

Comparative Studies on Synthesis and Characterization of Titania and Iron Oxide Doped Magnesia from Indian Salem Magnesite

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Abstract

Sintering, densification, and characterization of Salem Magnesite with Titania (TiO₂) and Iron Oxide (Fe₂O₃) addition have been carried out in this work. Salem Magnesite samples with 2 wt.% TiO₂ and Fe₂O₃ addition have been sintered in the temperature range of 1550°C - 1650°C. The sintered sample has been characterized in terms of physico-chemical properties like bulk density, apparent porosity, specific gravity and structural properties by X-ray diffraction and scanning electron microscope (SEM). Salem magnesite samples with 2 wt.% TiO₂ and Fe₂O₃ addition have been densified to the specific gravity of 3.75 and 3.41 g/cc respectively after sintering at 1650°C and 2 h. The presence of Calcium Titanate (CaTiO₃) phase at the grain boundary has been observed in the case of TiO₂ addition. For Iron Oxide addition, precipitation of "Y" shaped magnesium ferrite spinel has been observed inside the grains. Finally, TiO₂ addition in Salem Magnesite shows better densification compared to both as received Salem Magnesite and Salem Magnesite with Fe₂O₃ addition.

Keywords

Sintering, Additive, Magnesite, Densification

1. Introduction

Magnesia (MgO) based refractories have been a subject of continuing interest because of its high melting point

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(2858°C), high chemical inertness against both acidic and basic slags, low thermal expansion (CTE) values at elevated temperatures and benign ecological characteristics [1]–[3]. It is widely used in various applications such as steel ladles, cement rotary kilns, vacuum induction furnaces, continuous casting tundishes, degasser snorkels and lances and glass industries [4]. During processing of refractory materials, densification occurs via sintering process [5]. Though a very high melting point of the refractory material is essential for high-temperature applications, lower temperature processing is always preferable to reduce processing expenses. Thus, the addition of small additive plays an important role in its processing (*i.e.* sintering) as they not only lower the sintering temperature but also can enhance its mechanical strength and corrosion resistance during operation. Several authors have reported that the small additions (often less than 2 wt.%) of another material can have a very marked effect on the densification, grain growth and other characteristics of Magnesite refractory [6]–[9].

Magnesite refractories in India are manufactured mainly from naturally occurring magnesite mineral. Though India has vast reserves of natural magnesite, the Indian refractory industries are mostly reliant on imported magnesite. This is mainly due to the fact that Salem Magnesite contains impurities like Silica (SiO_2) and Calcia (CaO) which degrade refractoriness of Magnesite refractory at elevated temperatures by forming low melting Calcium Silicate phase [10]. The addition of small amount of additives which can react with these unwanted impurities and form high melting phases instead can potentially improve the refractoriness of Magnesite refractory produced from Salem Magnesite. Additives also can help in sintering.

There have been numerous studies on Magnesite with different additives. James W. Nelson *et al.* have suggested that the Iron Oxide addition can promote sintering with cation vacancies [11]. Fresh has shown that the reaction between MgO and Fe_2O_3 occurs to form MgFe_2O_4 in the temperature region 900°C to 1200°C which is a high melting spinel phase [12]. Work done by Bron has shown that Ti^{4+} ions are capable of entering the MgO lattice with the formation of a defect structure which is very similar to the mixture of Al_2O_3 and TiO_2 and help in densification [13]. According to Cosic *et al.*, MgO and TiO_2 react to form MgTiO_3 . This MgTiO_3 transforms into Mg_2TiO_4 and CaO from MgO - CaO solid solution reacts with TiO_2 forming CaTiO_3 [14]. Calcium Titanate is a high-temperature phase and formation of Calcium Titanate is preferable to low melting Calcium Silicate phase.

