{ \max \left\{ 0, \left(\sum_{g=1}^{nG} \bar{P}_g - \sum_{l=1}^{nL} \bar{P}_l \right) \right\}, \right. \\
 &\quad \left. \left[\max \left\{ 0, \left(\sum_{g=1}^{nG} \bar{P}_g - \sum_{l=1}^{nL} \bar{P}_l \right) \right\} \right] \right\}
 \end{aligned}$$

where the generation output values P_g are calculated at the solution of the linear program with open limits on the loads.

Table 3 summarizes some of the performance quality measures applied to the power system for three operating scenarios evaluated at the system peak-demand level (including reserve requirement). The first scenario represents the base system status with all facilities available, the second scenario represents the loss of a major Central-East interface for extended duration, while the third scenario represents the loss of a major generating station in the Eastern region for extended duration. The results of the first operating scenario indicate that the integrity of the supply-demand pattern is preserved in the base-case scenario with no un-served demand or generation bottling. However, there is 130 MW of surplus generation in the Eastern region, where most of the generation facilities of the interconnected system are located.

The results obtained for the second operating scenario reveal that the Load Not-Served in the Central-Riyadh is

450 MW. On the other hand, no Load Not-Served exists in the Central-Qassim zone for the same operating scenario, indicating that this zone has sufficient backup generation with adequate transmission facilities that enable the zone to be somehow shielded from the loss of an interface between the Central and Eastern regions. Also for this scenario, there are 420 MW and 30 MW of bottled generation capacity in the Eastern and Qassim regions, respectively, which would be sufficient to supply the Central-Riyadh zone if the interface facility had not been lost causing separation of the the two interconnected system regions.

It is also of interest to note that no Surplus generation Capacity exists in the Eastern region for this operating scenario, which confirms that the loss of the Eastern-Central interface is the sole reason (causing generation bottling) for the Load Not-Served in the Central-Riyadh zone.

The third operating scenario impacts directly on the generation availability at the Eastern region. The results for this scenario show that there are Load Not-Served in both the Central-Riyadh and Eastern region of 375 MW and 105 MW, respectively. On the other hand, a 30 MW of bottled generation capacity would exist in the Qassim regions, where the flows over transmission lines toward the Central-Riyadh region had already reached their limits.

Incidentally, the total system generation shortfall (Q_g101) in this scenario, which measures the needed-

Table 3. System performance quality assessment measures for three operating scenarios.

{PRIVATE} Power Grid Zone	First Operating Scenario (Base-Case Scenario—All Facilities are Available)		
	Load Not Served (NLS)	Bottled Generation Capacity (Q_g110)	Surplus Generation Capacity (Q_g011)
1. (Central-Riyadh)	-	-	-
2. (Central-Qassim)	-	-	-
3. (Eastern)	-	-	130 MW
{PRIVATE} Power Grid Zone	Second Operating Scenario (Loss of a Major Central-East Interface for Extended Duration)		
	Load Not Served (NLS)	Bottled Generation Capacity (Q_g110)	Surplus Generation Capacity (Q_g011)
1. (Central-Riyadh)	450 MW	-	-
2. (Central-Qassim)	-	30 MW	-
3. (Eastern)	-	420 MW	-
{PRIVATE} Power Grid Zone	Third Operating Scenario (Loss of a Major Generating Station for Extended Duration)		
	Load Not Served (NLS)	Bottled Generation Capacity (Q_g110)	Surplus Generation Capacity (Q_g011)
1. (Central-Riyadh)	375 MW	-	-
2. (Central-Qassim)	-	30 MW	-
3. (Eastern)	105 MW	-	-

yet does not exist—generation capacity which indeed can reach the demand is 345 MW. This shortfall generation is solely attributed to absence of sufficient generation capacity that transmission would otherwise have been able to deliver to the loads had such generation capacity been available.

4.2. Sensitivity Evaluation

While the system reliability and quality indices are valuable on their own, their sensitivities with respect to variations in the system operating parameters represent powerful information, which can be used to assess the level of degradation in the quality index under consideration.

In order to demonstrate this point, **Figure 5** shows the variations of two quality indices, namely the Load Not-Served in the Central-Riyadh area and the total Bottled Generation Capacity in the system, with respect to increase in the system demand level under the first (base-case) operating scenario.

