

# An Improved Model for Single-Frequency GPS/GALILEO Precise Point Positioning

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## Abstract

This paper introduces a new precise point positioning (PPP) model, which combines single-frequency GPS/Galileo observations in between-satellite single-difference (BSSD) mode. In the absence of multipath, all receiver-related errors and biases are cancelled out when forming BSSD for a specific constellation. This leaves the satellite originating errors and atmospheric delays unmodelled. Combining GPS and Galileo observables introduces additional biases that have to be modelled, including the GPS to Galileo time offset (GGTO) and the inter-system bias. This paper models all PPP errors rigorously to improve the single-frequency GPS/Galileo PPP solution. GPSPACE PPP software of Natural Resources Canada (NRCAN) is modified to enable a GPS/Galileo PPP solution and to handle the newly introduced biases. A total of 12 data sets representing the GPS/Galileo measurements of six IGS-MEGX stations are processed to verify the newly developed PPP model. Precise satellite orbit and clock corrections from IGS-MEGX networks are used for both GPS and Galileo measurements. It is shown that sub-decimeter level accuracy is possible with single-frequency GPS/Galileo PPP. In addition, the PPP solution convergence time is improved from approximately 100 minutes for the un-differenced single-frequency GPS/Galileo solution to approximately 65 minutes for the BSSD counterpart when a single reference satellite is used. Moreover, an improvement in the PPP solution convergence time of 35% and 15% is obtained when one and two reference satellites are used, respectively.

## Keywords

PPP, GPS, Galileo, BSSD

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## 1. Introduction

The concept of precise point positioning (PPP) was first introduced by [1]. Dual-frequency GPS PPP technique has been proven to be capable of providing positioning solution at the sub-decimeter level in static mode. This is

achieved through rigorous modeling or estimation of all errors and biases. Both un-differenced and between-satellite single difference (BSSD) ionosphere-free linear combinations of carrier-phase and pseudorange measurements have been used [2] [3]. More recently, [4] showed that a 50% improvement in the PPP convergence time is possible with BSSD dual frequency ionosphere-free GPS, in comparison with the un-differenced counterpart. Unfortunately, dual-frequency GPS receivers may not provide a cost-effective solution to many users. In addition, a drawback of a single GNSS system such as GPS is the availability of a sufficient number of visible satellites in urban areas.

The Galileo satellite system offers additional visible satellites to the user, which is expected to enhance the satellite geometry and the overall PPP solution when combined with GPS [5]. As shown in [6], combining GPS and Galileo observations in a PPP solution reduces the convergence time by up to 30% in comparison with the GPS-only PPP solution. Combining GPS and Galileo, however, comes at the expense of introducing additional biases to the observation mathematical models. These include the GPS to Galileo time offset, and Galileo satellite hardware delay. Recently, the European Space Agency (ESA) estimated the GPS to Galileo time offset (GGTO), which was found to be approximately 50 ns, or equivalently 15 m range error [7].

Generally, combining multi-constellation observations in a PPP solution improves the positioning accuracy, especially when the system biases are calibrated, as shown in [8]. [9] showed that prior correction of the differential GPS/Galileo (GIOVE) inter-system biases significantly increases the success rate of instantaneous ambiguity resolution for short baselines. Likewise, [10] showed that combining GPS/Galileo observables in a double-differenced carrier-phase and pseudorange technique improves the success rate of instantaneous ambiguity resolution in comparison with GPS-only solution. Unfortunately, however, their work was limited to differential positioning mode.