Even though Salem Magnesite is technologically important for refractory production, there has been a dearth of studies on Salem Magnesite with the additive addition to overcoming its inherent difficulty with impurities. The present work involves investigation of densification studies on the addition of dopants (additive) on Magnesite refractory aggregates produced from Salem Magnesite. The objectives of the present work are two folds. The first objective is to determine the influence of its physicochemical properties on dopant addition. The second objective is to correlate the mineralogical phases and as well as the microstructure of the developed phases in the presence of dopants. We have used Iron Oxide (Fe_2O_3) and Titania (TiO_2) as additives. These additives are chosen because they have an ionic radius not too different from that of Mg^{2+} but a different valence; the idea behind is that they might form solid solutions with Magnesite (MgO) and effect the sintering through the formation of defects and the subsequent change in the rate of diffusion. The amount of additives added was 2 wt.%.

2. Experimental Procedure

2.1. Material and Processing

For the present study natural Magnesite obtained from Salem district in Tamil Nadu (supplied by erstwhile Burn Standard Co. Ltd., presently SAIL Refractory Co. Ltd., India) was used as the base material. Commercially available powders of Iron Oxide (Fe_2O_3 , Glaxo Laboratories, India Ltd.) and Titania (TiO_2 , S.D. Fine Chem. Ltd., Boisar, India) of reagent grade were used for this study. Starting Magnesite lumps were first characterized for chemical analysis and phase analysis. Chemical analysis was done by the acid dissolution method. Phase identification was done by X-ray diffractometer (Philips X' pert Pro, PAN Analytical operated at 40 KV and 35 mA, The Netherlands). **Figure 1** shows the process flow chart of magnesite preparation from the Salem Magnesite. The magnesite, initially in the form of large aggregated lumps, was crushed in a jaw crusher and ground by hand rammer to the required fineness. The ground materials were sieved through BS 100 mesh sieves. Iron particles were separated from fine powders by using a U-shaped magnet. Then the fine powders were attrition milled using ethyl alcohol as a mixing media for 2 h. at 200 rpm. The batches were then dried at 50°C (overnight). The dried materials were sieved through BS 60 mesh and then mixed with a binder (5 wt.% poly-vinyl alcohol solution). Iron oxide and Titania were added separately. The bars of samples were prepared by filling approximately 7 gm. of powder mixtures in a toughened steel mold of length 7 cm and breadth 0.75 cm and then

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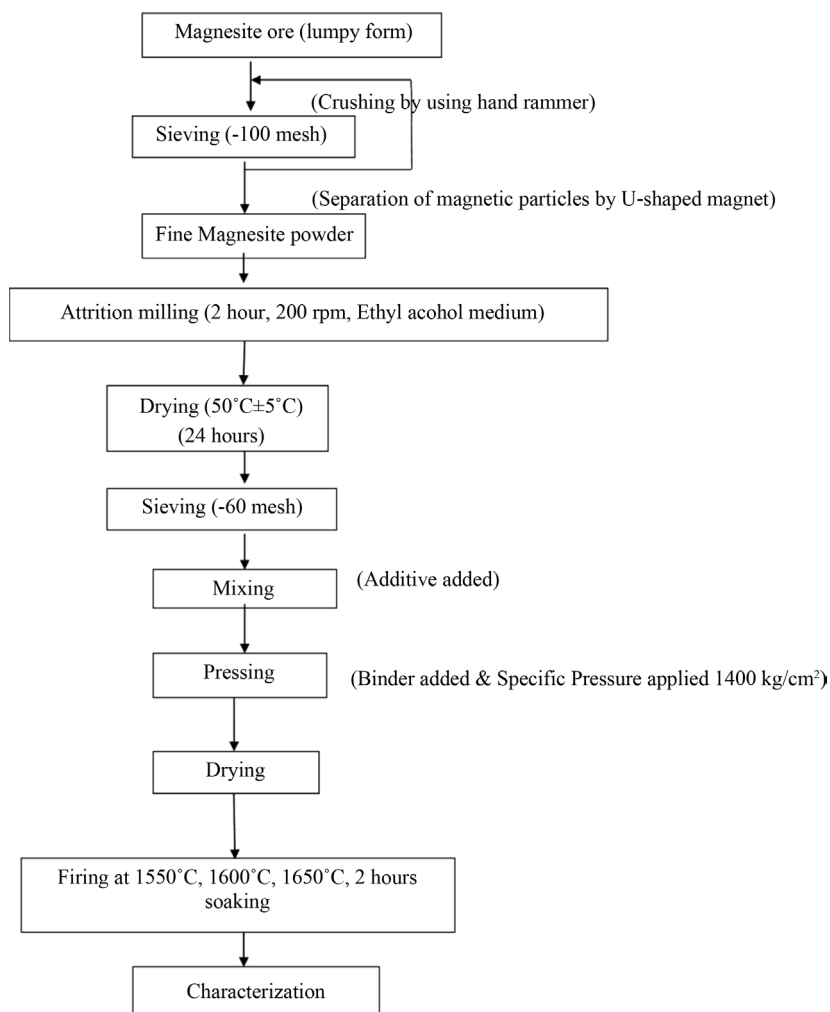


