

# Modeling of Surface Waves in a Fluid Saturated Poro-Elastic Medium under Initial Stress Using Time-Space Domain Higher Order Finite Difference Method

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## ABSTRACT

In this present context, mathematical modeling of the propagation of surface waves in a fluid saturated poro-elastic medium under the influence of initial stress has been considered using time dependent higher order finite difference method (FDM). We have proved that the accuracy of this finite-difference scheme is  $2M$  when we use 2nd order time domain finite-difference and  $2M$ -th order space domain finite-difference. It also has been shown that the dispersion curves of Love waves are less dispersed for higher order FDM than of lower order FDM. The effect of initial stress, porosity and anisotropy of the layer in the propagation of Love waves has been studied here. The numerical results have been shown graphically. As a particular case, the phase velocity in a non porous elastic solid layer derived in this paper is in perfect agreement with that of Liu *et al.* (2009).

**Keywords:** Love Waves; Fluid Saturated Initially Stressed Porous Layer; Time-Space Domain; Finite Difference Scheme; Accuracy; Dispersion Analysis; Phase Velocity

## 1. Introduction

The simulation of surface waves propagating in a fluid saturated poro-elastic media is of great importance to seismologists due to its possible applications in geophysical prospecting, reservoir engineering and survey techniques for understanding the cause and estimation of damage due to natural and manmade hazards. Also the difficulty in exploring natural resources is gradually increasing as the nature of the reservoir is more complex and heterogeneous than it was assumed in past and the characterization of the subsurface materials as fluid saturated porous media is more realistic. It is also more accurate to consider soil as two phase composite materials, granular solid and pore fluid. The size of pores is assumed to be small and macroscopically speaking, their average distribution is uniform.

Since poro-elastic theory was developed by Biot [1-3] many efforts have been made in using experimental and numerical methods to characterize elastic wave propagation in porous, liquid-saturated solids. Quite a good amount of information about the effect of initial stress on propagation of surface waves is available in the literature of many authors namely, A. M. Abd-Alla [4], S. Gupta

[5], Shishir Gupta [6]. In these papers they have followed the conventional analytical method to solve these problems. But recently the finite difference method appears as an important tool for numerical simulations of partial differential equations and has been used widely in simulating elastic waves. Due to easy and straightforward approach, robustness, requiring small memory and computation time, the Finite Difference Methods are the most popular methods for seismic modeling. Also wave equation modeling in the time domain is popular because of its easy implementation and accuracy, compared to frequency domain modeling. In time-domain modeling, higher-order differencing operators are used to reduce the required spatial sampling. Virieux [7,8] have used velocity-stress finite difference method for the propagation of P-SV wave and SH wave in heterogeneous media. To improve the accuracy and stability of finite difference scheme, many authors have used and developed different types of difference schemes. Levander [9] applied 4th order approximation in space to the P-SV scheme. Hayashi and Burns [10] developed finite difference scheme with variable grids. R. W. Graves [11] discussed the simulation of seismic wave propagation in 3D elastic me-

dia using staggered-grid finite difference method. Kristek *et al.* [12] considered seismic wave propagation in visco-elastic media using 3D fourth order staggered-grid finite difference scheme. Saenger *et al.* [13] have considered the rotated staggered grid finite difference method. Bohlen *et al.* [14] discussed the accuracy of heterogeneous staggered-grid finite-difference modeling. Kristek *et al.* [15] discussed on the accuracy of the finite-difference schemes for the one dimensional elastic problem. Tessmer [16] discussed Seismic finite difference modeling with spatially variable time steps. Finkelstein *et al.* [17] developed finite difference time domain dispersion reduction schemes. Y. Liu *et al.* [18,19] discussed advanced and truncated finite difference method for seismic modeling and Y. Liu *et al.* [20] employed a plane wave theory and the Taylor series expansion of dispersion relation to derive the FD coefficients in the joint time-space domain for the scalar wave equation with second-order spatial derivatives. They demonstrated that the method has greater accuracy and better stability than the conventional method. Dublain [21] has demonstrated the advantages of the higher order difference scheme. Lie *et al.* [22] designed spatial finite difference stencils on a time-space domain to simulate wave propagation in acoustic vertically transversely isotropic medium. Two-dimensional dispersion analysis and numerical modeling demonstrate that this stencil has greater precision than one used in a conventional F. D. Lie *et al.* [23] discussed finite difference numerical modeling in two phase anisotropic media with even order accuracy. Zhu *et al.* [24] developed finite difference modeling of the seismic response of fluid saturated, porous, elastic solid using Biot theory. Lie *et al.* [25] developed a time-space domain dispersion-relation-based staggered-grid finite-difference schemes for modeling the scalar wave equation. Also, the new stencils can adopt a larger time step. Dispersion analysis and numerical modeling results demonstrate that the new stencils have greater accuracy and can effectively suppress the dispersion and retain the waveform.

