

Thermal and Mechanical Modeling of Fluid and Heat Flow in a Porous Metal Using Neural Networks for Application as TPS in Space Vehicles

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Abstract

This paper contains novel model using feedback neural networks for a work piece temperature prediction. The heat and mass transfer in a porous metal workpiece which is heated by a fire gun is studied. The heat flux distribution is determined by thermocouple connected on the workpiece at definite distances. The gun work piece distance were also change and the temperature distribution and heat flux were determined. The permeability's were in range of 0.01 - 0.15. The ANN model parameters of the result output were simulated using the ANN parameters the simulation was done using MATLAB 6.0[®] Neural Network Toolbox.

Keywords: Neyral Network, Porous Media, Prous Passages

1. Introduction

The heat and mass transfer in a porous metal workpiece which is heated by a fire gun is studied. The heat flux distribution in a workpiece due to effect of thermal spray nozzle (uniform external heat source) causing high radiation conduction and convection transfer in the workpiece. The flame gun was kept at various distance and the effect of the source studied for the radiation and convection. This work mainly deals with the studies on heat flux and temperature prediction in a metal workpiece subjected to firing gun (fired using mixture of oxygen and acetylene gas) generally used for gas cutting and welding operations

Studies on Flow and transport at interface between a porous medium and clear fluid have been studied widely. Fauchius, Vandelle and others [1] studied the mechanisms and models for Thermal spraying. Sampath and Jiang [2] discussed the procedures for computing design parameters in Substrate temperature spray coatings. Pop [3] did studies on modeling of heat flow in a porous cavity. Lai [4] studied the effect of Non-Darcy Convection in the free surface of a porous media. In this paper a general treatment of convection force and the effect of free surface hydrodynamics on the heat transfer is dealt with. A novel model incorporating computation of

local and average heat flux has been discussed. Ras [5,6] did studies on the free surface convection while others including Lai [4] studied the Forced convection on the surface of porous layer. Pop and Postelnicu [7] discussed on the effect of heat generation effect on the layers in porous media.

Flow and transport at interface between a porous medium and clear fluid is of importance in heat transfer in porous enclosures and extended surfaces. The mechanisms that contribute to the enhanced heat transfer include heat conduction in the metal foam matrix (whose conductivity is always higher by several orders of magnitude). The well known Darcy's law is based on a balance between the present gradient and the viscous forces and breaks down for high velocities when inertia terms are no longer negligible. Here we present numerical and experimental results for buoyancy induced flow in a high porosity metal foam

The Associative Neural network (ASNN) is an extension of the ANN that goes beyond a simple/weighted average of different models. Associative Neural network represents a combination of an ensemble of feed-forward neural networks and the k -nearest neighbor technique. It uses the correlation between ensemble responses as a measure of distance amid the analyzed cases for the ANN. This corrects the bias of the neural

network ensemble. An associative neural network has a memory that can coincide with the training set. If new data becomes available, the network instantly improves its predictive ability and provides data approximation (self-learn the data) without a need to retrain the ensemble. Another important feature of ASNN is the possibility to interpret neural network results by analysis of correlations between data cases in the space of models. BAM (binary associative memory) is the recurrent memory achieved by the exemplar on being trained by standard inputs prior to its deployment for modeling and simulation applications

2. Experimental Methods:

The heat flux distribution is determined by thermocouple connected on the workpiece at definite distances. The gun work piece distance were also changed and the temperature distribution and heat flux were determined. Cu-Ni Thermocouples were attached on the surface of the workpiece. The flame was generated by acetylene and oxygen gasses as in gas welding process, the flame was kept at distances from 5 cm to 20 cm and the heat flux distribution studied.

During a typical experimental run the powers were varied to achieve different base late temperature and hence Rayleigh numbers. Due to temperature constraints the parameters of the heat input were restricted to maximum base plate temperature of 80*c a metal foam sample heated from above .

The foam sample is saturated with & surrounded by a fluid, which extends a distance s_1 in x direction and s_2 in y direction.