Figure 1. Process flow chart of sample preparation.

application of uniaxial pressure 1400 kg/cm². The pressure was applied in a hydraulic press (Fred S. Carver Inc., Wabash, IN, USA). The dried samples were then sintered in an electrically heated programmable furnace to 1550°C - 1650°C with 2 hours of soaking at the peak temperature. The heating rate for the furnace was maintained 5°C/min up to 1000°C, then 3°C/min up to the peak temperature. The samples were allowed to cool in the furnace before characterization in terms of their physical properties and structures.

2.2. Characterization of the Sintered Samples

Sintered samples were polished using SiC abrasive paper of different grit size and diamond paste. Post processing, characterization conducted were density measurements through Archimedes method in kerosene, X-ray diffraction (XRD) for phase identification (Philips X' pert Pro, PAN Analytical operated at 40 KV and 35 mA, The Netherlands) using CuK α radiation. Scanning electron microscopy (Zeiss, Germany) of the polished sample surface was carried out for the observation of microstructures and phase identification with energy-dispersive X-ray microanalysis (EDAX, Mahwah, NJ, USA).

3. Results

In this section, the phase analysis results are first reported, followed by the density and microstructural observations.

3.1. Chemical Analysis

Table 1 shows the chemical analysis results. Salem Magnesite contains a significant amount of impurities. Important impurities on the basis of wt.% are Silica (SiO_2) and Calcia (CaO). Minor impurities are Alumina (Al_2O_3), Iron Oxide, Titania, Potassium Oxide (K_2O) and Sodium Oxide (Na_2O).

3.2. XRD Analysis

3.2.1. With TiO_2 Addition

Normalized XRD patterns of the Salem Magnesite with TiO_2 addition after heat treatment at 1550°C , 1600°C , and 1650°C are shown in **Figures 2(a)-2(c)**. The presence of magnesium Titanate (Mg_2TiO_4), Calcium Titanate (CaTiO_3) and Magnesium Silicate (Mg_2SiO_4) phases in XRD pattern are identified. Binary phase diagram of MgO - TiO_2 shows stable phase for 3 wt% TiO_2 addition in MgO is Mg_2TiO_4 and MgO . Our XRD results corroborate that. Our starting composition also has a significant amount of SiO_2 and CaO as impurities. Our XRD results show the presence of CaTiO_3 and Mg_2SiO_4 which form during the sintering when the impurity phase reacts with Periclase (MgO) and Titania (TiO_2) phase.

Table 1. Chemical analysis of the starting materials.

Constituent	Weight (%)	Weight (%) on fired basis
SiO_2	2.44	4.8
Al_2O_3	0.17	0.34
Fe_2O_3	0.24	0.48
TiO_2	0.02	0.4
CaO	1.41	2.79
MgO	45.68	90.49
Na_2O	0.08	0.16
K_2O	0.05	0.99
L.O.I.	49.52	-

