

Thermodynamic Study for Arsenic Removal from Freshwater by Using **Electrocoagulation Process**

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Abstract

Insert Industrial treatment of mineral-processing and non-ferrous metal-smelting acid wastewater effluents is becoming an enormous worldwide problem. In Mexico, heavy metalscontaminated natural waters, including freshwater, surface water and ground water, are a significant problem as some of these compounds are known as toxic, mutagenic, and carcinogenic. A very promising electrochemical treatment technique that does not require chemical additions to remove arsenic is electrocoagulation (EC) with air injection. The proposed electrochemical process is efficient because used low cost iron electrodes and promising in industrial application. Theoretical the purpose of this research was to investigate the thermodynamic of arsenic adsorption on iron species using the Langmuir's Isotherm. Also, thermodynamic parameters such as ΔH° , ΔS° and ΔG° were calculated and the adsorption process was found to be exothermic and spontaneous. X-ray Diffraction and Scanning Electron Microscopy, were used to characterize the solid products formed during EC. The results of this study suggest that magnetite particles and amorphous iron oxyhydroxides are present in the examined EC products and this study indicate that arsenic can be successfully adsorbed on iron species by electrocoagulation process. Field pilot-scale study demonstrated the removal of As(III)/As(V) with an efficiency of more than 99% from both wastewater and wells.

Keywords

Coprecipitation, Electrocoagulation, Magnetite Particles

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1. Introduction

Arsenic contaminated natural waters, including surface water and ground water, are a significant problem as some of these compounds are known to be toxic, mutagenic, and carcinogenic. The deleterious health effects associated with ingestion of arsenic require that its concentrations should be kept below 10.0 ppb in potable water supplies. The metals existing in wastewater are usually removed by precipitation. Arsenic is conventionally removed by chemical techniques such as treatment with lime, aluminum coagulation, iron coagulation, activated carbon and reverse osmosis [1]. These conventional processes generate a considerable quantity of secondary pollutants such as solid sludge, which also pose serious environmental problems. These drawbacks have forced various industries to search for effective alternative treatment technologies for arsenic removal, mainly electrochemical methods. The purpose of this research was to investigate the arsenic adsorption on iron species. A very promising electrochemical treatment technique that does not require addition of chemicals is electrocoagulation (EC) with air injection [2]. The EC process operates on the principle that the cations produced electrolytically from iron and/or aluminum anodes enhance the coagulation of contaminants from an aqueous medium. The sacrificial metal anodes are used to continuously produce polyvalent metal cations in the vicinity of the anode. These cations facilitate coagulation by neutralizing the negatively charged particles that are carried toward the anodes by electrophoretic motion. In the flowing EC techniques, the production of polyvalent cations from the oxidation of the sacrificial anodes (Fe and/or Al) and the production of electrolysis gases (H_2 and O_2) are directly proportional to the amount of current applied (Faraday's law) [1]. The electrolysis gases enhance the flocculation of the coagulant materials.

EC is a complicated process involving many chemical and physical phenomena. It can be said that in an EC process the coagulant is produced "*in situ*" and this involves three successive stages:

- 1) Formation of coagulants by electrolytic oxidation of the "sacrificial electrode". Fe is dissolved from the anode generating corresponding metal ions, which almost immediately hydrolyze to ferric hydroxide and polymeric Iron; the generated $Fe_{(aq)}^{3+}$ ions will immediately undergo further spontaneous reactions to produce corresponding hydroxides and/or polyhydroxides. Ferric ions generated by electrochemical oxidation of iron electrode may form monomeric ions, $Fe(OH)_3$ and polymeric hydroxy complexes, namely: $Fe(H_2O)_6^{3+}$, $Fe(H_2O)_5(OH)_2^{+}$, $Fe(H_2O)_4(OH)^{2+}$, $Fe_2(H_2O)_8(OH)_2^{4+}$ and $Fe_2(H_2O)_6(OH)_4^{4+}$ depending on the pH of the aqueous medium. These hydroxides/polyhydroxides/polyhydroxymetallic compounds have strong affinity for dispersed particles as well as counter ions to cause coagulation. The gas evolved at the cathode may impinge on and cause flotation of the coagulated materials.
- 2) Destabilization of the contaminants, particulate suspension, and breaking of emulsions. Contaminants present in the wastewater stream are treated either by chemical reactions and precipitation or physical and chemical attachment to coagulant materials.
- 3) Aggregation of the destabilized phases to form flocs. Polymeric hydroxides are excellent coagulating agent