This paper introduces a new PPP model, which combines single-frequency GPS and Galileo observables in BSSD mode. Precise corrections from the International GNSS Service multi-GNSS experiment (IGS-MEGX) network are used to account for GPS and Galileo satellite orbit and clock errors [11]. As these products are presently referenced to the GPS time and since we use mixed GNSS receivers that also use GPS time as a reference, the GGTO is cancelled out in our model. The inter-system bias is either cancelled out through differencing the observations or is treated as an additional unknown parameter as detailed below. The ionospheric delay is largely corrected through the global ionosphere maps (GIM) model [12]. The hydrostatic component of the tropospheric zenith path delay is modelled through the Hopfield model, while the wet component is considered as an additional unknown parameter [5]. All remaining errors and biases are accounted for using existing models as shown in [13]. When forming BSSD, we consider three scenarios in the selection of the reference satellite. Either a GPS or a Galileo satellite is selected as a reference for both GPS and Galileo observables. Alternatively, two reference satellites are selected: a GPS reference satellite for the GPS observables and a Galileo satellite for the Galileo observables. The first approach is sometimes referred to as tight combination, while the latter is sometimes referred to as per constellation or loose combination [9] [14]. It is shown that the use of a single reference satellite provides a sub-decimeter level positioning accuracy and 35% improvement in the convergence time, in comparison with the un-differenced single-frequency GPS/Galileo solution. The use of two reference satellites, although provides comparable positioning accuracy, improves the solution convergence time by 15% only.

## 2. Un-Differenced GPS/Galileo Model

GNSS observations are affected by random and systematic errors, which must be accounted for to ensure that precise positioning solution is obtained. The positioning accuracy of a PPP model depends on the ability to mitigate errors and biases. These errors can be categorized into three classes, namely satellite related errors, signal propagation related errors, and receiver/antenna associated errors. The main GNSS errors include the satellite/receiver clock errors, satellite/receiver hardware delays, ionospheric and tropospheric delays, and multi-path [15].

In addition to the above errors and biases, combining GPS and Galileo observations in a PPP model introduces additional errors such as GGTO due to the fact that each system uses a different time frame. The GPS system uses the GPS time system, which is referenced to coordinated universal time (UTC) as maintained by the US Naval Observatory (USNO). On the other hand, the Galileo satellite system has its own time frame, namely the Galileo system time (GST), which is a continuous atomic time scale with a nominal constant offset with re-

spect to the international atomic time (TAI) [5]. Taking the above errors and biases into consideration and assuming that the observations are taken simultaneously from a mixed GNSS receiver, which uses GPS time as a reference, the GPS and Galileo observation equations can be written as:

$$P_G(t_G) = \rho_G(t_G, t_G - \tau_G) + c[d_{rG}(t_G) + d_G^S(t_G - \tau_G)] + c[dt_{rG}(t_G) - dt_G^S(t_G - \tau_G)] + T_G + I_G + \varepsilon_{PG} \quad (1)$$

$$P_E(t_G) = \rho_E(t_G, t_G - \tau_E) + c[d_{rE}(t_G) + d_E^S(t_G - \tau_E)] + c[dt_{rG}(t_G) - GGTO - dt_E^S(t_G - \tau_E)] + T_E + I_E + \varepsilon_{PE} \quad (2)$$

$$\Phi_G(t_G) = \rho_G(t_G, t_G - \tau_G) + c[\delta_{rG}(t_G) + \delta_G^S(t_G - \tau_G)] + c[dt_{rG}(t_G) - dt_G^S(t_G - \tau_G)] + T_G - I_G + \lambda_G[N + \varphi_r(t_0) - \varphi^S(t_0)]_G + \varepsilon_{\Phi G} \quad (3)$$

$$\Phi_E(t_G) = \rho_E(t_G, t_G - \tau_E) + c[\delta_{rE}(t_G) + \delta_E^S(t_G - \tau_E)] + c[dt_{rG}(t_G) - GGTO - dt_E^S(t_G - \tau_E)] + T_E - I_E + \lambda_E[N + \varphi_r(t_0) - \varphi^S(t_0)]_E + \varepsilon_{\Phi E} \quad (4)$$