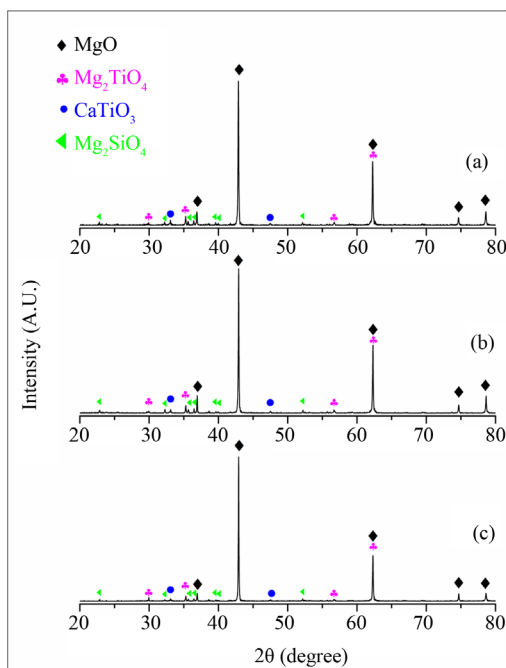


Figure 2. Phase analysis of Indian magnesite with Titania additive after sintering at (a) 1550°C , (b) 1600°C and (c) 1650°C .

3.2.2. With Fe₂O₃ Addition

XRD patterns of the Salem Magnesite with Fe₂O₃ addition after sintering at 1550°C, 1600°C and 1650°C are shown in **Figures 3(a)-3(c)**. XRD pattern after sintering has confirmed the formation of Magnesium Ferrite (MgFe₂O₄) spinel mainly by counter diffusion of cations through oxygen lattice. Phase diagram of MgO-Fe₂O₃ shows that over the temperature of 1400°C, the reaction occurs between MgO-Fe₂O₃ to form a MgFe₂O₄ spinel. Our XRD results support that. Our starting composition also has a significant amount of CaO and SiO₂. Consequently, our XRD results also show the presence of Calcium Magnesium Silicate (CaMgSiO₄) and Mg₂SiO₄ which have formed during the sintering.

3.3. Sintering and Densification

Bulk density and apparent porosity with TiO₂ addition in Magnesia are shown in **Figure 4**. Here, the significant

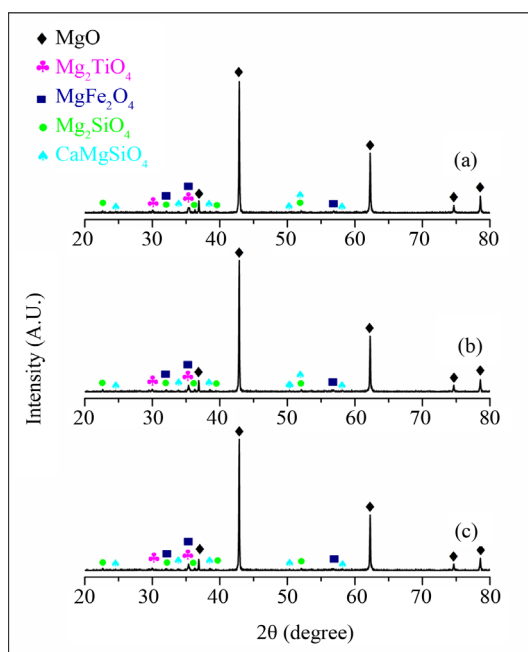


Figure 3. Phase analysis of Indian magnesite with Fe₂O₃ additive after sintering at (a) 1550°C, (b) 1600°C and (c) 1650°C.

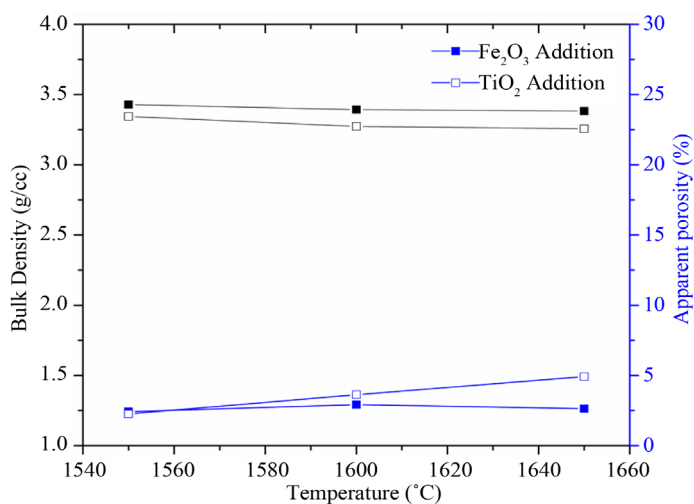


Figure 4. Variation of bulk density and apparent porosity with sintering temperature and different additives.

increase in specific gravity (Figure 5) with an increase in sintering temperature is observed whereas bulk density almost remains the same. Bulk density and apparent porosity with the addition of Fe_2O_3 additive are also shown in Figure 4. Change in specific gravity is shown in Figure 5. It shows that the maximum bulk density of 3.429 g/cc is achieved at the sintering temperature of 1550°C. With progressing increase in sintering temperature, bulk density almost remains the same for 1600°C but after sintering to 1650°C, specific gravity reduces quite a bit.