EC has been employed for removing heavy metals such as Pb, Cd, Cr and As, metals such as Mn, Cu, Zn, Ni, Al, Fe, Co, Sn, Mg, Se, Mo, Ca, Pt among others, anions such as CN, PO₄, SO₄, NO₃, F and Cl, non metals such as P, organic compounds such as TPH, TBX, MTBE, COD, BOD, suspended solids, clay minerals, organic dyes, oil and greases from a variety of industrial effluents. Some of the factors that influence EC performance are: type of electrolytes, electrodes material, applied power, acidity and final pH. A schematic representation of the EC process is shown in Figure 1.

The chemical reactions that have been proposed to describe EC mechanisms for the production of $H_{2(g)}$,

 $OH^-_{(aq)}$ and $H^+_{(aq)}$ [3] [4] at different pH values are:

For pH < 4 Anode:

$$Fe \rightarrow Fe^{+2} + 2e$$
 (1)

$$Fe \rightarrow Fe^{+3} + 3e$$
 (2)

Cathode:

$$2\mathrm{H}^{+} + 2 \mathrm{e}^{-} \to \mathrm{H}_{2(\mathrm{g})} \uparrow \tag{3}$$



Figure 1. Conceptual illustration of the EC mechanism.

For 4 < pH < 7: Anode: reactions (1) and (2) Comments: In fact iron also undergoes hydrolysis

$$Fe + 6H_2O \rightarrow Fe(H_2O)_4(OH)_2 \tag{4}$$

$$Fe + 6H_2O \rightarrow Fe(H_2O)_3(OH)_{3(20)} + 3H^{+1} + 3e^{-1}$$
 (5)

Fe(III) hydroxide begins to precipitate floc with yellowish color.

$$\operatorname{Fe}(\operatorname{H}_{2}\operatorname{O})_{3}(\operatorname{OH})_{3(\operatorname{aq})} \to \operatorname{Fe}(\operatorname{H}_{2}\operatorname{O})_{3}(\operatorname{OH})_{3(\operatorname{s})}$$
(6)

"Rust" may also be formed [4].

$$2\operatorname{Fe}(\operatorname{H}_{2}\operatorname{O})_{3}(\operatorname{OH})_{3} \leftrightarrow \operatorname{Fe}_{2}\operatorname{O}_{3}(\operatorname{H}_{2}\operatorname{O})_{6}$$

$$\tag{7}$$

Cathode: More hydrogen evolution takes place (Equation (3)); but $[H^+]$ now comes from weak acids and iron hydrolysis.

For 6 < pH < 9:

Anode: reactions (1) and (2)

Comments:

Precipitation of Fe(III) hydroxide (7) continues, and Fe(II) hydroxide precipitation also occurs presenting a dark green floc.

$$\operatorname{Fe}(\operatorname{H}_{2}\operatorname{O})_{4}(\operatorname{OH})_{2(\operatorname{aq})} \to \operatorname{Fe}(\operatorname{H}_{2}\operatorname{O})_{4}(\operatorname{OH})_{2(\operatorname{s})}$$

$$\tag{8}$$

The pH for minimum solubility of $Fe(OH)_n$ is in the range of 7 - 8. EC floc is formed due to the polymerization of iron oxyhydroxides [5].

Formation of rust (dehydrated hydroxides) occurs as shown in the following:

 $2\text{Fe}(\text{OH})_3 \leftrightarrow \text{Fe}_2\text{O}_3 + 3\text{H}_2\text{O} \text{ (hematite, maghemite)}$ (9)

$$Fe(OH)_2 \leftrightarrow FeO + H_2O$$
 (10)

$$2Fe(OH)_{3} + Fe(OH)_{2} \leftrightarrow Fe_{3}O_{4} + 4H_{2}O \text{ (magnetite)}$$
(11)

$$Fe(OH)_3 \leftrightarrow FeO(OH) + H_2O$$
 (goethite, lepidocrocite) (12)

Hematite, maghemite, rust, magnetite, lepidocrocite and goethite have been identified as EC by-products [6]. **Cathode:** More hydrogen evolution takes place (Equation (3)); but $\begin{bmatrix} H^+ \end{bmatrix}$ now comes from weak acids and iron hydrolysis.