In this paper, following [22,25] we have modeled the Love waves in a fluid saturated poro-elastic media under the influence of initial stress using time-space domain higher order finite difference method. The dispersion equation has been obtained and the presence of the porosity parameter, the non-dimensional anisotropic parameter and the non-dimensional parameters due to the initial stress in the equation of dispersion shows the significant effect on the propagation of love waves. The phase velocity of Love wave has been computed numerically and presented graphically. It is observed that the anisotropic parameter in the porous layer and the porosity of the layer both have the increasing effect but the initial stress field has an decreasing effect on the phase velocity

of Love wave.

## 2. Formulation of the Problem and Its Finite Difference Approximation

### 2.1. Formulation

We consider a model consisting of fluid saturated anisotropic poro-elastic layer of finite thickness under compressive initial stress; the  $x$ -axis is chosen parallel to the layer in the direction of propagation of surface wave and the  $z$ -axis is taken vertically downward.

Neglecting the viscosity of the fluid and the body force, Biot's dynamical equations for the fluid-saturated anisotropic porous layer under compressive initial stress are given by [1,2]

$$\begin{aligned} \frac{\partial s_{11}}{\partial x} + \frac{\partial s_{12}}{\partial y} + \frac{\partial s_{13}}{\partial z} - P \left( \frac{\partial w_3}{\partial y} + \frac{\partial w_2}{\partial z} \right) &= \frac{\partial^2}{\partial t^2} (\rho_{11} u_1 + \rho_{12} U_1) \\ \frac{\partial s_{21}}{\partial x} + \frac{\partial s_{22}}{\partial y} + \frac{\partial s_{23}}{\partial z} - P \frac{\partial w_3}{\partial x} &= \frac{\partial^2}{\partial t^2} (\rho_{11} u_2 + \rho_{12} U_2) \\ \frac{\partial s_{31}}{\partial x} + \frac{\partial s_{32}}{\partial y} + \frac{\partial s_{33}}{\partial z} + P \frac{\partial w_2}{\partial z} &= \frac{\partial^2}{\partial t^2} (\rho_{11} u_3 + \rho_{12} U_3) \end{aligned} \quad (1)$$

$$\left. \begin{aligned} \frac{\partial s}{\partial x} &= \frac{\partial^2}{\partial t^2} (\rho_{21} u_1 + \rho_{22} U_1), \\ \frac{\partial s}{\partial y} &= \frac{\partial^2}{\partial t^2} (\rho_{12} u_2 + \rho_{22} U_2), \\ \frac{\partial s}{\partial z} &= \frac{\partial^2}{\partial t^2} (\rho_{12} u_3 + \rho_{22} U_3) \end{aligned} \right\} \quad (2)$$

where  $P = -S_{11}$ , the initial stress along  $x$  axis,  $s_{ij}$ , ( $i, j = 1, 2, 3$ ), are the components of stress tensor in the solid skeleton,  $s (= -fp)$  is the reduced pressure of the fluid ( $p$  is the pressure in the fluid, and  $f$  is the porosity of the porous layer),  $u_i$  are the components of the displacement vector of the solid and  $U_i$  are those of fluid of the porous aggregate,  $w_i$ , ( $i = 2, 3$ ) are the angular displacement vectors. The dynamic coefficients,  $\rho_{11}, \rho_{12}, \rho_{22}$  take into account of the inertia effects of the moving fluid and are related to the densities of the solid  $\rho_s$  the fluid  $\rho_f$  and the layer  $\rho'$  by the equation

$$\rho_{11} + \rho_{12} = (1-f)\rho_s, \quad \rho_{12} + \rho_{22} = f\rho_f,$$

so that the mass density of the aggregate is

$$\rho' = \rho_{11} + 2\rho_{12} + \rho_{22} = \rho_s + f(\rho_f - \rho_s).$$

Also the dynamic coefficients, moreover, obey the inequalities  $\rho_{11} > 0, \rho_{12} \leq 0, \rho_{22} > 0, \rho_{11}\rho_{22} - \rho_{12}^2 > 0$ .