3.4. Microstructural Analysis

3.4.1. With TiO_2 Addition

Figure 6 shows the microstructure of the polished section of sintered Magnesite with Titania addition at the temperature of 1600°C. This microstructure consists of rounded grains with lighter contrast material in the inter-granular region. MgO and TiO_2 react during the sintering and to form Mg_2TiO_4 . In addition to that impurity phase Calcia, reacts with Titania to form stable CaTiO_3 . Figure 7 shows the EDS elemental map after the sintering at 1650°C. It shows that the segregated phase at the grain boundary is CaTiO_3 . The XRD results also confirm the presence of CaTiO_3 phase. Figure 7 elemental analysis shows that inside the grain boundary the main phase is MgO . The presence of Magnesium Silicate phase in the grain boundary can also be seen from the Figure 7.

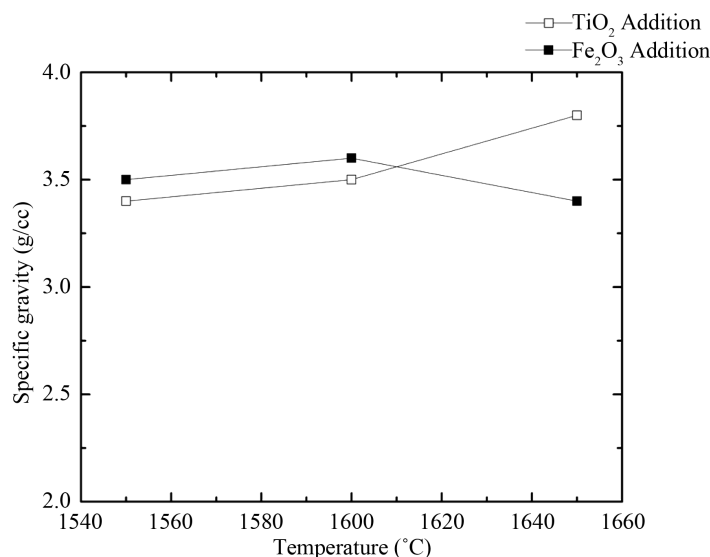


Figure 5. Variation of specific gravity with sintering temperature and different additives.

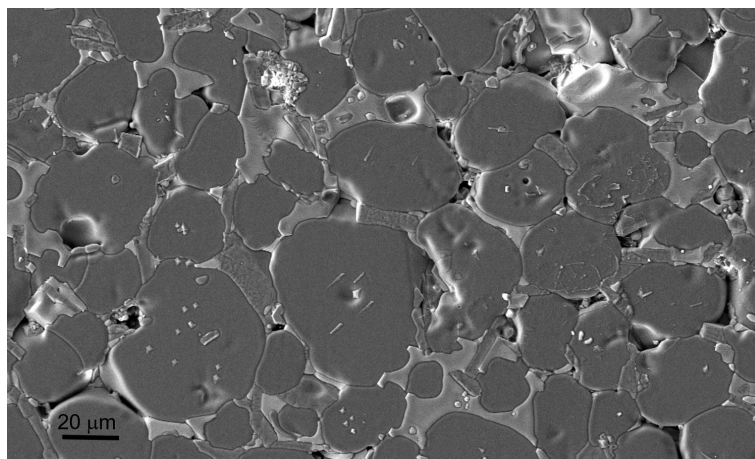


Figure 6. SEM micrograph of Indian magnesite with 2 wt.% Titania addition after sintering at 1600°C.