The steady two dimensional equations for the fluid saturated porous medium & for the clear fluid region outside the metal foam are written separately as shown below.

The Flow in a Square Pore cavity is modeled using the continuity and energy equations using a square computational grid with velocity and temperature boundaries.

The continuity and energy equations are given by

$$\frac{\partial u}{\partial r} + \frac{\partial v}{\partial \theta} = 0 \quad (1)$$

$$\frac{1}{\varepsilon^2} \frac{u \partial u}{\partial r} + \frac{v \partial v}{\partial r} = a \left[\frac{\partial^2 u}{\partial r^2} + \frac{\partial}{\partial \theta^2} + \rho \frac{\partial T}{\partial \theta} \right] \quad (2)$$

where volumetric heat sources (r, y, z) represents the contribution of frictional heating. The parameters ρC_p & k_e may depend on y & z but remain independent of r . More importantly the contribution of axial conduction deferred to the subsequent is neglected, hence Equation (4) reduces

$$u \frac{\partial u}{\partial r} + v \frac{\partial v}{\partial r} a \left[\frac{\partial^2 u}{\partial r^2} + \frac{\partial^2 v}{\partial \theta^2} \right] + \frac{\mu}{k \rho c_p} (u^2 + v^2) \quad (3)$$

$$\begin{aligned} & u \frac{\partial T}{\partial r} + v \frac{\partial T}{\partial r} \\ & = \frac{\partial}{\partial r} \left[\lambda \frac{\partial T}{\partial r} \right] + \frac{\partial}{\partial \theta} \left[\lambda \frac{\partial T}{\partial \theta} \right] + (1 - \varepsilon) Q_0 \end{aligned} \quad (4)$$

where the Heat generation number Q_d is given by

$$Q_0 = \frac{L_{ref}^2}{\alpha_f \rho_f C_{pf}} \frac{q''}{(T_h - T_c)} \quad (4a)$$

The governing equations are scaled on basis of fluid Raleigh number as in the case of viscous fluid (independent of permeability) instead of modified Raleigh's number. The scaling is introduced to study the effective change in values of individual matrix & fluid parameters (6). Finite element method is used for prediction of parameters. A suitable grid scheme with iso-parametric, quadrilateral elements is used for stability of numerical solution, all the elements are containing 8 nodes, one at each corner and one at midpoint of each of the sides. All nodes are given velocity & temperature boundaries and corners of the grid pressure boundaries. This is an accepted practice given by Taylor (2). For depicting the variation in pressure by the shape function M_i of one order less than shape function N_i defined for velocities and temperature.

2.1. Direct Problem:

$$\rho C_p \frac{\partial T}{\partial r} = k \frac{\partial}{\partial r} r \frac{\partial T}{\partial r} + \frac{\partial^2 T}{\partial z} \quad (5)$$

$$-\frac{k \partial T}{\partial z} = q(r, t) \quad t > 0 \quad r \in (0, R) \quad z = H \quad (5a)$$

$$\frac{\partial T}{\partial n} = 0 \quad z = 0, r = [0, R] \quad (5b)$$

$$T = T_0 \quad t = 0 \quad \text{at } r \in [0, R] \quad (5c)$$

2.2. Sensitivity Problem

$$\rho C_p \frac{\partial \delta T}{\partial r} = k \frac{\partial}{\partial r} r \frac{\partial \delta T}{\partial r} + \frac{\partial^2 \delta T}{\partial z} \quad (6)$$

$$\frac{k \partial \delta T}{\partial z} = q(r, t) \quad t > 0 \quad r \in (0, R) \quad z = H \quad (7)$$

$$\frac{\partial \delta T}{\partial n} = 0, z = 0, r = [0, R] \quad (8)$$

2.3. Adjoint Problem

$$J(q) = \sum \sum r [T(r_{ms}, z_{ms}, t; q) - Y_{ms}(t)]^2 \quad (9)$$

where $T(r_{ms}, z_{ms}, t, q)$ is the temperature calculated at the measuring points (rms) through the direct problem Equations 5 & (5a)-(c), $Y_{ms}(t)$ is measured temperature and the subscript ms denotes the thermocouple number.