where, the subscript  $G$  refers to the GPS satellite system and the subscript  $E$  refers to the Galileo satellite system;  $t_G$  is the true signal reception time;  $\tau_G$  and  $\tau_E$  are signal propagation times for both GPS and Galileo, respectively;  $P_G$  and  $P_E$  are the GPS and Galileo pseudorange measurements, respectively;  $\Phi_G$  and  $\Phi_E$  are the GPS and Galileo carrier-phase measurements, respectively;  $\rho_G(t_G, t_G - \tau_G)$  and  $\rho_E(t_G, t_G - \tau_E)$  are the GPS and Galileo geometric ranges from the receiver at reception time  $t_G$  to the satellite at transmission times  $(t_G - \tau_G)$  and  $(t_G - \tau_E)$ , respectively;  $dt_{rG}(t_G)$  is the receiver clock error at reception time  $t_G$ ;  $dt_G^S(t_G - \tau_G)$  and  $dt_E^S(t_G - \tau_E)$  are the GPS and Galileo satellite clock errors at transmission times  $(t_G - \tau_G)$  and  $(t_G - \tau_E)$ , respectively;  $d_{rG}(t_G)$  and  $d_{rE}(t_G)$  are frequency-dependent code hardware delays in the receiver at reception time  $t_G$  for GPS and Galileo, respectively;  $d_G^S(t_G - \tau_G)$  and  $d_E^S(t_G - \tau_E)$  are frequency-dependent code hardware delays in the satellites at transmission time  $(t_G - \tau_G)$  and  $(t_G - \tau_E)$  for GPS and Galileo, respectively;  $\delta_{rG}(t_G)$  and  $\delta_G^S(t_G - \tau_G)$  are frequency-dependent carrier phase hardware delays in the receiver at reception time  $t_G$  for GPS and Galileo, respectively;  $\delta_{rE}(t_G)$  and  $\delta_E^S(t_G - \tau_E)$  are frequency-dependent carrier phase hardware delays in the satellites at transmission time  $(t_G - \tau_G)$  and  $(t_G - \tau_E)$  for GPS and Galileo, respectively;  $T$  is the tropospheric delay;  $I$  is the ionospheric delay;  $\lambda_G$  and  $\lambda_E$  are the wavelengths of carrier frequencies for GPS and Galileo signals, respectively;  $\Phi_r(t_0)$ ,  $\Phi^S(t_0)$  are frequency-dependent initial fractional phases in the receiver and satellite channels, respectively;  $t_0$  is the receiver (or satellite) initial time;  $N_G$  and  $N_E$  are the integer numbers of cycles for GPS and Galileo carrier phase measurements, respectively; GGTO is the GPS to Galileo time offset;  $c$  is the speed of light in vacuum; and  $\varepsilon_P$ ,  $\varepsilon_\Phi$  are the relevant noise and unmodeled errors.

As indicated earlier, precise orbit and satellite clock corrections of IGS-MGEX network are used for both GPS and Galileo observations. Clock corrections from the two networks are referred to the GPS time. In addition, they include the ionosphere-free linear combination of the satellite hardware delays of L1/L2 P(Y) code for GPS and the ionosphere-free linear combination of the satellite hardware delays of E1/E5a pilot code for Galileo [16]. As such, using Equations (1)-(4) and dropping the time arguments, the L1/E1 single-frequency code and carrier phase observation equations take the form:

$$P_{P1} = \rho_G + \tilde{dt}_{rG} - c[dt_{prec(G)}^s + \beta_G DCB_{P1-P2}^s] + T_G + I_{P1} + \varepsilon_{PG} \quad (5)$$

$$P_{C1} = \rho_G + \tilde{dt}_{rG} - c[dt_{prec(G)}^s + \beta_G DCB_{P1-P2}^s + DCB_{P1-C1}^s] + T_G + I_1 + \varepsilon_{PG} \quad (6)$$

$$P_{E1} = \rho_E + \tilde{dt}_{rG} - c[dt_{prec(E)}^s + \beta_E DCB_{E1-E5a}^s] + T_E + I_1 + ISB + \varepsilon_{PE} \quad (7)$$

$$\Phi_{L1} = \rho_G + \tilde{dt}_{rG} - c[dt_{prec(G)}^s + \beta_G DCB_{P1-P2}^s] + T_G - I_1 + \tilde{N}_{L1} + \varepsilon_{\Phi L1} \quad (8)$$