3.4.2. With Fe_2O_3 Addition

Figure 8 shows the SEM micrograph of Magnesite with Iron Oxide additive addition. It shows precipitation of a second phase all over the matrix. EDS elemental line scan of the Magnesite with 2 wt.% Iron Oxide addition is shown in **Figure 9**. From the line scan, it can be seen that the second phase contains Iron and is well distributed inside the grain boundary. XRD results show the only Iron containing phase in this material is Magnesium Ferrite spinel. Therefore, the second phase, which has precipitated inside the Magnesite grain, likely is the Magnesium Ferrite spinel. This Magnesium Ferrite spinel also shows “Y” shaped morphology and is also oriented in a particular direction inside a grain. The orientation of Magnesium Ferrite spinel, however, changes from one grain to other. Elemental line scan also shows that the Ca and Si have segregated at the grain boundary region. This phase likely is the CaMgSiO_4 as this is the only Ca and Si-containing phase detected by the XRD study.

4. Discussion

4.1. With TiO_2 Addition

In Magnesite with titania addition, a small increase in specific gravity with an increase in sintering temperature is observed whereas bulk density remains similar. The addition of the Ti^{+4} results in a cation vacancy in MgO lattices as shown in **Figure 10(b)**. Possibly, the vacancy in the lattice is enhancing the cation movement and mass transfer in the presence of TiO_2 and improving the densification. Titanium ion in Magnesium site of MgO lattice

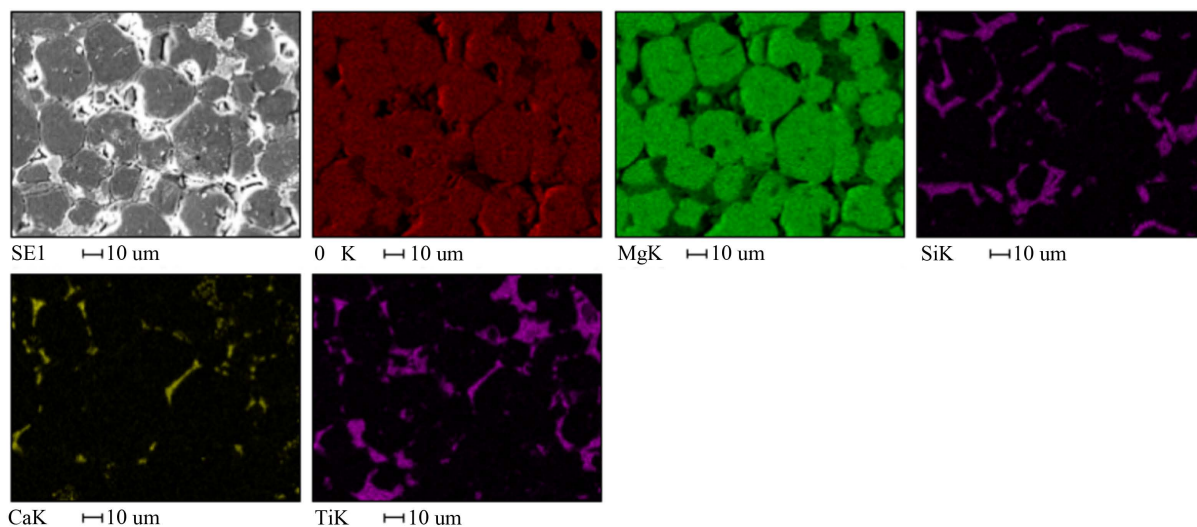


Figure 7. EDS elemental map of Indian magnesite with 2 wt.% Titania addition after sintering at 1650°C.