The stress-strain relations for the fluid-saturated anisotropic porous layer under initial stress are given by

$$\left. \begin{aligned} s_{11} &= (A + P)e_{11} + (A + P - 2N)(e_{22} + e_{33}) + Q\varepsilon \\ s_{22} &= (A + P - 2N)e_{11} + (A + P)e_{22} \\ &\quad + (A + P - 2N)e_{33} + Q\varepsilon \\ s_{11} &= (A + P - 2N)(e_{11} + e_{22}) + (A + P)e_{33} + Q\varepsilon \\ s_{12} &= 2Ne_{12}, s_{13} = 2Le_{13}, s_{23} = 2Le_{23}, \\ s &= Qe + R\varepsilon \end{aligned} \right\} \quad (3)$$

where  $e_{ij} = \frac{1}{2}(u_{i,j} + u_{j,i})$  and  $e = \nabla \cdot \mathbf{u}$  and  $\varepsilon = \nabla \cdot \mathbf{U}$  are the corresponding dilatations which opposite in sign,  $A, N, L$  correspond to the familiar Lamé's constants,  $R$  is the amount of pressure required on the fluid to force a certain volume of the fluid into the aggregate while the total volume remains constants and  $Q$  is the coefficient of coupling between the volume change of the solid and that of the fluid.

Also the angular displacements are given by

$$w_2 = \frac{1}{2} \left( \frac{\partial u_1}{\partial z} - \frac{\partial u_3}{\partial x} \right) \quad \text{and} \quad w_3 = \frac{1}{2} \left( \frac{\partial u_2}{\partial x} - \frac{\partial u_1}{\partial y} \right)$$

For the propagation of Love waves along x axis, using conventional conditions,

$$i.e. \quad \mathbf{u} = (0, u_2, 0) \quad \text{and} \quad \mathbf{U} = (0, U_2, 0)$$

where  $u_2 = v(x, z, t)$  and  $U_2 = V(x, z, t)$  the equations of motion given by (1) and (2) are reduced to the form

$$N' \left( \frac{\partial^2 v}{\partial x^2} \right) + L \left( \frac{\partial^2 v}{\partial z^2} \right) = \frac{\partial^2}{\partial t^2} [\rho_{11}v + \rho_{12}V] \quad (4)$$

$$\frac{\partial^2}{\partial t^2} [\rho_{12}v + \rho_{22}V] = 0 \quad (5)$$

where  $N' = N(1 - \xi)$  and  $\xi = P/2N$  is the non-dimensional parameters due to the initial stress.

Eliminating the component of liquid displacement  $V$  from (4) and (5) we have

$$N' \left( \frac{\partial^2 v}{\partial x^2} \right) + L \left( \frac{\partial^2 v}{\partial z^2} \right) = d' \frac{\partial^2 v}{\partial t^2} \quad (6)$$

where

$$d' = \rho_{11} - \frac{\rho_{12}^2}{\rho_{22}} \quad (7)$$

From the Equation (6) it can be seen that the velocities of shear waves in the porous medium in  $x$  and  $z$  directions are  $\sqrt{N'/d'}$  and  $\sqrt{L/d'}$  respectively and from (7),  $d'$  is less than  $\rho_{11}$  and hence, in turn, less than  $\rho'$ , the density of the elastic layer for all values of  $\rho_{12} \neq 0$ . This shows that the velocities of shear waves in  $x$  and  $z$  directions in the fluid saturated porous layer will be more those of corresponding elastic layer.

## 2.2. Finite Difference Approximation

Equation (6) can be written as

$$\gamma \left( \frac{\partial^2 v}{\partial x^2} \right) + \left( \frac{\partial^2 v}{\partial z^2} \right) = \frac{\gamma}{\alpha^2} \frac{\partial^2 v}{\partial t^2} \quad (8)$$

where  $\gamma = \varsigma(1 - \xi)$ ,  $\varsigma = N/L$  and  $\alpha = \sqrt{N'/d'}$ , the velocity of shear wave in the porous medium in  $x$  direction.