The adjoint problem is obtained by introducing the Lagrange multiplier $\psi(r, z, t)$ into the direct problem equations and by integrating over the spatial and then over the temporal domain as follows.

For the region $r \in (0, R), z \in (0, H)$

$$\rho C_p \frac{\partial T}{\partial t} = k \frac{\partial}{\partial t} \left[\frac{r \partial \psi}{\partial r} + \frac{\partial^3 \psi}{\partial z^3} \right] \quad (10)$$

$$= [T(r, z, t, q) - Y(t)] \frac{\delta(r - r_w)}{\delta(z - z_{ms})} \text{ at } t > 0$$

$$\frac{\partial \psi}{\partial n} = 0, z = 0, r = [0, R], z = 0, H \quad (11)$$

$$\psi = 0 \text{ at } t = t_f, r \in [0, R], z = 0, H \quad (12)$$

where $\delta(\dots)$ is the Dirac delta function. It is required for solving the adjoint equations with the end condition at time $t = t_f$, one should first proceed with variable change $\tau = t - t_f$, The adjoint problem becomes an initial value problem in τ via the transformation.

Step size and Gradient

The iterative equation for determining $q(r, z, t)$ can be given by

$$q^{n+1}(r, t) = q^n(r, t) - \beta P^n(r, t) \quad (13)$$

where the superscript n denotes the iteration number and β^n is the search stepsize defined by

$$\beta^n = \frac{\int_0^H \int_0^H [\delta T^n(r_{mz}, z_{ms}, t; q) - Y_{ms}(t)] dr dt}{\int_0^H \int_0^R r \delta T^n(r_{mz}, z_{ms}, t; q)^2 dr dt} \quad (14)$$

and the descending direction P^n is estimated by

$$p^n(r, z, t) = \psi^n + \gamma^n p^{n-1}(r, z, t) \quad (15)$$

Where $n = 1, \gamma^1 = 0$. General definition of γ is given by

$$\gamma^n = \frac{[\psi(q^n), \psi(q^n) - \psi(q^{n-1})]}{\|\psi(q^{n-1})\|^2} \quad (16)$$

where $\|\cdot\|$ represents the norm and (\cdot, \cdot) the scalar product.

Time stepsize and algorithm stop criterion

The stopping criterion is satisfied when the Fourier

Table 1. Properties of workpiece (Cu).

Thermal conductivity	$k = 396 \text{ W/m}\cdot\text{c}$
C_p	$389 \text{ J/kg}\cdot\text{c}$
Density	8900 kg/m^3

Table 1a. Artificial Neural Network (ANN) variable description.

Category	Parameter	Lower limit	Upper limit	Neuron number
Input pattern	D gun workpiece distance	30	100	1
	t -preheating time s	0	10	1
	Y_1 First thermocouple temperature	10	60	3
	Y_2 second thermocouple temperature	10	65	2
	Y_3 third thermocouple temperature	10	60	5
Output pattern	radial position mm	0	50	4
	q -heat flux Mw/sqm	0	1.2	1

number (F_o) satisfies the condition

$$F_o = \frac{k}{\rho C_p} \cdot \frac{\Delta t}{H_p} > 0.05 \quad (17)$$

where $F_o = 0.028$, Δ is the time step, and H_p is the location of thermocouples to the surface in front of the flame, according to parameters listed in **Table 1**.

Since the Fourier number satisfies Equation (17), the increase of measuring errors is weak and few obvious noisy signals can be captured. In this study, $\Delta t = 0.5 \text{ s}$ has been considered for the time step according to the limit of data acquisition system. If the problem contains no noisy signals, the general stopping criterion condition is expressed by

$$J(q) < \varepsilon \quad (18)$$

Where ψ is specified stopping criterion. But the measurement precision of data ψ acquisition is about 10^{-3} . Hence it should not be reasonable to expect the functional Equation (9) to be equal to zero. A small value of $\varepsilon = 0.002$ is chosen for above criterion

Algorithm for CGM method

The algorithm for Conjugate gradient method (CGM) is given below.