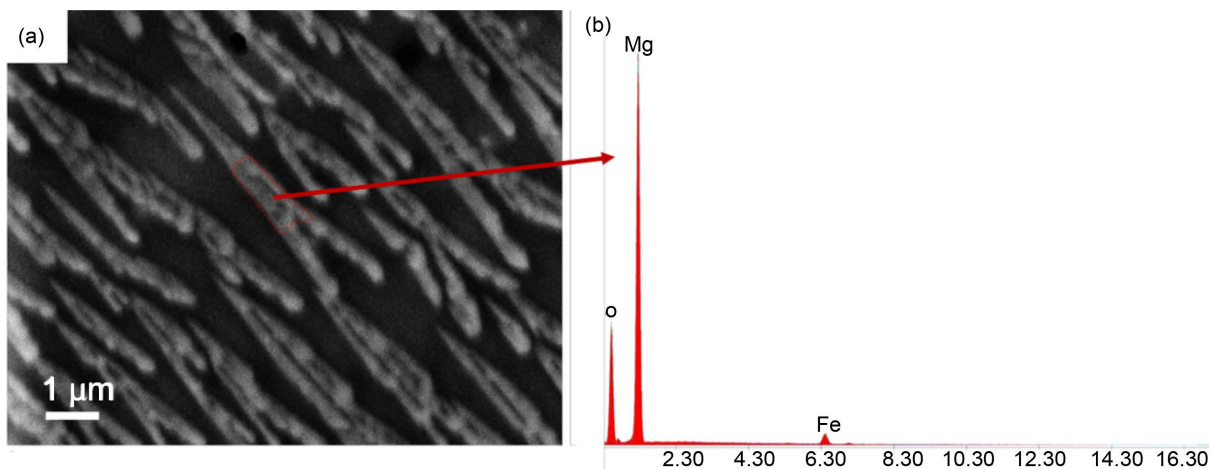


Figure 8. SEM micrograph of Indian magnesite with 2 wt.% iron oxide addition after sintering at 1600°C.

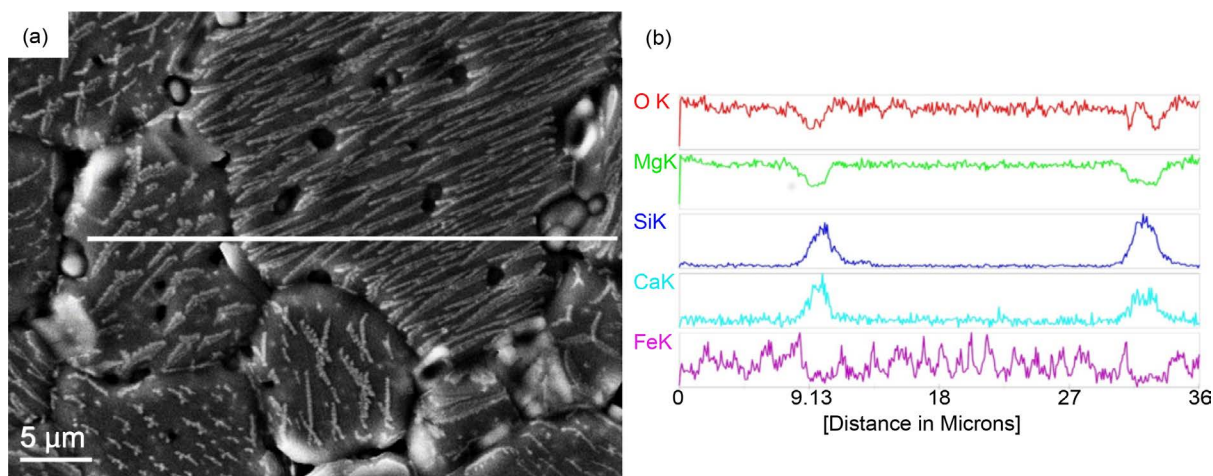


Figure 9. SEM micrograph and elemental line scan of Indian magnesite with 2 wt.% iron oxide addition after sintering at 1650°C.

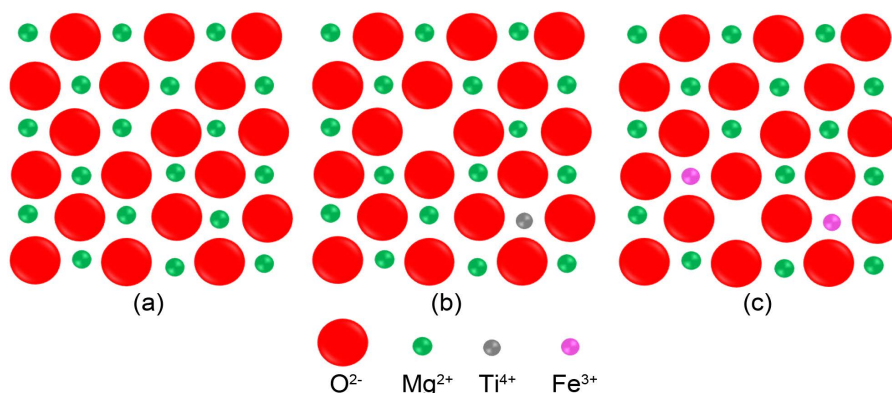


Figure 10. (a) Shows the schematic of MgO system, (b) and (c) show the lattice structure after Ti^{+4} and Fe^{+3} addition.