Overall reactions are:

$$\operatorname{Fe} + 6\operatorname{H}_{2}\operatorname{O} \to \operatorname{Fe}(\operatorname{H}_{2}\operatorname{O})_{4}(\operatorname{OH})_{2(s)} + \operatorname{H}_{2(g)} \uparrow$$
(13)

$$\operatorname{Fe} + 6\operatorname{H}_{2}\operatorname{O} \to \operatorname{Fe}(\operatorname{H}_{2}\operatorname{O})_{3}(\operatorname{OH})_{3(s)} + \frac{3}{2}\operatorname{H}_{2(g)} \uparrow$$
(14)

Conditions throughout the cell are not constant; concentrations, species and pH are changing. This may be illustrated with an iron Pourbaix diagram.

2. Materials and Methods

The adsorption experiments were performed in a 400 ml glass beaker equipped with two carbon steel electrodes (6 cm \times 3 cm) located 5 mm apart. There was used a source of current and voltage (universal AC/DC adaptor). The pH was measured with an electrode/pH meter-VWR scientific 8005. Arsenic adsorption onto iron species was investigated with electrolytes prepared with sodium arsenate Na₂HAsO₄, (analytical reagent with a purity of 97% supplied by Chemical Products, Monterrey) and deionized water with conductivity of 0.95 μ S cm⁻¹ (Aldrich Chemical Co. 99.5%). The solutions and solids were then separated by filtration through cellulose filter paper. The sludge from the EC was dried either in an oven or under vacuum at room temperature. The experimental set-up is presented in **Figure 2**. The current and voltage during the EC process were measured and recorded, using Cen-Tech multimeters. The pH values of the solution before and after EC were measured with a VWR scientific 8005 pH meter.

In **Table 1**, the initial conditions of arsenic for the range of concentrations listed are presented. The Langmuir isotherm model was used to analyze adsorption data.

The amount of arsenic adsorbed onto iron species at equilibrium N (mg/g) was calculated by using the following relationship [7]:



Figure 2. Experimental set-up for arsenic removal two-electrode electrocoagulation cell.

Lanc 1. Conditions for assente ausorphon experiments.										
Samples	Concentration (mg/L)	Temperature (°C)	pН	Current (A)	Cell Potential (V)	Time (min)				
1	1	20	2.86	0.49	8.5	5				
2	2	20	3.02	0.52	12	5				
3	5	20	2.90	0.44	10	5				
4	7	20	3.05	0.41	12.8	5				
5	13	20	2.90	0.48	10.7	5				
6	20	20	3.02	0.50	10.25	5				
7	30	20	4.14	0.75	6.68	5				

 Table 1. Conditions for arsenic adsorption experiments.

$$N = V \left[C_0 - C_e \right] / W \tag{15}$$

which, C_0 and C_e (mg/L) are the liquid phase concentrations of arsenic initially and at equilibrium, respectively, *V* the volume of the solution (L) and *W* is the mass of adsorbent used (g) (in this case the Fe dissolved from EC). The mass of metal dissolved (or other species discharged) depends on the quantity of charge (electrons) supplied to the electrocoagulation cell during the holding time that happens across the electrolytic solution and the time of residence of the water in the electrocoagulation cell. A simple relation between the current density and the quantity of substance dissolved (g of *M* per cm²) stems from Faraday's law [7]:

$$W = \frac{D \cdot t \cdot M}{n \cdot F} \tag{16}$$

where W is the mass of the electrode dissolved (g/cm⁻²), D is the density of current (A per cm⁻²), t is the time (seconds), M is the relative molar mass of the electrode, n the electrons number in the electrode reaction, and F is Faraday's constant (96,500 coulombs). Then, arsenic moles numbers adsorbed onto iron species are calculate by Equation (15).

In Table 2 arsenic moles number adsorbed onto iron species are presented. High adsorption was showed while the concentration increases.