$$\Phi_{E1} = \rho_E + \tilde{d}t_{rG} - c \left[ dt_{prec(E)}^s + \beta_E DCB_{E1-E5a}^s \right] + T_E - I_1 + ISB + \tilde{N}_{E1} + \varepsilon_{\Phi E1} \quad (9)$$

where  $dt_{prec(G)}^s$  and  $dt_{prec(E)}^s$  are the precise satellites clock corrections for both GPS and Galileo satellites, respectively, which are obtained from IGS-MGEX;  $DCB_{P1-P2}^s$ ,  $DCB_{E1-E5a}^s$  and  $DCB_{P1-C1}^s$  are the satellite differential code biases for GPS P1/P2, P1/C1 and Galileo E1/E5a signals, respectively, which are obtained from IGS;  $\beta_G$  and  $\beta_E$  are the ionosphere-free linear combination coefficients, which equal 1.546 and 1.261 for GPS and Galileo, respectively;  $\tilde{d}t_{rG}$  represents the combined effect of the receiver clock error and the GPS receiver code hardware delay, *i.e.*,  $\tilde{d}t_{rG} = c[d_{rP1} + dt_{rG}]$  when P-code is used and  $\tilde{d}t_{rG} = c[d_{rC1} + dt_{rG}]$  when C/A-code is used;  $ISB$  is the inter-system bias, which equals  $c[d_{rP1} - d_{rE1}]$  when P-code is used and equals  $c[d_{rC1} - d_{rE1}]$  when C/A-code is used;  $\tilde{N}$  is the ambiguity parameter lumped to the satellite and receiver hardware delays, *i.e.*,

$$\tilde{N}_{L1} = \lambda \left[ N + \varphi_r - \varphi^s \right]_G + c \left[ \delta_{rL1} + \delta_{L1}^s \right] - c \left[ d_{rP1} + d_{P1}^s \right] \quad (10)$$

$$\tilde{N}_{E1} = \lambda \left[ N + \varphi_r - \varphi^s \right]_E + c \left[ \delta_{rE1} + \delta_{E1}^s \right] - c \left[ d_{rE1} + d_{E1}^s \right] \quad (11)$$

It should be pointed out that in both of our GPS-only and GPS/Galileo PPP models, the GPS receiver hardware delay is lumped to the receiver clock error as explained above. This strategy maintains the consistency of the estimated receiver clock error for both of the GPS-only and the GPS/Galileo PPP solutions [17]. It should also be mentioned that some of our data sets contain the C/A-code pseudorange rather than the P-code pseudorange. In this case, Equation (6) should replace Equation (5) for the GPS code measurements. In addition, the receiver clock error would be lumped to the receiver hardware delay of the C/A code. Furthermore, the  $ISB$  would equal the difference in the receiver hardware delays of the C/A code and E1 code, scaled by the speed of light.

Equations (5) to (9) can be simplified for the pseudorange and carrier phase observables after applying the corrections for the satellite clock errors, the hydrostatic component of the tropospheric zenith path delay, the correction to the ionospheric delay, the satellite differential code biases, and the other remaining biases. As stated earlier, the global ionosphere maps (GIM) are used to account for the ionospheric delay [12]. Generally, GIM ionospheric model was found superior to other global models such as the Klobuchar model [18]-[20]. The Hopfield tropospheric correction model is used, along with Vienna mapping function, to account for the hydrostatic component of the tropospheric delay [21] [22]. All other remaining biases are modeled using existing models, including the effects of ocean loading [23] [24], Earth tide [13], carrier-phase windup [25] [26], Sagnac [27], relativity [5], and satellite and receiver antenna phase-center variations [28]. Applying these corrections and considering P-code observations only lead to:

$$\rho_G + \tilde{d}t_{rG} + m_f zpd_w + \tilde{\varepsilon}_{PG} - \tilde{P}_{P1} = 0 \quad (12)$$

$$\rho_E + \tilde{d}t_{rG} + m_f zpd_w + ISB + \tilde{\varepsilon}_{PE} - \tilde{P}_{E1} = 0 \quad (13)$$