also causes lattice strain due to the larger size of the titanium ion (size of Titanium is 0.068 nm and that of Magnesium is 0.066 nm [15]), which also enhances the mass transport process for densification. In the case of TiO_2 addition, Ti^{4+} can substitute Mg^{2+} ions and form cation vacancies resulting in solid solution at the grain boundaries. Titanium is generally strongly attached to the oxygen interface and concentrates at the grain boundary due to its high chemical reactivity with oxygen [11]. As our SEM micrograph has shown, Ti^{4+} ion also reacts with Calcia impurity present in the raw material to form calcium titanate as secondary phase across the periclase grain boundaries.



4.2. With Fe_2O_3 Addition

Additions of Fe_2O_3 to MgO facilitate sintering with increasing sintering temperature except at 1650°C at which temperature the densification decreases slightly. The addition of the Fe^{+3} results in a cation vacancy in MgO lattices as shown in Figure 10(c). But the vacancy in the lattice is not enhancing the mass transfer and densification in the presence of Fe_2O_3 , especially at higher temperatures. Fe_2O_3 reacts with MgO to produce Magnesium Ferrite spinel which is known to hinder densification [6]. Possibly this is responsible for lesser densification at a higher temperature. XRD results show Calcia and Silica, which are impurities, reacts with Magnesia to form Calcium Magnesium Silicate which is different from Titania addition, where Calcia reacts with Titania to form Calcium Titanate at the grain boundary.

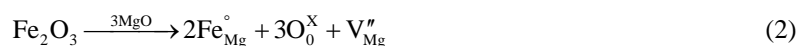


Table 2. Summary table of specific gravity with the variation of sintering temperature and different additives.

Sintering temperature (°C)	Specific gravity (g/cc)		
	Without addition of any additive [10]	Addition of Fe ₂ O ₃ additive	Addition of TiO ₂ additive
1550	3.52	3.48	3.36
1600	3.42	3.59	3.48
1650	3.55	3.41	3.75

4.3. Comparison with as Received Salem Magnesite

Table 2 shows the comparison of specific gravity between as received Salem Magnesite and Salem Magnesite with Titania and Iron Oxide addition. Both Titania and Iron Oxide addition create cation vacancy and improve densification of Salem Magnesite up to 1600°C. At 1650°C, Iron Oxide seems detrimental to the densification, as the specific gravity reduces. This reduction is possibly due to the formation of spinel structure which has been reported to hinder densification [6]. But in the case of Titania addition densification improves with temperature and finally achieves much higher specific gravity compared to the as received Salem Magnesite. This shows that addition of Titania improves sintering and densification of Salem Magnesite.

The main challenge for Salem Magnesite, to be used as a refractory material, is the impurities present namely Silica and Calcia which typically reacts to produce low melting phase (melting point ~1400°C) and degrades the refractoriness. But the addition of Titania prevents this detrimental reaction and produces Calcium Titanate instead which has a much higher melting point (>1800°C). This will certainly improve the refractoriness of Salem Magnesite.

5. Conclusion

The present investigation shows that the Salem Magnesite with Titania and Iron Oxide can be densified to the specific gravity of 3.75 and 3.41 g/cc after sintering at 1650°C and 2 h. Titania addition improves densification compared to both as received Magnesite and Iron Oxide addition. The presence of Calcium Titanate phase at the grain boundary is also observed in the case of Titania addition. In addition to Calcium Titanate phase, the presence of Magnesium Silicate phase was also observed in the grain boundary. For Iron Oxide addition, MgO grains are directly bonded. Here, precipitation of Magnesium Ferrite spinel is observed inside the grains. These spinel precipitates show “Y” shaped morphology.

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