- 1) Select an initial guess $q^n(r, t)$. generally equal to zero.
- 2) Calculate the direct problem, Equations (1)-(4), obtain the solution $T(r_{ms}, z_{ms}, t; q^n)$.
- 3) Decide if the stopping criterion Equation (18) is satisfied. If yes go to step (6), otherwise continue.
- 4) Solve the adjoint problem. Equations (10)-(12) [note: $\tau = (t_1 - t)$ in place of t], calculate the conjugate

Table 2. ANN output results of parameters.

Time <i>t</i> secs	<i>y_r</i>	<i>y_p</i>	<i>E_t</i>	<i>I_{k1}</i>	<i>D</i> m	<i>Y₁</i> m	<i>Y₂</i> m	<i>Y₃</i> m	Radial posn	heat flux <i>q</i> MW/sqm
8	0.87	0.54	0.05	0.51	0.056	0.028	0.039	0.06	20	0.7
9	0.92	0.63	0.07	0.73	0.082	0.035	0.054	0.064	22	0.81
10	1.01	0.78	0.095	0.81	0.093	0.055	0.07	0.073	26	0.98
12	1.21	0.91	0.11	0.96	0.098	0.07	0.085	0.082	29	1.03

Table 3. Computation of flux parameters using CGM.

Time <i>t</i> secs	<i>n</i> (cm)	<i>Pⁿ(r, z, t)</i>	<i>qⁿ⁺¹(r, t)</i>	<i>T_f</i>	<i>T</i>	$\tau = T_f - T$	<i>E_o'</i>	γ	<i>q'</i>	<i>F_o</i>	<i>Q_d</i>
2	2	1.83	0.628	340	280	60	0.15	1.5	2.43	0.185	0.003
	4	1.84	0.651	347	284	63	0.173	1.48	2.45	0.21	0.0034
	6	1.91	0.731	378	293	68	0.18	1.54	2.63	0.27	0.0041
4	2	1.41	0.78	390	297	72	0.21	1.64	2.71	0.32	0.0046
	4	1.63	0.82	410	302	78	0.28	1.81	2.91	0.45	0.0047
	6	1.73	0.87	412	308	81	0.32	1.92	3.12	0.51	0.0049
6	2	1.45	0.81	402	304	74	0.23	1.71	2.8	0.41	0.005
	4	1.71	0.92	408	307	76.3	0.28	1.81	2.9	0.43	0.0051
	6	1.81	1.02	415	308	77.4	0.41	1.93	3.2	0.48	0.0053
8	2	1.84	1.08	418	312	79	0.48	2.01	3.43	0.52	0.0054
	4	1.86	1.13	421	315	81	0.51	2.11	3.51	0.58	0.0056
	6	1.91	1.31	428	321	85	0.61	2.33	3.81	0.7	0.0058

coefficient γ^n , Equation (19) and the direction of descendent p^n Equation (18).

5) Solve the sensitivity problem Equations (5)-(8), calculate the stepsize β^n from the *n*th to the (*n*+1)st iteration, Equation (17) and calculate a new vector q^{n+1} . Go to step 2.

6) The iteration is terminated.

3. A Neural Computational Procedure

The heat flux calculated by solving the inverse problem was correlated to the workpiece temperature and other parameters with the aid of an artificial neural network (ANN). Such a structure considers three main categories.

1) The processing and the experiment design parameters with aid of an artificial neural network (ANN). Such a structure considers following types.

2) The processing and experiment design parameter as an input (1) pattern. These were the gun workpiece distance, the preheating time, the thermocouple temperatures and radial position.

3) The heat flux as an output (O) unit calculated using CGM.

4) An intermediate structure called hidden layers, encoding the correlations between I/O patterns.