$$\rho_G + \tilde{d}t_{rG} + m_f zpd_w + \tilde{N}_{L1} + \tilde{\varepsilon}_{\Phi L1} - \tilde{\Phi}_{L1} = 0 \quad (14)$$

$$\rho_E + \tilde{d}t_{rG} + m_f zpd_w + ISB + \tilde{N}_{E1} + \tilde{\varepsilon}_{\Phi E1} - \tilde{\Phi}_{E1} = 0 \quad (15)$$

where  $\tilde{P}$  and  $\tilde{\Phi}$  are the corrected carrier phase and pseudorange observables;  $zpd_w$  is the wet component of the tropospheric zenith path;  $m_f$  is the troposphere mapping function;  $\tilde{\varepsilon}_{PG}$ ,  $\tilde{\varepsilon}_{PE}$ ,  $\tilde{\varepsilon}_{\Phi L1}$  and  $\tilde{\varepsilon}_{\Phi E1}$  are the noise terms.

### 3. BSSD GPS/Galileo Combination Model

Differencing the observations between satellites cancels out most receiver-related errors, including receiver clock error, receiver hardware delay for the same constellation, and non-zero initial phase bias [15]. As the L1 and E1 frequencies are the same, we can select a single satellite, either a GPS or a Galileo as a reference when forming the BSSD. This means that the observations of all other GPS and Galileo satellites are differenced with

respect to the observations of that satellite. As indicated earlier, this approach is sometimes referred to as tight combination. Alternatively, two reference satellites can be used, *i.e.*, per constellation BSSD. The former approach produces two additional BSSD equations in comparison with the second approach, one for code and another for carrier-phase observables. However, the ISB is cancelled out when the per-constellation approach is used. When a GPS satellite is used as a reference in a tight combination, we obtain:

$$\nabla \rho_{G,G}^{ij} + m_f^{ij} zpd_w + \nabla \tilde{\epsilon}_{PG}^{ij} - \nabla \tilde{P}_{P1}^{ij} = 0 \quad (16)$$

$$\nabla \rho_{E,G}^{ik} + m_f^{ik} zpd_w + ISB + \nabla \tilde{\epsilon}_{PE}^{ik} - \nabla \tilde{P}_{E1G}^{ik} = 0 \quad (17)$$

$$\nabla \rho_{G,G}^{ij} + m_f^{ij} zpd_w + \tilde{N}_{L1}^{ij} + \nabla \tilde{\epsilon}_{\Phi L1}^{ij} - \nabla \tilde{\Phi}_{L1}^{ij} = 0 \quad (18)$$

$$\nabla \rho_{E,G}^{ik} + m_f^{ik} zpd_w + ISB + \tilde{N}_{E1}^{ik} + \nabla \tilde{\epsilon}_{\Phi E1}^{ik} - \nabla \tilde{\Phi}_{E1G}^{ik} = 0 \quad (19)$$

where  $\nabla$  refers to the BSSD operator;  $\tilde{N}_{L1}^{ij}$  and  $\tilde{N}_{E1}^{ik}$  are the BSSD non-integer the ambiguity parameters lumped to the receiver and satellite hardware delays as shown in Equations (20) and (21).

$$\tilde{N}_{L1}^{ij} = \lambda [N_G^j - N_G^i] - \lambda [\phi_G^j - \phi_G^i] + c [\delta_{L1}^j - \delta_{L1}^i] - c [d_{P1}^j - d_{P1}^i] \quad (20)$$

$$\begin{aligned} \tilde{N}_{E1}^{ik} &= \lambda [N_E^k - N_E^i] - \lambda [\phi_E^k - \phi_E^i] + c [\delta_{rE1}^k + \delta_{E1}^k] - c [\delta_{rL1}^i + \delta_{L1}^i] \\ &\quad - c [d_{rE1}^k + d_{E1}^k] + c [d_{rP1}^i + d_{P1}^i] \end{aligned} \quad (21)$$