Then, the Langmuir isotherm was employed to describe the adsorption equilibrium in the system:

$$N = \left(\frac{N_{\text{Max}}K_L C_e}{1 + K_L C_e}\right)$$
(17)

where N is the amount of arsenic adsorbed onto iron species in equilibrium (mg/g), N_{max} is the maximum adsorption capacity corresponding to complete monolayer coverage on the surface (mg/g), C_e is the equilibrium concentrations of metals ions in the solution at equilibrium (mg/L) and K_L is the Langmuir constant (L/mg). Equation (7) can be rearranged to a linear form as follows [8]:

$$\frac{C}{N} = \frac{1}{N_{\text{Max}}K_L} + \frac{C_e}{N_{\text{Max}}}$$
(18)

3. Results and Discussion

Following the model of the Langmuir's isotherm (see **Figure 2**) shows the arsenic adsorption capacity on iron species. The constants can be evaluated from the intercepts and the slopes of the linear plots of C_e/N versus C_e . Table 2, shows the results of the linear regression. The value of N_{max} indicates the maximum adsorption capacity corresponding to complete monolayer coverage on the iron surface. The value of K_L is the constant of adsorption of Langmuir.

The thermodynamic parameters [such as change in standard free energy (ΔG°) , enthalpy (ΔH°) and entropy (ΔS°) were determined [5] by using the following equations:

$$\ln b = -\frac{\Delta G^{\circ}}{RT} \tag{19}$$

$$\ln(b) = b_0 - \left(\frac{\Delta H^\circ}{RT}\right) \tag{20}$$

Table 2. Arsenic moles adsorbed on iron species (N).										
Sample	C _{0As} (mmol/L)	C _{eAs} (mmol/L)	W (g)	N (mmol/g)						
1	0.013347	0.0002	0.028435	0.161827						
2	0.026695	0.0006	0.033658	0.270655						
3	0.066737	0.0009	0.025534	0.901994						
4	0.093432	0.0020	0.023793	1.344981						
5	0.173518	0.0049	0.027855	2.118223						
6	0.266951	0.0126	0.029016	3.067147						
7	0.400427	0.0168	0.043523	3.084857						

$$\Delta G_{\rm ads}^{\circ} = \Delta H_{\rm ads}^{\circ} - T \Delta S_{\rm ads}^{\circ} \tag{21}$$

In which *R* is the gas constant, *T* (°K) the absolute temperature, *b* is the Langmuir's constant which is related to the energy of adsorption, and b_0 is a constant. **Table 3**; show the negative value of ΔG° obtained, indicated that the arsenic adsorption on iron species by EC is a spontaneous process. The negative value of ΔH° represents an exothermic process and suggests a fisiad sorption behavior according with the liberated heat between -20 and -40 KJ/mol. The negative value of ΔS° suggests that a significant change does not happen in the internal structure of the adsorbent during the adsorption of As.

Product Characterization

In this study, chemical analysis, powder X-ray diffraction (XRD), and scanning electron microscopy (SEM) were used to characterize the solid products generated in the EC cell, operated with carbon-steel electrodes. **Figure 3** shows the diffractogram for an arsenic sample obtained from a solution at pH 7, containing 2 ppm arsenic. The species identified were magnetite, goethite, lepidocrocite, iron arsenate and iron hydroxide oxide in crystalline form.

Figure 4, shows, respectively, the SEM and EDAX images of As contaminated iron oxide/oxyhydroxide particles. These displays show that the surfaces of these iron oxide/oxyhydroxide particles were coated with a layer of As species.

Also, the results of this study suggest that EC produces magnetic particles of magnetite and amorphous iron oxyhydroxide species that serve to remove As(III)/As(V) species. In order to prove this, FTIR spectra for solids collected from EC trials with various starting pH value of ca. 7.0. The positions of the important absorption bands for the various iron containing phases are summarized in Table 1 [9]-[15]. This table is modeled after the work by Nauer *et al.* [9] that tabulated the peak positions of goethite (δ -FeOOH), akaganéite (δ -FeOOH), lepidocrocite (δ -FeOOH), feroxyhite (δ -FeOOH), and bernalite (Fe(OH)₃). These authors also used the following assignments for IR absorbances:

- 1) 3600 to ca. 3000 cm⁻¹: OH stretching vibration, v(OH).
- 2) 1200 to 600 cm⁻¹: Fe-O-H bending vibrations and Fe-O stretching vibrations.
- 3) 600 to 200 cm⁻¹: absorptions caused by the overlapping of lattice vibrations with molecular frequencies (Fe-O stretching vibrations can also absorb down to ca. 350 cm⁻¹).