The shear wave velocity in the  $x$ -direction may be expressed as

$$\alpha = \beta_a \sqrt{\frac{(1 - \xi)}{d}} \quad (9)$$

where  $d = \gamma_{11} - \gamma_{12}^2/\gamma_{22}$  and  $\beta_a = \sqrt{N/\rho'}$ , the velocity of the shear wave in the corresponding non-porous, initial stress free anisotropic elastic medium along the direction of  $x$ . Also,

$$\gamma_{11} = \rho_{11}/\rho', \quad \gamma_{12} = \rho_{12}/\rho, \quad \gamma_{22} = \rho_{22}/\rho' \quad (10)$$

are the non-dimensional parameters for the material of the porous layer [1,2].

To improve the accuracy we have considered here the higher order finite difference scheme for spatial derivatives as

$$\frac{\partial^2 v}{\partial x^2} \approx \frac{1}{h^2} \left[ a_0 v_{0,0}^0 + \sum_{m=1}^M a_m (v_{m,0}^0 + v_{-m,0}^0) \right] \quad (11)$$

$$\frac{\partial^2 v}{\partial z^2} \approx \frac{1}{h^2} \left[ a_0 v_{0,0}^0 + \sum_{m=1}^M a_m (v_{0,m}^0 + v_{0,-m}^0) \right] \quad (12)$$

As generally higher order finite difference on temporal derivatives scheme requires large space in the computer memory and usually unstable, 2nd order finite difference scheme is used for temporal derivatives as

$$\frac{\partial^2 v}{\partial t^2} \approx \frac{1}{\tau^2} \left[ -2v_{0,0}^0 + (v_{0,0}^1 + v_{0,0}^{-1}) \right] \quad (13)$$

where  $v_{m,j}^n = v(x + mh, z + jh, t + n\tau)$ ,  $h$  is the grid size and  $\tau$  is the time step.

Using (11)-(13) into (8) we have

$$\begin{aligned} & a_0(1 + \gamma)v_{0,0}^0 + \sum_{m=1}^M a_m \left[ \gamma(v_{m,0}^0 + v_{-m,0}^0) + (v_{0,m}^0 + v_{0,-m}^0) \right] \\ &= \frac{\gamma h^2}{\tau^2 \alpha^2} \left[ -2v_{0,0}^0 + (v_{0,0}^1 + v_{0,0}^{-1}) \right] \end{aligned} \quad (14)$$

Using the plane wave theory, let us consider

$$v_{m,j}^n = e^{i[k_x(x+mh) + k_z(z+jh) - \omega(t+n\tau)]} \quad (15)$$

Substituting (15) into (14) and simplifying, we have

$$\begin{aligned} & \frac{1}{2} a_0(1 + \gamma) + \sum_{m=1}^M a_m \left[ \gamma \cos(mkh \cos \theta) + \cos(mkh \sin \theta) \right] \\ &= \gamma r^{-2} \left[ -1 + \cos(\omega\tau) \right] \end{aligned} \quad (16)$$

where  $r = \frac{\tau\alpha}{h}$ ,  $k_x = k \cos \theta$ ,  $k_z = k \sin \theta$ ,  $\theta$ , being the propagation direction angle of the plane wave.

Using the Taylor series expansion for cosine functions, we have from (16)

$$\sum_{m=1}^M a_m \left\{ (1+\gamma) + \sum_{j=1}^{\infty} (-1)^j \frac{[\gamma \cos^{2j} \theta + \sin^{2j} \theta] (m k h)^{2j}}{(2j)!} \right\} + \frac{1}{2} a_0 (1+\gamma) = \gamma \sum_{j=1}^{\infty} (-1)^j \frac{r^{2j-2} (k h)^{2j}}{(2j)!} \tag{17}$$

Comparing the coefficients of  $k^{2j}$ , we get,

$$a_0 + 2 \sum_{m=1}^M a_m = 0 \tag{18}$$

$$\sum_{m=1}^M a_m (\gamma \cos^{2j} \theta + \sin^{2j} \theta) (m)^{2j} = \gamma r^{2j-2}, \tag{19}$$

where  $j = 1, 2, \dots, M$ .

This equation indicates that the coefficients  $a_m$  are the function of  $\theta$ . To obtain a single set of coefficients, an optimal angle has to be chosen. We solve the equation (19) to get  $a_m$  by using  $\theta = \pi/4$  and then  $a_0$  can be obtained from (18).