If, however, a Galileo satellite is used as a reference in a tight combination, we obtain the following set of BSSD equations:

$$\nabla \rho_{G,E}^{lj} + m_f^{lj} zpd_w - ISB + \nabla \tilde{\epsilon}_{PG}^{lj} - \nabla \tilde{P}_{P1E}^{lj} = 0 \quad (22)$$

$$\nabla \rho_{E,E}^{lk} + m_f^{lk} zpd_w + \nabla \tilde{\epsilon}_{PE}^{lk} - \nabla \tilde{P}_{E1}^{lk} = 0 \quad (23)$$

$$\nabla \rho_{G,E}^{lj} + m_f^{lj} zpd_w - ISB + \tilde{N}_{L1}^{lj} + \nabla \tilde{\epsilon}_{\Phi L1}^{lj} - \nabla \tilde{\Phi}_{L1E}^{lj} = 0 \quad (24)$$

$$\nabla \rho_{E,E}^{lk} + m_f^{lk} zpd_w + \tilde{N}_{E1}^{lk} + \nabla \tilde{\epsilon}_{\Phi E1}^{lk} - \nabla \tilde{\Phi}_{E1}^{lk} = 0 \quad (25)$$

where,  $\tilde{N}_{L1}^{lj}$  and  $\tilde{N}_{E1}^{lk}$  are the BSSD non-integer ambiguity parameters lumped to the receiver and satellite hardware delays as shown in Equations (26) and (27).

$$\begin{aligned} \tilde{N}_{L1}^{lj} &= \lambda [N_G^j - N_E^l] - \lambda [\phi_E^l - \phi_G^j] + c [\delta_{rL1}^j + \delta_{L1}^j] - c [\delta_{rE1}^l + \delta_{E1}^l] \\ &\quad - c [d_{rP1}^j + d_{P1}^j] + c [d_{rE1}^l + d_{E1}^l] \end{aligned} \quad (26)$$

$$\tilde{N}_{E1}^{lk} = \lambda [N_E^k - N_E^l] - \lambda [\phi_E^k - \phi_E^l] + c [\delta_{E1}^k - \delta_{E1}^l] - c [d_{E1}^k - d_{E1}^l] \quad (27)$$

Finally, the per-constellation BSSD equations take the form:

$$\nabla \rho_{G,G}^{ij} + m_f^{ij} zpd_w + \nabla \tilde{\epsilon}_{PG}^{ij} - \nabla \tilde{P}_{P1}^{ij} = 0 \quad (28)$$

$$\nabla \rho_{E,E}^{lk} + m_f^{lk} zpd_w + \nabla \tilde{\epsilon}_{PE}^{lk} - \nabla \tilde{P}_{E1}^{lk} = 0 \quad (29)$$

$$\nabla \rho_{G,G}^{ij} + m_f^{ij} zpd_w + \tilde{N}_{L1}^{ij} + \nabla \tilde{\epsilon}_{\Phi L1}^{ij} - \nabla \tilde{\Phi}_{L1}^{ij} = 0 \quad (30)$$

$$\nabla \rho_{E,E}^{lk} + m_f^{lk} zpd_w + \tilde{N}_{E1}^{lk} + \nabla \tilde{\epsilon}_{\Phi E1}^{lk} - \nabla \tilde{\Phi}_{E1}^{lk} = 0 \quad (31)$$

where,  $\tilde{N}_{L1}^{ij}$  and  $\tilde{N}_{E1}^{lk}$  are the BSSD non-integer ambiguity parameters lumped to the receiver and satellite

hardware delays as shown in Equations (32) and (33).

$$\tilde{N}_{L1}^{ij} = \lambda [N_G^j - N_G^i] - \lambda [\varphi_G^j - \varphi_G^i] + c [\delta_{L1}^j - \delta_{L1}^i] - c [d_{P1}^j - d_{P1}^i] \quad (32)$$

$$\tilde{N}_{E1}^{lk} = \lambda [N_E^k - N_E^l] - \lambda [\varphi_E^k - \varphi_E^l] + c [\delta_{E1}^k - \delta_{E1}^l] - c [d_{E1}^k - d_{E1}^l] \quad (33)$$

It should be noticed from the above equations that the modified receiver clock error (*i.e.*, the common term  $\tilde{dt}_{rG}$ ) and the initial phase bias cancel out when forming BSSD with one satellite selected as a reference (*i.e.*, tight combination). However, when forming per constellation BSSD, the modified receiver clock error, the inter-system bias, and the initial phase bias are all cancelled out.