Each of the ANN types is defined by a set of neurons playing role of simple processing elements as in **Table**

1a. A neuron has ability to receive a sum of numbers from other neurons and to emit a signal number toward other neurons according to

$$I_{k1} = W_{ijk1} O_{ij} \tag{19}$$

where I_{k1} is input of neuron 1 from layer *k*, O_{ij} is output of neuron *j* from layer; W_{ijk1} is called the weight relating neuron *j* and neuron 1 and this corresponds to neuron strength

$$q^{n+1}(r, t) = q^n(r, t) - \beta P^n(r, t) = 2.35 \times 1.45 = 0.628$$

from (16)

$$\gamma^n = \frac{[\psi(q^n), \psi(q^n) - \psi(q^{n-1})]}{\|\psi(q^{n-1})\|^2} = \frac{1.2 - 0.73}{1.43^2} = 0.243$$

$$F_0 = \frac{k}{\rho C_p} \frac{\Delta t}{H_{tp}} > 0.05 = \alpha \Delta t / H_{tp} = \frac{396}{8900 \times 389} \cdot \frac{1.5}{0.0021} = 0.885 > 0.05$$

from (14)

$$P^n(r, z, t) = \psi^n + \gamma^n P^{n-1}(r, z, t) = 1.2 + 1.5 \times (0.43) = 1.83$$

from (4a) we have

$$Q_d = \frac{L_{ref}^2 q'''}{\alpha_f \rho_f C_{pf} (T_h - T_c)}$$

$$= \frac{0.85^2 \times 154}{0.00011 \times 8900 \times 389 (260 - 118)} = 0.0028 \text{kJ/kg} \cdot \text{s}$$

A Neural Network Model Formulation

The CGM solution is validated by comparing the temperatures at measuring points recorded by data acquisition unit with those of one step direct problem resolution with the convergent solution regarded as the known boundary conditions. The heat flux profiles were compared with simulated and experimental Values. For the ANN simulation computation was done using Conjugate Gradient Method (CGM).

Different iteration levels were considered from 10^3 to 2.5×10^5 . The best compromise was obtained for 1500 cycles since over-fitting is avoided. The best compromise was at 8×20 Different ANN configurations with the ANN convergence property was validated as the ratio of classification was equal to 100% at end of iterative process. Different ANN configurations were examined introducing neuron penalty “permitting to add or remove neurons depending on the training or the test error evolutions. The optimization procedure permitted us to obtain a two layer structure as in **Figure**. The first hidden layer contained 13 neurons and the second one contained 8 neu-

rons. Such structures are known to be sufficient to encode nonlinear correlations. At the end of iterative process the average and maximum training errors were 7×10^{-3} and 2.5×10^{-2} respectively. **Figure** shows the instantaneous heat flux profiles determined by the CGM and the ANN for the gun workpiece distance 30mm. Along the radial direction the flux strength decreases rapidly. In the proximity of z axis the flux distribution appears singular because of unavailability of temperature information between $r = 0$ and $r = 20$ mm. The same phenomena can also be found between $r = 20$ and 40 mm for gun workpiece distance of 60 mm. There is an inflexion point away from which axis; this means that the flux becomes more and more concentrated *i.e* decrease of effective preheating. Moreover the maximal flux heat for 30 mm reaches 1.1 MW/m^2 which is four times larger than 90 mm.

The maximum of heat flux calculated corresponds to the heat flux experienced by the workpiece at the Z position corresponding to the geometric axis of the flame gun. Thus this value is expected to be the largest one at the surface of the workpiece at the Z position corresponding to geometric axis of the flame gun.

A Two layer BAM (Binary Associative memory) Hopfield network for the flame gun temperature & flux estimation.

It can also be observed that the heat flux profiles estimated by the ANN are very similar to those of the CGM.

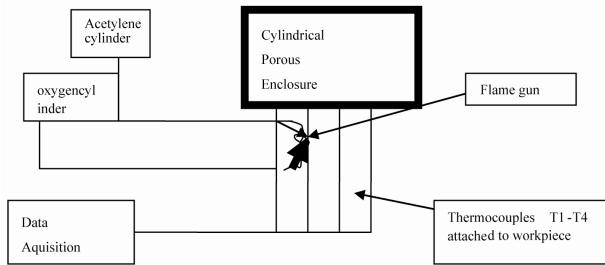


Figure 1. Metal foam sample experiments experimental setup of gas welding.