### 3. Errors and Accuracy

The error function of Equation (17) can be written as

$$\varepsilon = \left| \sum_{j=M+1}^{\infty} \frac{2(-1)^j}{(2j)!} \left\{ \sum_{m=1}^M a_m [\gamma \cos^{2j} \theta + \sin^{2j} \theta] (m)^{2j} - \gamma r^{2j-2} \right\} k^{2j} h^{2j-2} \right| \tag{20}$$

Since the minimum power of  $h$  in the error function (20) is  $2M$ , the accuracy of this finite difference scheme is  $2M$  when we use 2nd order time domain finite difference scheme and  $2M$ -th order space domain finite difference scheme. The increase in  $M$  may decrease the magnitude in errors but may not increase the order of accuracy. As we have used the finite difference scheme in both time domain and space domain, the wave Equation (8) can be solved in both time domain and space domain simultaneously by (14).

### 4. Dispersion Analysis

Let us define a parameter  $\delta$  to describe the dispersion of Finite difference by using Equation (17) as follows:

$$\delta = \frac{v_{FD}}{\beta_a} = \frac{1}{r \pi h_x} \cdot \sqrt{\frac{1-\xi}{d}} \sin^{-1} \left( \sqrt{\frac{r^2}{\xi(1-\xi)}} X \right) \tag{21}$$

where

$$X = \sum_{m=1}^M a_m \left[ \zeta (1-\xi) \sin^2 (m \pi h_x \cos \theta) + \sin^2 (m \pi h_x \sin \theta) \right] \tag{22}$$

If  $\delta$  is equal to 1, then there is no dispersion. However, if  $\delta$  is far from 1, a large dispersion will occur. In calculating  $\delta$ ,  $d \rightarrow 0$ , the grid points per wavelength, ranges from 0.04 to 0.5 and the variation of  $\theta$  is from 0 to  $\pi/4$ .

The presence of  $d$ , the porosity parameter,  $\zeta = N/L$ , the non-dimensional anisotropic parameter and  $\xi = P/2N$ , the non-dimensional parameters due to the initial stress shows that the dispersion curve are affected by these also.

It may be noted that  $(1-d)$  gives the fraction of porosity in the layer. If the layer is non-porous then  $f \rightarrow 0$  and hence  $\rho_s \rightarrow \rho'$  and we find  $\gamma_{11} + \gamma_{12} \rightarrow 1$  and  $\gamma_{12} + \gamma_{22} \rightarrow 0$  which leads to  $\gamma_{11} - \frac{\gamma_{12}^2}{\gamma_{22}} \rightarrow 1$  i.e.

$d \rightarrow 1$ .

Again if  $f \rightarrow 1$  then  $\rho_f \rightarrow \rho'$  and the layer becomes a fluid, and in that case the shear wave velocity in the layer cannot exist which so happens when  $d \rightarrow 0$ .

Thus we have the following:

- i)  $d \rightarrow 1$ , when the layer is non-porous solid;
- ii)  $d \rightarrow 0$ , when the layer tends to be fluid;
- iii)  $0 < d < 1$ , when the layer is porous.

Here we study the dispersion curves for different grid points per wave length, velocities, porosity, anisotropic parameters, non-dimensional parameters due to the initial stress and time steps.

### 5. Numerical Calculation and Discussions

The numerical calculation of the Equation (21) has been done for different values of the parameters  $\gamma$ ,  $d$  and by taking,  $\alpha = 1500$ . The phase velocity  $v_{FD}/\beta_a$  of Love wave from the Equation (21) versus  $h_x$ , the grid points per wavelength, has been computed for different values of

$$d = 1, 0.95, 0.90, 0.85, 0.80, \dots, 0.45,$$

$$\xi = P/2N = 0, 0.2, 0.4, 0.6, 0.8, \quad \zeta = N/L = 1, 2,$$

the propagation angle  $\theta = 0, \pi/16, \pi/8, 3\pi/16, \pi/4$  and  $t = 0.0005, 0.001, 0.0015, 0.002, 0.0025, 0.003$ .