As is expected, the Load Not-Served increases steadily with the increase in system demand. Below the 110% load level (with respect to the base-case level), both the Load Not-Served and Bottled Generation Capacity are equal, indicating that during this range the generation bottling represents the sole reason for demand non-ful-

fillment. Beyond the 110% load level, the two indices are different. While the Load Not-Served keeps increasing, the Bottled Generation saturates at 125 MW at 115% load level. At this point, the generation insufficiency—rather than the transmission limitation—becomes the sole reason for unsupplied demand in the system.

5. Conclusions

This paper has shared the findings and results of a recent major study to formulate—and develop the general theory for—the overall integrated quality indices, and lay the foundation for practical large-scale, network-oriented composite adequacy and reliability determination and assessment. The paper has also taken an important step towards effective and meaningful evaluation of the overall system quality measures by offering a general framework for evaluation of power system performance quality indices. The novel framework is based on three metaphors (dimensions) representing the relationship between certain system generation capacity and the demand. The first metaphor defines whether or not the capacity exists, the second metaphor defines whether or not the capacity is needed, and the last metaphor defines whether or not the capacity can reach (delivered to) the demand. The eight possible combinations associated with the 0/1 (Yes/No) values of the three metaphors would, in turn,

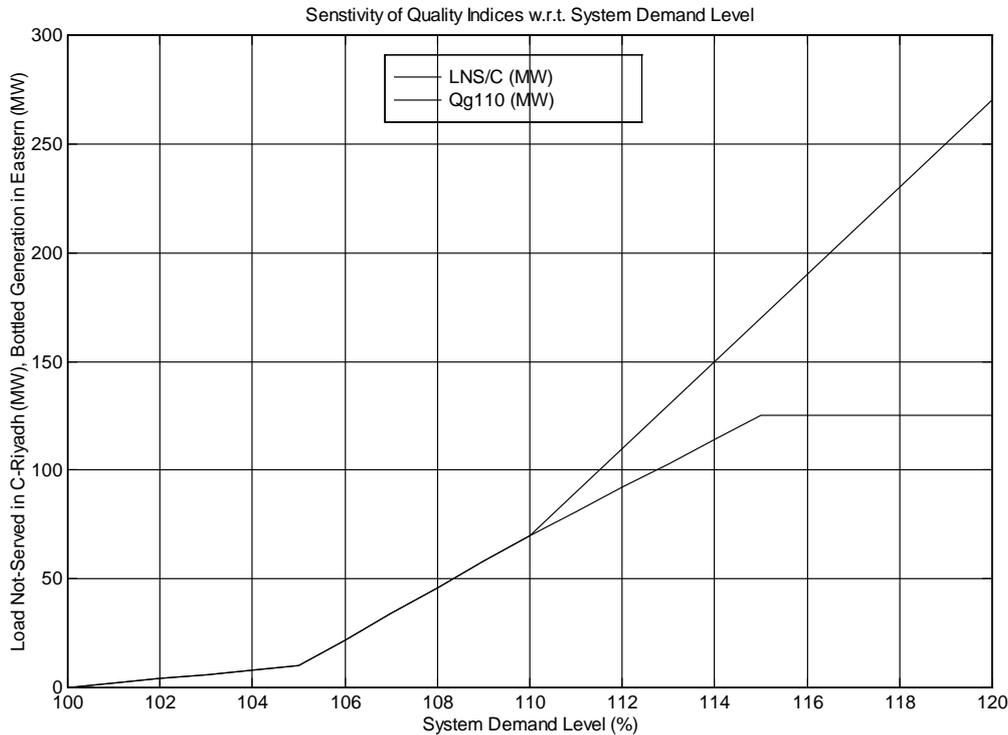


Figure 5. Sensitivity analysis of quality indices.

define a set of powerful system-wide performance quality measures relating to deficiency, redundancy, bottling, etc.