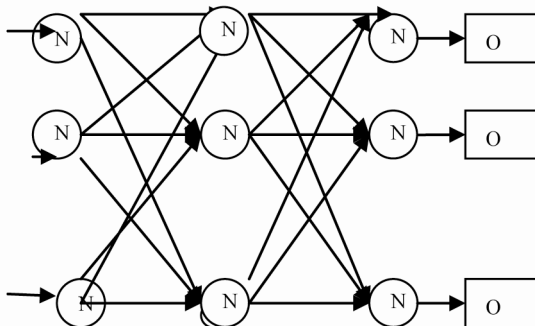


Figure 2. Map of two layer BAM neural network for the problem model.

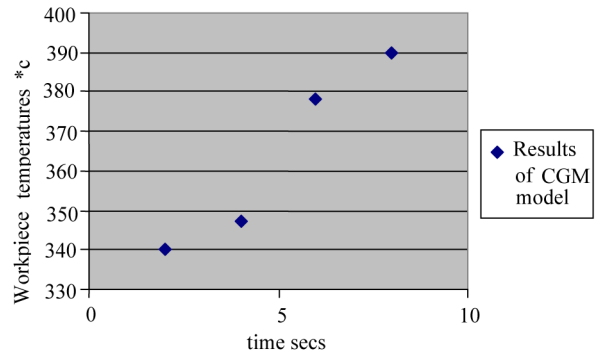


Figure 3. Predicted temperature profiles.

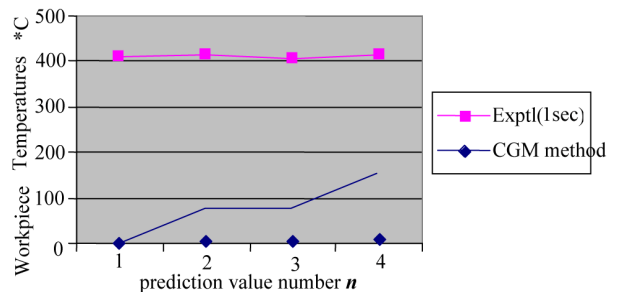


Figure 4. Temperature prediction at different points.

The peak values at the Z axis for workpiece distances 30, 60 and 90 mm are about 1.1.0.8 and 0.3 Mw/sqm for the two solutions.

To compare the q-r profiles calculated by CGM and ANN methodologies an average error o the preheating time was considered. Table 3 shows the errors obtained for different gun workpiece distances. It appears that the average error depends on mesh density is not high enough to allow the ANN structure to finally describe the exponential decay of the heat flux mechanism

ANN has the ability to predict property evolution for intermediate and limiting parameter values. Two examples for such properties are presented through the consideration of optimized ANN structure where the q-r curves were built for the gun workpiece distances of 45 mm and 75 m. These two distances belong to the parameter space defined for the ANN structure. As at the ANN input, thermocouple temperatures are needed to build the q-r curve;these were calculated using the following linear relationship

$$\begin{cases} Y_{mst}^{45} = \frac{Y_{mst}^{30} + Y_{mst}^{60}}{2} \\ Y_{mst}^{75} = \frac{Y_{mst}^{60} + Y_{mst}^{90}}{2} \end{cases} \quad ms = 1..5; \quad t=1..7$$

where the subscripts ms and t are relative to the th-

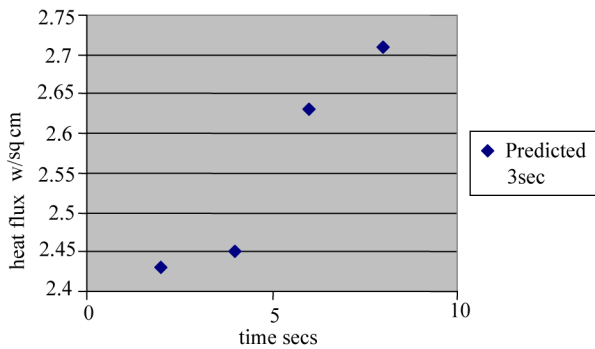


Figure 5. Heat flux profiles workpiece dist 60 mm.