Figures 1-3 display the dispersion curves of Love waves with respect to different grid points per wave length, at different values of  $M$  in a homogeneous non porous initial stress free elastic solid, porous isotropic and anisotropic layer under the influence of initial stress respectively. It is found that dispersion is more for the lower values of  $M$  and less for higher values of  $M$ . Here

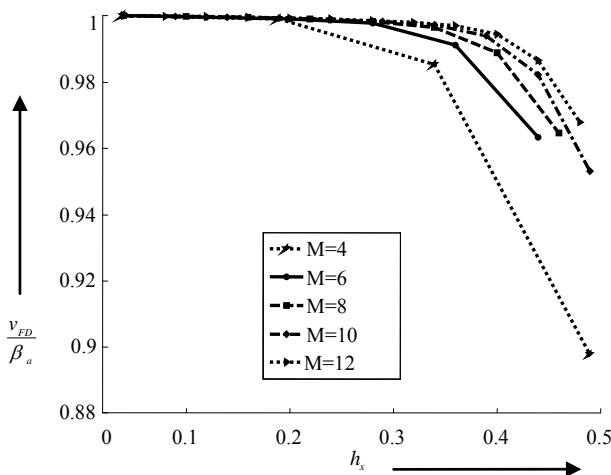


Figure 1. Dispersion curves for love waves for different values of  $M$  when  $\zeta = 1$ ,  $d = 1$  and  $\xi = 0.0$ .

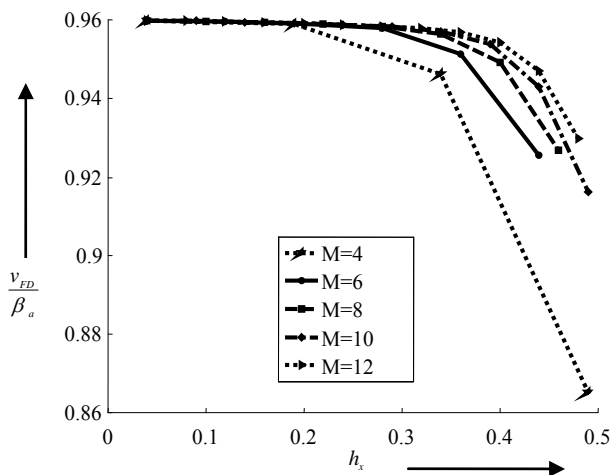


Figure 2. Dispersion curves for love waves for different values of  $M$  when  $\zeta = 1$ ,  $d = 0.8$  and  $\xi = 0.2$ .

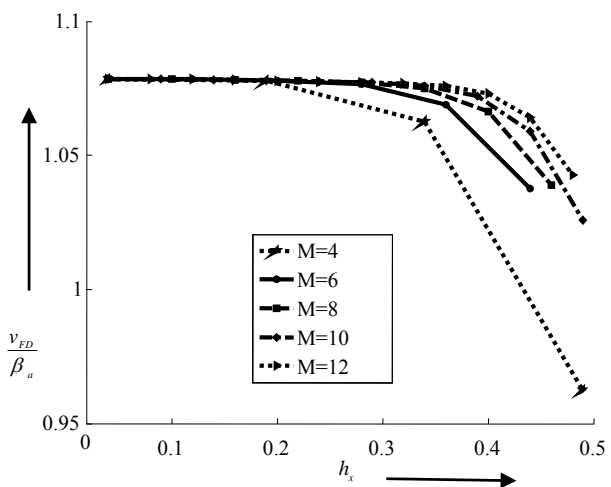


Figure 3. Dispersion curves for love waves for different values of  $M$  when  $\zeta = 2$ ,  $d = 0.8$  and  $\xi = 0.2$ .

also it is observed that the increase in porosity and anisotropy leads to the increase in the magnitude of the phase velocity of Love waves whereas the increase in initial stress parameter leads to decrease in the phase velocity of Love waves.

Figure 4 shows the effect of porosity in the dispersion of phase velocity of Love waves with respect to different grid points per wave length in a homogeneous, isotropic porous layer without initial stress field and under the influence of initial stress. It is observed that as the porosity increases, that is, as the value of  $d$  decreases, the phase velocity of Love wave increases and decreases as the initial stress field increases.