Through the quality assessment formulation introduced in the paper, a general, comprehensive framework is established together with a proper methodology to assess the harmony and compatibility of generation, transmission and demand in power systems. This computer-aided assessment can reveal, in an efficient and reliable manner, areas of deficiencies and bottle-necks in various portions of the system. Furthermore, using the method proposed, integrated system quality assessment can be performed globally on the whole system or locally on portions or even nodes (buses) in the power grid. It can be applied to the nominal system or subject to contingencies.

Based on the solution of the basic linear program described in this paper, a more realistic (less conservative) flow pattern can be established. The more realistic nature of such a flow pattern comes from the fact that when load curtailments are anticipated, all system generation resources would be re-dispatched in such a way which minimizes such load cuts. The feasible flow pattern established from the Master Linear Program is then used to evaluate various integrated system quality indices through a set of subsequent sub-problems. In the practical application presented for the Saudi electricity system, three reliability and quality indices were considered in

the paper, namely the load-not-served (*LNS*), bottled generation capacity (Q_g110) and surplus generation capacity (Q_g011).

The performance quality measures were applied to three operating scenarios evaluated at the system peak-demand level constituting the base-case system (with all facilities available), the loss of a major Central-East interface and the loss of a major generating station in the Eastern region. While adequate supply-demand pattern was preserved in the base-case scenario, notable levels of un-served demand and generation bottling were observed in the two other operating scenarios.

While the system reliability and quality indices are valuable on their own, their sensitivities with respect to variations in the system operating parameters represent powerful information, which can be used to assess the level of degradation in the quality index under consideration. This fact was also demonstrate in the paper where the impacts on two quality indices, namely the Load Not-Served in the Central-Riyadh area and the total Bottled Generation Capacity in the system, were evaluated with respect to potential increase in the system demand level.

6. Acknowledgements

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Appendix

Quality Indices for 2-Bus Sample System

\bar{P}_L	\bar{P}_G	\bar{P}_T	$\bar{\bar{P}}_G$	$\bar{\bar{P}}_T$	LNS	GENERATION INDICES (<i>Needed-Exist-Can-reach</i>)							
						SA 000	SP 001	RE 010	SU 011	DE 100	SF 101	BO 110	UT 111
50	70	40	90	100	10	20	0	20	0	0	0	10	40
105	70	100	90	110	35	0	0	0	0	0	20	0	70
105	70	100	120	110	35	15	0	0	0	5	30	0	70
100	10	70	95	90	90	0	0	0	0	25	60	0	10
100	10	70	195	90	90	95	0	0	0	30	60	0	10
100	10	70	95	130	90	0	0	0	0	25	60	0	10
100	10	70	195	130	90	95	0	0	0	30	60	0	10
100	80	70	95	110	30	0	0	0	0	15	0	10	70
100	80	70	115	110	30	51	0	0	0	20	0	10	70
90	70	100	95	120	20	0	5	0	0	0	20	0	70
90	70	100	145	120	20	45	10	0	0	0	20	0	70
90	120	100	125	135	0	5	0	20	10	0	0	0	90
50	70	300	80	305	0	0	10	0	20	0	0	0	50
50	70	300	310	305	0	10	230	0	20	0	0	0	50
90	100	40	100	80	50	0	0	10	0	0	0	50	40
90	100	40	130	80	50	30	0	10	0	0	0	50	40
90	100	40	100	250	50	0	0	10	0	0	0	50	40
90	100	40	130	250	50	30	0	10	0	0	0	50	40
140	130	70	140	135	70	0	0	0	0	10	0	60	70
140	130	70	170	135	70	30	0	0	0	10	0	60	70
140	130	70	140	145	70	0	0	0	0	10	0	60	70
140	130	70	170	145	70	30	0	0	0	10	0	60	70
130	70	140	80	150	60	0	0	0	0	0	10	0	70
130	70	140	150	150	60	10	10	0	0	0	60	0	70
90	200	190	210	220	0	10	0	10	100	0	0	0	90
50	90	100	95	105	0	0	5	0	40	0	0	0	50
50	90	100	105	105	0	5	10	0	40	0	0	0	50

G = Generation**T** = Transmission**L** = Load**LNS** = load Not Served**UT** = Utilized**BO** = Bottled**SF** = Short-fall**DE** = Deficient**SU** = Surplus**RE** = Redundant**SP** = Spared**SA** = Saved