

Dual DVCC Based Voltage-Mode Digitally Programmable Biquadratic Filter

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ABSTRACT

The recent advances in IC technology have led to the trend of designing hybrid systems to benefit both analog and the digital domain. Among analog circuits, multifunctional filter along with multiphase oscillator constitutes a building block of critical importance. In this paper, a digitally reconfigurable multi-input-multi-output voltage mode multifunctional biquadratic filter has been presented. The circuit comprises of two differential voltage current conveyors (DVCCs), two grounded capacitors and two floating resistors. The digital controllability is incorporated using a current-summing network (CSN). Tunability of quality factor is achieved by the use of a 3-bit digital control word while keeping the resonant frequency constant. PSPICE simulations using TSMC 0.25 µm CMOS technology have been performed to validate the theoretically predicted results.

KEYWORDS

Voltage-Mode; Differential Voltage Current Conveyor (DVCC); Multifunctional Filter; Digitally Controlled Circuits; Current Summing Network

1. Introduction

Voltage-mode active filters exhibiting high input impedance are of great interest as a number of cells can be easily cascaded for the realization of the higher order filters. The significance of the digitally controlled blocks can be appreciated in situations where a filter needs to be designed for the given filter parameters, *i.e.* its cut-off frequency and quality factor. According to the given specifications and the transfer function of the circuit, the values of passive elements are selected to meet the requirements. If any parameter of the circuit is altered, the circuit needs to be designed again and again which is a tedious task. This problem can be alleviated by employing digitally controlled circuits which provide the flexibility to design the circuit for certain discrete values of the parameters instead of the single fixed value in conventional filters. The number of values will depend on the minimum resolution of the control word.

There have been countless applications that involve realization of active transfer functions employing current conveyors, which have received a considerable amount

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of research attention [1]. The continuous-time analog filter is a ubiquitous circuit component in a vast variety of applications including, but not limited to, noise rejection & signal separation in industrial and measurement circuits, feedback of phase & amplitude control in servo loops, smoothing of digitally generated analog signals, audio signal shaping & sound enhancement, and channel separation & signal enhancement in communication electronics.

Among the several variations of current conveyor, the most successful type is second-generation current conveyor (CCII) introduced by Sedra and Smith [2]. However, when it comes to applications demanding differential or floating inputs like impedance converter circuits and current-mode instrumentation amplifiers, which also require two high input impedance terminals, a single CCII block is no more sufficient. Moreover, these applications employ floating elements to minimize the number of used CCII blocks [3]. Considering the obvious drawbacks of CCIIs, a new building block called differential voltage current conveyor (DVCC) building block was introduced [4]. DVCC is a widely used versatile analog building block whose applications exist in the literature [5-9]. In this paper, the Q-factor of multifunctional filter proposed by Chen *et al.* [10] is digitally tuned with the help of a Current Summing Network (CSN). The paper is organized as follows. Section 2 presents a brief description about DVCCs. In Section 3, the circuit proposed in [10] by Chen *et al.* which has been digitally controlled is discussed, followed by Section 4, which gives a brief idea about the operation of the Digitally-Controlled DVCC (DC-DVCC) using CSN. Section 5 deals with the details of the proposed digitally controlled multifunctional biquadratic filter along with its design. Finally, the results are discussed in Section 6, followed by the concluding remarks appearing in Section 7.

2. Differential Voltage Current Conveyor

The DVCC is a five-port, widely used analog building block defined by the following matrix equation [4].

$$\begin{bmatrix} I_{Y_1} \\ I_{Y_2} \\ V_X \\ I_{Z^+} \\ I_{Z^-} \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 1 & -1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & -1 & 0 & 0 \end{bmatrix} \begin{bmatrix} V_{Y_1} \\ V_{Y_2} \\ I_X \\ V_{Z^+} \\ V_{Z^-} \end{bmatrix}$$
(1)

The block level implementation of an ideal DVCC is shown in **Figure 1**, whereas its CMOS transistor realization [4] used in this paper for implementing multifunctional filter is depicted in **Figure 2**.

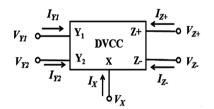


Figure 1. Symbolic representation of the dual output DVCC.

3. CMOS Implementation of DVCC Filter

The implemented voltage mode multifunctional filter [10] is shown in **Figure 3**. Routine analysis of the circuit, yields the following voltage transfer functions of the voltage-mode second order low-pass, high-pass, band-pass and band-reject filters given respectively by Equations (2)-(5).