Figures 5 and 6 show the effect of initial stress field in the propagation of Love waves with respect to different grid points per wave length in an isotropic and anisotropic non-porous elastic solid and fluid saturated porous layer. As the anisotropy increases, the phase velocity of Love wave increases and the phase velocity of Love

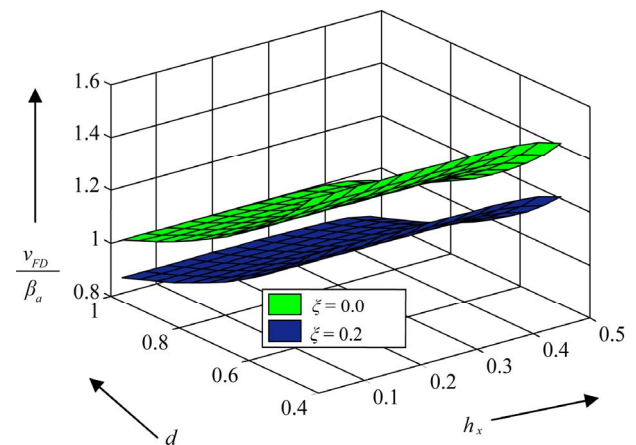


Figure 4. Dispersion curves for love waves for different values of porosity  $d$  and initial stress  $\xi$  when  $\zeta = 1$ .

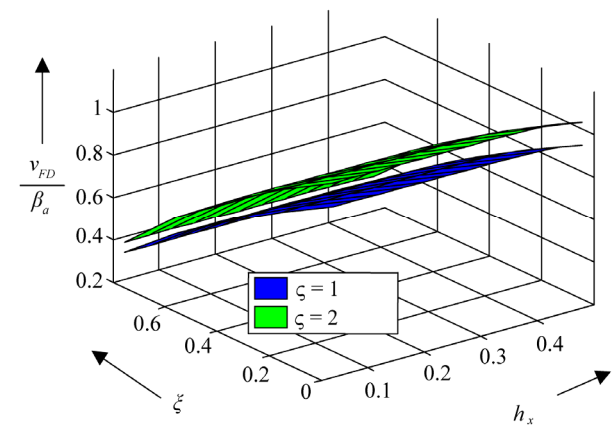
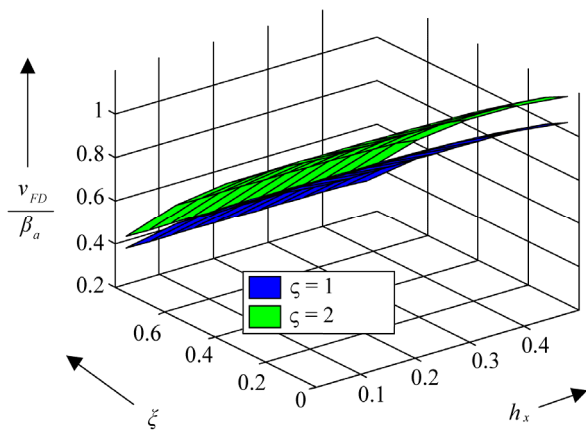


Figure 5. Dispersion curves for love waves for different values of initial stress  $\zeta$  and anisotropic parameter  $\xi$  when  $d = 1$ .



**Figure 6.** Dispersion curves for love waves for different values of initial stress  $\xi$  and anisotropic parameter  $\zeta$  when  $d = 0.8$ .

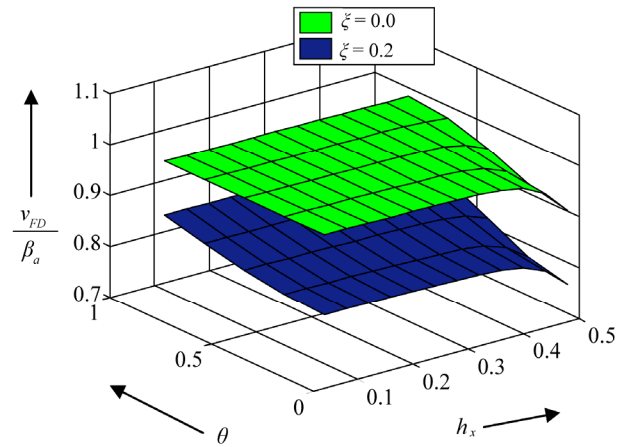
wave decreases as the initial stress field increases.

**Figures 7 and 8** display the dispersion curves of Love waves with respect to different grid points per wave length at different angles of propagation in a homogeneous fluid saturated porous layer and non-porous elastic solid layer for different values of initial stress respectively. It is observed that dispersion is more for the lower degree of propagation angles as compare to the higher degree of angle. Phase velocity is more in fluid saturated porous layer than in non-porous elastic solid layer. Later is the case discussed by Yang Liu *et al.* [20].