#### 4. Sequential Least Squares Estimation

The sequential least-squares estimation technique is used to obtain the best estimates, in the least squares sense, of the unknown parameters. The noise terms in the above observations equations are modeled stochastically using an exponential function, as described in [6]. They showed that, in comparison with existing stochastic models such as the general sine function, the use of the exponential model improves the PPP solution precision and convergence time. The general linearized form for the above observations equations around the initial (approximate) vector  $\mathbf{u}^0$  and observables  $\mathbf{l}$  can be written in a compact form as:

$$\mathbf{f}(\mathbf{u}, \mathbf{l}) \approx \mathbf{A}\Delta\mathbf{u} - \mathbf{w} - \mathbf{r} \approx 0 \quad (34)$$

where  $\mathbf{u}$  is the vector of unknown parameters;  $\mathbf{A}$  is the design matrix, which includes the partial derivatives of the observation equations with respect to the unknown parameters  $\mathbf{u}$ ;  $\Delta\mathbf{u}$  is the unknown vector of corrections to the approximate parameters  $\mathbf{u}^0$ , *i.e.*,  $\mathbf{u} = \mathbf{u}^0 + \Delta\mathbf{u}$ ;  $\mathbf{w}$  is the misclosure vector and  $\mathbf{r}$  is the vector of residuals. The sequential least-squares solution for the unknown parameters  $\Delta\mathbf{u}_i$  at an epoch  $i$  can be obtained from (Vanicek and Krakiwsky, 1986):

$$\Delta\mathbf{u}_i = \Delta\mathbf{u}_{i-1} + \mathbf{M}_{i-1}^{-1} \mathbf{A}_i^T (\mathbf{C}_i + \mathbf{A}_i \mathbf{M}_{i-1}^{-1} \mathbf{A}_i^T)^{-1} [\mathbf{w}_i - \mathbf{A}_i \Delta\mathbf{u}_{i-1}] \quad (35)$$

$$\mathbf{M}_i^{-1} = \mathbf{M}_{i-1}^{-1} - \mathbf{M}_{i-1}^{-1} \mathbf{A}_i^T (\mathbf{C}_i + \mathbf{A}_i \mathbf{M}_{i-1}^{-1} \mathbf{A}_i^T)^{-1} \mathbf{A}_i \mathbf{M}_{i-1}^{-1} \quad (36)$$

$$\mathbf{C}_{\Delta\mathbf{u}_i} = \mathbf{M}_i^{-1} = \mathbf{M}_{i-1}^{-1} - \mathbf{M}_{i-1}^{-1} \mathbf{A}_i^T (\mathbf{C}_i + \mathbf{A}_i \mathbf{M}_{i-1}^{-1} \mathbf{A}_i^T)^{-1} \mathbf{A}_i \mathbf{M}_{i-1}^{-1} \quad (37)$$

where  $\Delta\mathbf{u}_{i-1}$  is the least-squares solution for the estimated parameters at epoch  $i-1$ ;  $\mathbf{M}$  is the matrix of the normal equations;  $\mathbf{C}_i$  and  $\mathbf{C}_{\Delta\mathbf{u}}$  are the covariance matrices of the observations and unknown parameters, respectively. It should be pointed out that the usual batch least-squares adjustment should be used in the first epoch, *i.e.*, for  $i = 1$ . The batch solution for the estimated parameters and the inverse of the normal equation matrix are given respectively by [29]:

$$\Delta\mathbf{u}_1 = [\mathbf{C}_x^0 + \mathbf{A}_1^T \mathbf{C}_1^{-1} \mathbf{A}_1]^{-1} \mathbf{A}_1^T \mathbf{C}_1^{-1} \mathbf{w}_1 \quad (38)$$

$$\mathbf{M}_1^{-1} = [\mathbf{C}_x^0 + \mathbf{A}_1^T \mathbf{C}_1^{-1} \mathbf{A}_1]^{-1} \quad (39)$$

where  $\mathbf{C}_x^0$  is a priori covariance matrix for the approximate values of the unknown parameters.