If $V_{i1} = V_{i3} = V_{in}$ (the input voltage signal) and $V_{i2} = 0$, then

Low Pass:
$$\frac{V_{LP}}{V_{in}} = \frac{\frac{1}{R_1 R_3 C_1 C_2}}{s^2 + \frac{s}{R_2 C_2} + \frac{1}{R_1 R_3 C_1 C_2}}$$
 (2)

High Pass:
$$\frac{V_{HP}}{V_{in}} = \frac{-s^2}{s^2 + \frac{s}{R_2C_2} + \frac{1}{R_1R_3C_1C_2}}$$
 (3)

Band Pass:
$$\frac{V_{BP}}{V_{in}} = \frac{-\frac{S}{R_3C_2}}{s^2 + \frac{s}{R_2C_2} + \frac{1}{R_1R_2C_1C_2}}$$
 (4)

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Band Reject:
$$\frac{V_{BR}}{V_{in}} = \frac{s^2 + \frac{1}{R_1 R_3 C_1 C_2}}{s^2 + \frac{s}{R_2 C_2} + \frac{1}{R_1 R_3 C_1 C_2}}$$
 (5)

where the quality factor, Q and the resonant angular frequency, ω_0 are given by:

$$Q = \frac{R_2 C_2}{\sqrt{R_1 R_3 C_1 C_2}}$$
(6)

$$\omega_0 = \frac{1}{\sqrt{R_1 R_3 C_1 C_2}}$$
(7)

It is to be noted that the low-pass, high-pass, band-pass and band reject functions can be simultaneously realized

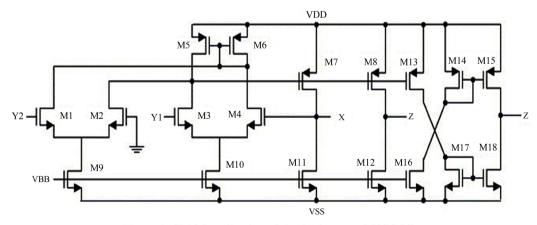


Figure 2. CMOS realization of the dual output DVCC [4].

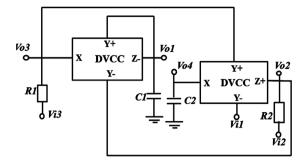


Figure 3. Circuit diagram of voltage mode multifunctional filter with two DVCCs [10].

without changing the circuit configuration. The multifunctional filter has been designed for a cut-off frequency of 1 MHz with $C_1 = C_2 = 15.9$ pF, $R_1 = R_2 = 10$ kΩ. The responses of the multifunctional filter for the above given design is shown in **Figure 4**. The circuit has been simulated with the help of 0.25 µm technology. TSMC process parameters using PSPICE package have been used for carrying out the analysis and the results are in conformity with the theoretical analysis.

4. Digitally Programmable DVCC

For introducing the digital control in the multifunctional filter we have used Digitally Controllable DVCC (DC-DVCC), shown in **Figure 5**. It's basically a 5-terminal analog building block defined by the following relations:

As defined by the characteristics equations in Equation (8), the voltage on the X-terminal realizes the difference of potentials on terminals Y1 and Y2. Furthermore, the current injected at the X-terminal is replicated by a factor of k to the Z-terminals. For the Z+ and Z- terminals, the conveyed current flows in the same and opposite direction respectively, to the current flowing in the X terminal [11].

For digitally reconfiguring the DVCC and obtaining a digitally controlled DVCC (DC-DVCC), a Current Summing Network (CSN) has been employed at the Z-and Z+ terminal for controlling the current transfer gain parameter k. The gain parameter k can be varied from 1 to $(2^n - 1)$, where n represents the number of transistor arrays. The modified circuit of DVCC *i.e.* Digitally Controlled-DVCC employing a CSN is shown in Figure 6 [11]. The CSN consists of n transistor pairs, the aspect ratios of whose NMOS and PMOS transistors are given by:

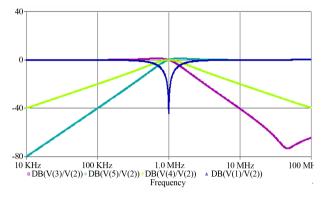


Figure 4. Gain-frequency characteristic (in dB) of the lowpass, high-pass, band-pass and band-reject outputs.