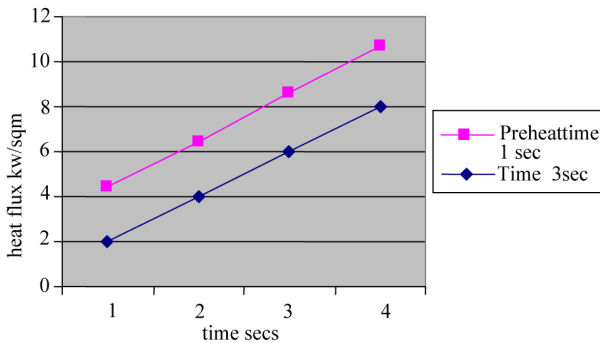


Figure 6. Heat flux profile (workpiece distance 90 mm)

Table 4. Artificial Neural Network (ANN)variable description.

Category	Parameter	Lower limit	Upper limit	Neuron number
Input pattern	D gun workpiece distance	30	100	1
	t -preheating time s	0	10	1
	Y ₁ Firstthermocouple temperature	10	60	5
	Y ₂ secondthermocouple temperature	10	65	
	Y ₃ thirdthermocouple temperature	10	60	
	Output pattern	radial position mm	0	50
q -heat flux Mw/sqm		0	1.2	1

ermocouple position and the preheating time, and the superscript is relative to gun workpiece distance.

Interpolation of thermocouple temperatures are introduced in order to predict realistic behavior related to intermediate workpiece distances. Indeed as the ANN structure learns from the database, any set of thermocouple temperatures can be introduced as input parameter. The calculated heat-flux profiles represent actual intermediate evolutions when comparing maximum strengths (r = 0). Whatever the gun workpiece distance the heat flux was found to increase with the preheating

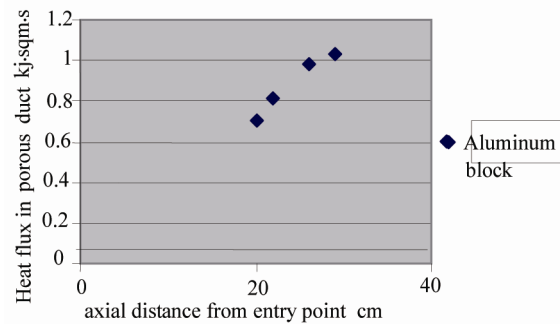


Figure 7. Experimental values of heat flux profile using model equations.

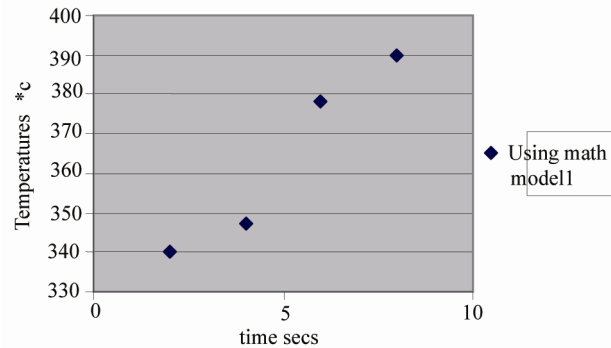


Figure 8. Predicted temperature profiles.

time for a given radial position and to decrease with increase of radial distance for a given preheating Time. The inflection point for the intermediate gun-work-piece distance 45 mm is located at 30 mm which is the intermediate value between the cases of gun-work-piece distances of 30 mm and 60 mm.