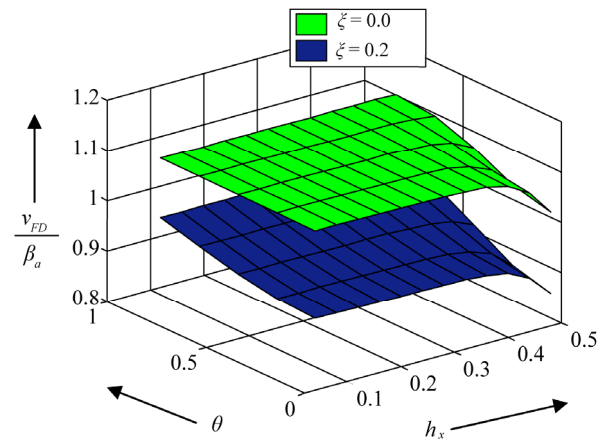
**Figures 9 and 10** displays the dispersion curves of Love waves with respect to different grid points per wave length at different time steps in a homogeneous non porous elastic solid and non-homogeneous, anisotropic fluid saturated porous layer without initial stress field and under the influence of initial stress respectively. It is found that initially the dispersion is less and as time increases, the dispersion increases.

### 6. Conclusion

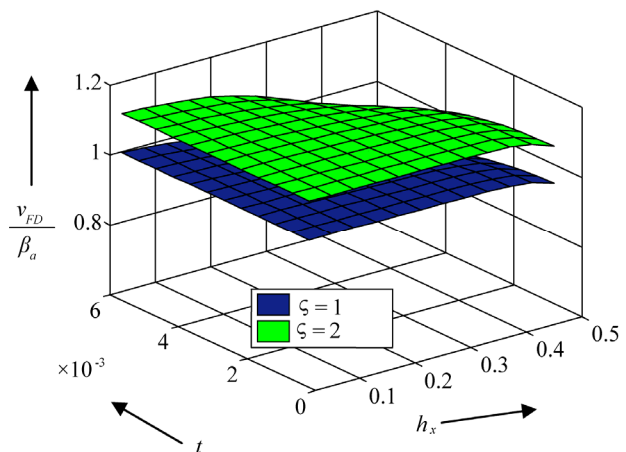
It is observed that the higher order time dependent finite difference method plays an important role in the propagation of Love waves in a porous layer under the influence of initial stress. Graphically we have shown that the dispersion curves of Love waves are less dispersed for higher order finite difference method. It has also been shown that initially the dispersion is less and as time increases, the dispersion increases. The significant effect of porosity, anisotropy and initial stress simultaneously in the propagation of Love waves in a porous layer has also been discussed. The phase velocity of Love wave is more in fluid saturated porous layer than in non-porous elastic solid layer. The anisotropy has an increasing effect whereas the initial stress field has a decreasing effect on the



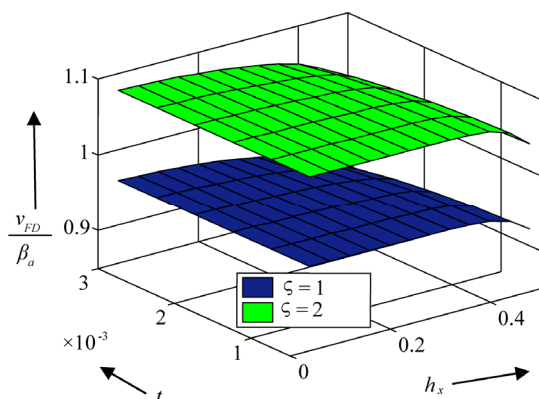
**Figure 7.** Dispersion curves for love waves at different propagation angle  $\theta$  for different values of initial stress  $\xi$  when anisotropic parameter  $\zeta = 1$  when  $d = 1$ .



**Figure 8.** Dispersion curves for love waves at different propagation angle  $\theta$  for different values of initial stress  $\xi$  when anisotropic parameter  $\zeta = 1$  when  $d = 0.8$ .



**Figure 9.** Dispersion curves for love waves waves at different time steps for different values of anisotropic parameter  $\zeta$  when initial stress  $\xi = 0$  and  $d = 1$ .



**Figure 10.** Dispersion curves for love waves at different time steps for different values of anisotropic parameter  $\zeta$  when initial stress  $\xi = 0.2$  and  $d = 0.8$ .

phase velocity of Love waves.

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