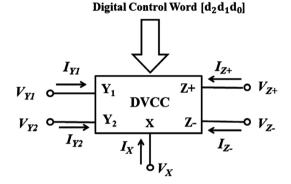


Figure 5. Symbolic representation of the Digitally Programmable DVCC [11].

$$\left(\frac{W}{L}\right)_{i} = 2^{i} \left(\frac{W}{L}\right)_{12} \tag{9}$$

Furthermore, the current at the Z terminal, assumed to be flowing out of the DC-DVCC, can be expressed by:

$$I_Z = \sum_{i=0}^{n-1} d_i 2^i \left(I_7 - I_{11} \right)$$
(10)

Therefore, the proposed DC-DVCC provides a current transfer gain, k equal to:

$$k = \frac{I_Z}{I_X} = \frac{\sum_{i=0}^{n-1} d_i 2^i (I_7 - I_{11})}{(I_7 - I_{11})} = \sum_{i=0}^{n-1} d_i 2^i$$
(11)

where d_i represents the bits applied to the *i*-th branch in the CSN. Now depending upon its value, whether it's a logic 1 or logic 0, the current is enabled or disabled to flow in that particular branch [13-15].

5. Digitally Programmable Multifunctional Filter

In this section, the voltage-mode multifunctional biquadratic filter of **Figure 3** is digitally programmed by using a Current Summing Network (CSN) with electronic control of quality factor as shown in **Figure 7**. The introduc-

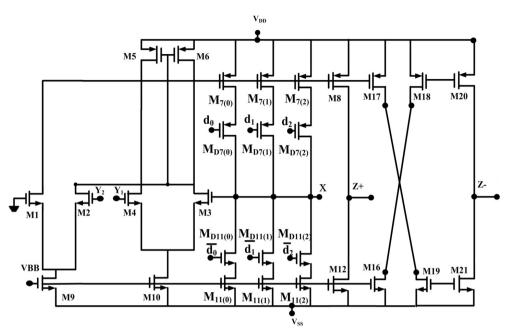


Figure 6. CMOS realization of the digitally programmable DVCC with gain k [12].

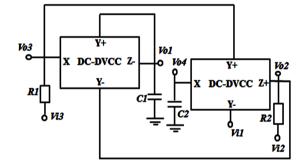


Figure 7. Digitally controlled current-mode biquadratic filter.

tion of the digital control module, comprising of CSN leads to a significant change in the expression of the transfer function of multifunctional filter. The expression for the digitally programmable filter functions can now be expressed as:

Low Pass:
$$\frac{I_{LP}}{I_{in}} = \frac{\frac{1}{R_1 R_3 C_1 C_2}}{s^2 + \frac{s}{k R_2 C_2} + \frac{1}{R_1 R_3 C_1 C_2}}$$
 (12)

High Pass:
$$\frac{I_{HP}}{I_{in}} = \frac{-s^2}{s^2 + \frac{s}{k R_2 C_2} + \frac{1}{R_1 R_3 C_1 C_2}}$$
 (13)

Band Pass:
$$\frac{I_{BP}}{I_{in}} = \frac{-\frac{s}{kR_3C_2}}{s^2 + \frac{s}{kR_2C_2} + \frac{1}{R_1R_3C_1C_2}}$$
 (14)

S

Band Reject:
$$\frac{I_{notch}}{I_{in}} = \frac{s^2 + \frac{1}{R_1 R_3 C_1 C_2}}{s^2 + \frac{s}{k R_2 C_2} + \frac{1}{R_1 R_3 C_1 C_2}}$$
 (15)

The resonant angular frequency, ω_o and the quality factor, Q, are given by:

$$\omega_0 = \frac{1}{\sqrt{R_1 R_3 C_1 C_2}}$$
(16)

1

$$Q = \frac{k R_2 C_2}{\sqrt{R_1 R_3 C_1 C_2}}$$
(17)

where

$$k = \frac{I_Z}{I_X} = \frac{\sum_{i=0}^{n-1} d_i 2^i (I_7 - I_{11})}{(I_7 - I_{11})} = \sum_{i=0}^{n-1} d_i 2^i$$
(18)

where d_i represents the bits applied to the *i*-th branch in the Current Summing Network (CSN).