After examining the spectra in that work, the current authors added the indications of shoulders on the v(OH) stretching vibrations for δ -FeOOH, δ -FeOOH, and δ -FeOOH. For δ -FeOOH, trimodality of the v(OH) stretching vibrations has also been indicated by adding the peaks at both 3450 and 2900 cm⁻¹. Another extensive study by Weckler and Lutz [12] found spectra for δ -FeOOH, δ -FeOOH, δ -FeOOH, and δ -FeOOH that closely resemble those summarized in **Table 4**. However, two additional features were added for goethite. The earlier work of Misawa *et al.* [13] also confirm the results discussed above for δ -FeOOH and also assigned a peak at 470 cm⁻¹ and shoulders at 668 and 442 cm⁻¹ to magnetite (Fe₃O₄). However, Musić [14] and Nasrazadani [10] observed peaks at ca. 575 and 385 cm⁻¹ for magnetite and Nyquist and Kagel [15] observed peaks at 725 and 575 cm⁻¹ for magnetite. The study by Musić [15] was also used as a reference for additional peaks for Fe(OH)₃, while Nasrazadani also assigned peaks at 630 and 430 cm⁻¹ to magnetite (δ -Fe₂O₃).



Figure 3. XRD diffractogram for the iron impregnated with arsenic.

Table 3. Linear regression results for arsenic adsorption onto iron species.								
Parameter	Results							
\mathbb{R}^2	0.9665							
N _{max} (mmol _{As} /gFe)	4.242281							
K _L (L/mmol)	181.30							

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		Goethite	F	Akaganeite	Lej	pidocrocite	ŀ	eroxyhite		Bernalite	Н	lematite	Maghemite	Magnetite
		α -FeOOH		β -FeOOH		γ-FeOOH		δ -FeOOH		Fe(OH) ₃		α -Fe ₂ O ₃	γ -Fe ₂ O ₃	Fe ₃ O ₄
1)	\mathbf{sh}	3500^{*}	ss	3480			s	3450^{*}						
	s	3155	\mathbf{sh}	3000^*	s	3100	s	3150	m	3500 - 2500				
		1385 ^d			sh	2800^{*}	s	2900^{*}		1507 ^c				
2)	w w	1125 ^a 1081 ^a			m s	1155 1160 ^f	m	1130	vw	1044 ^c	w	1010^{f}		
	w	1020^{f}			m s	$\begin{array}{c} 1020 \\ 1020^{\mathrm{f}} \end{array}$	m	915						
	s	890	sh	875							w	885^{f}		
	s	790	w	800	s	740	s	795						
			s	700								725 ^e	785 ^d	725 ^e

460

335

270 Peak notes: very strong (ss), strong (s), medium (m), weak (w), very weak (vw), shoulder (sh), broad (b).

480

360

ss

SS

ss

ss

SS

4. Conclusion

640

455

400

270

s

ss

s

3) sh

620

425

w

ss

The results of this study indicate that arsenic is readily adsorbed onto iron species generated by electrocoagulation. It was found that 99% of the arsenic in a batch cell is removed in the lab-scale EC reactor within 60 seconds or less for most experiments, and with a current efficiency of 100%. Correlation of the adsorption behavior with the Langmuir isotherm revealed an adsorption capacity of 4.24 mmol As/g of Fe absorbent. The negative values of ΔG° obtained indicate that the arsenic adsorption onto iron species generated by EC is a spontaneous process. The negative values of ΔH° represent an exothermic process.

590^e

535°

568°

566

448

630^d

550

668^b sh

570^{c,d}

470^b 442^b

385^{c,d}

sh



Figure 4. SEM and EDAX images for by-products generated from the arsenic contaminated water samples.

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