4. Results and Discussion

Figure 2 shows the map of Two layer BAM neural network for the problem model which was used for our computation. **Figure 3** shows the plot of predicted temperature profiles at 3.5 kJ/cm². Next **Figure 4** depicts the temperature prediction at different points at an input value of the heat flux being 6 kJ/cm². The temperatures gradually decreased from the heated end of the workpiece. **Figure 5** shows the heat flux profile (at a workpiece distance 60 mm), The heat flux is initially steady and decreases over the middle of the workpiece. This is attributed to the accelerated heat dissipation on the surface of the porous metal workpiece. Finally **Figure 6** shows the heat flux profile. Here the workpiece distance was kept at 90 mm from the laser gun used for heating it. **Figure 7** gives the depiction of Experimental values of heat flux profile using model equations. These data correlated with the results of the neural network model whose results are given in **Figures 3-6** and **Tables 4-6**. **Figure 8** shows the predicted temperature profiles in the workpiece computed using the CGM method. **Table 1** gives the Properties of workpiece (Cu). **Table 2** gives the ANN model parameters of the result output simulated using the ANN parameters the simulation was done using MATLAB 6.0[®] Neural Network Toolbox. **Table 6** Computation of flux parameters using CGM. **Table 5** depicts ANN output results of parameters. **Table 4** Artificial Neural Network (ANN) variable description. **Table 1a** gives the description of parameters of an Artificial Neural Network (ANN) variable.

When Heat transport by Free convection occurs in a porous medium with a closed cavity the viscous dissipation is neglected. Aluminum foam samples of different pore sizes (5-60PPI) and porosities (0.8-0.99) were used to illustrate the effects of metal foam geometry on heat transfer (3).

5. Conclusions and Suggestions

This paper contains a novel model using feedback neural

networks for a workpiece temperature prediction. The ANN model parameters of the result output were simulated using the ANN parameters. The simulation was done using MATLAB 6.0[®] Neural Network Toolbox. The article aimed at presenting a calculation principle based on statistical (ANN) and deterministic (CGM) models to evaluate the heat flux distribution generated by the flame gun in cylindrical workpiece. These models were complementary to each other, as the first one integrated the process variables that are not handled in the physical problem and the second one described by $q-r$ profiles required to predict the system response. The heat flux profiles exhibit a universal exponential decay characterized by increasing stability at a given radial position when increasing the preheating time. The ANN optimization revealed a two hidden layer structure which learned adequately the correlations (generalization property) encoded by the physical problem: the increase of heat flux with decrease of radial distance and with increase of preheating time. In addition, the ANN structure computed the heat flux decrease with increase of gun-workpiece distance.

6. References

- [1] P. Fauchius, A. Vandelle and B. Dussoubs, "Quo Vadis Thermal Spraying?" *Journal of Thermal Spray Technology*, Vol. 10, No. 1, 2001, pp. 44-66. [doi:10.1361/105996301770349510](https://doi.org/10.1361/105996301770349510)
- [2] Sampath and X. Jiang, "Substrate Temperature Spray Coatings," *Materials Science and Engineering*, Vol. 45, No. 124, 2002.
- [3] I. Pop, "Modeling of Heat Flow in a Porous Cavity," *International Journal of Heat and Mass Transfer*, Vol. 23, No. 187, 2003.
- [4] F. C. Lai, "Non Darcy Convection from a Line Source," *International Communications in Heat and Mass Transfer*, Vol. 12, No. 17, 1994, pp. 875-880.
- [5] D. A. S. Ras and I. Pop, "Modeling of Natural Convection in Shallow Porous Concrete Slab to Control Heat-flow," *International Communications in Heat and Mass Transfer*, Vol. 26, No. 6, 1999, pp. 761-770.
- [6] D. A. S. Ras, "Free Convection Stagnation Point Flow in a Porous Media in a Thermal Nonequilibrium Region," *International Communications in Heat and Mass Transfer*, Vol. 12, 1990, pp. 162-171.
- [7] A. Postelneicu and I. Pop, "Convection in Porous Media with Generation," *International Journal of Numerical Methods for Heat Transfer*, Vol. 26, No. 8, 2002.