It can be seen from Equations (16) and (17) that only the expression of quality factor is varying with control word, whereas the cut-off frequency is independent of it. Since quality factor indicates the selectivity characteristic of a filter and it's significance is more with the band pass, as compared to the other filters, so for this digitally controlled circuit focus will be only on the response of band pass filter.Moreover, the circuit utilizes grounded capacitors for the filter's realization, which makes it suitable for integrated circuit implementation.

6. Simulation Results

The proposed digitally controllable multifunctional vol-

tage mode filter has been simulated and all the realizations are designed and verified using PSPICE simulation tool with good results in support of the theory to ensure that the expected functionality is indeed obtained. The CMOS implementation of Digitally Programmable DVCC is shown in Figure 7 and it employs TSMC 0.25 µm CMOS technology process parameters. Figures 8-10 show resultant waveforms of Band Pass Filter for control word [0 0 1], [1 0 1] and [1 1 1] respectively by setting the associated bits to either logic1 or logic 0, where each bit corresponds to a particular binary weight. Furthermore, Figures 11 and 12 illustrate the variation in quality factor and resonant frequency with different control words. Theoretically, the quality factor of digitally controlled band pass filter has a linear relationship with control word, as indicated by Equation (17) and the same is verified with the help of PSPICE simulations, summarized in the form of a graph, shown in Figure 10. The quality factor of the band pass filter is found to vary from 1.01 to 6.33 and resonant frequency is almost constant all

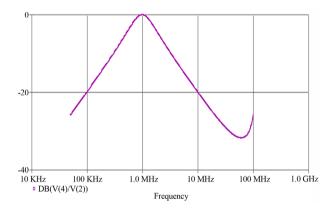


Figure 8. Simulated magnitude response of band pass filter with control word $[d_2 d_1 d_0 = 0 \ 0 \ 1]$ selected Q = 1, fo = 1 MHz.

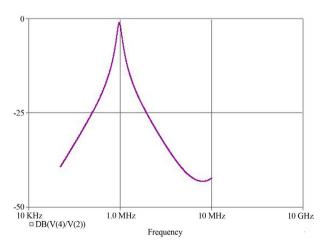


Figure 9. Simulated magnitude response of band pass filter with control word $[d_2 d_1 d_0 = 1 \ 0 \ 1]$ selected Q = 4.23, *fo* = 1 MHz.

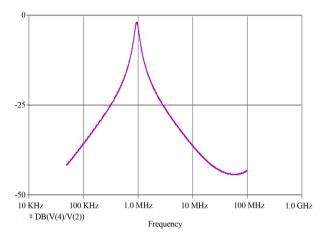


Figure 10. Simulated magnitude response of band pass filter with control word $[d_2 d_1 d_0 = 1 \ 1 \ 1]$ selected Q = 6.13, *fo* =1 MHz.

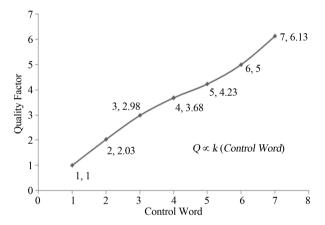


Figure 11. Variation (linear) of quality factor with digital control word.

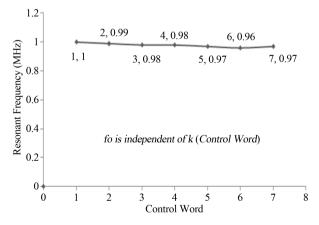


Figure 12. Variation (constant) of resonant frequency with digital control word.

the plots are in excellent mathematical conformity with the transfer functions given in equations. The slight decrease in the resonant frequency is because of the nonideal effects. The performance of the DVCC generally deviates from the ideal behavior since, the voltage and current conveying actions are not exact, therefore leading to slight degradation in performance of the circuit realized using these active elements. In order to account for these non ideal effects, the parameters of α and β are introduced, where α accounts for current transfer gains and β accounts for voltage transfer gains. These transfer gains differ from unity, by the voltage and current tracking errors of the DVCC.

The Digitally Programmed Multifunctional filter can be controlled by a 3-bit control word that can be varied from 1 to 8. However in order to achieve more variation in the Q-factor of the circuit, the digital control word could be increased by adding more transistor pairs in the current summing network of digitally controlled DVCC.

7. Conclusion

In this paper, a novel digitally controllable voltage-mode universal biquadratic filter based on DVCC was presented. Digital tuning has been achieved by the variation of 3-bit digital control word. PSPICE simulations were carried out to ascertain the working of the proposed filters and the results were found to match with the theoretical results.

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