Under the assumption that the observations are uncorrelated and the errors are normally distributed with zero mean, the covariance matrix of the un-differenced observations takes the form of a diagonal matrix. The elements along the diagonal line represent the variances of the code and carrier phase measurements. In our solution, we consider that the ration between the standard deviation of the code and carrier-phase measurements to be 100. When forming BSSD, however, the differenced observations become mathematically correlated. This leads to a fully populated covariance matrix at a particular epoch.

Considering the un-differenced mode, the matrix  $\mathbf{A}$  and the vector  $\Delta\mathbf{u}$  at a particular epoch are given by:

$$\mathbf{A} = \begin{bmatrix} \left(\frac{x_0 - X^{1G}}{\rho_0^{1G}}\right) & \left(\frac{y_0 - Y^{1G}}{\rho_0^{1G}}\right) & \left(\frac{z_0 - Z^{1G}}{\rho_0^{1G}}\right) & 1 & m_f^{1G} & 0 & 0 & \cdots & 0 & 0 & \cdots & 0 \\ \left(\frac{x_0 - X^{1G}}{\rho_0^{1G}}\right) & \left(\frac{y_0 - Y^{1G}}{\rho_0^{1G}}\right) & \left(\frac{z_0 - Z^{1G}}{\rho_0^{1G}}\right) & 1 & m_f^{1G} & 0 & 1 & \cdots & 0 & 0 & \cdots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \ddots & \vdots \\ \left(\frac{x_0 - X^{nG}}{\rho_0^{nG}}\right) & \left(\frac{y_0 - Y^{nG}}{\rho_0^{nG}}\right) & \left(\frac{z_0 - Z^{nG}}{\rho_0^{nG}}\right) & 1 & m_f^{nG} & 0 & 0 & \cdots & 0 & 0 & \cdots & 0 \\ \left(\frac{x_0 - X^{nG}}{\rho_0^{nG}}\right) & \left(\frac{y_0 - Y^{nG}}{\rho_0^{nG}}\right) & \left(\frac{z_0 - Z^{nG}}{\rho_0^{nG}}\right) & 1 & m_f^{nG} & 0 & 0 & \cdots & 1 & 0 & \cdots & 0 \\ \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) & \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) & \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) & 1 & m_f^{1E} & 1 & 0 & \cdots & 0 & 0 & \cdots & 0 \\ \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) & \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) & \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) & 1 & m_f^{1E} & 1 & 0 & \cdots & 0 & 1 & \cdots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \ddots & \vdots \\ \left(\frac{x_0 - X^{nE}}{\rho_0^{nE}}\right) & \left(\frac{y_0 - Y^{nE}}{\rho_0^{nE}}\right) & \left(\frac{z_0 - Z^{nE}}{\rho_0^{nE}}\right) & 1 & m_f^{nE} & 1 & 0 & \cdots & 0 & 0 & \cdots & 0 \\ \left(\frac{x_0 - X^{nE}}{\rho_0^{nE}}\right) & \left(\frac{y_0 - Y^{nE}}{\rho_0^{nE}}\right) & \left(\frac{z_0 - Z^{nE}}{\rho_0^{nE}}\right) & 1 & m_f^{nE} & 1 & 0 & \cdots & 0 & 0 & \cdots & 1 \end{bmatrix}_{2n \times (n+6)}$$

$$\Delta \mathbf{u} = \begin{bmatrix} \Delta x \\ \Delta y \\ \Delta z \\ \hat{d}t_{rG} \\ zpd_w \\ ISB \\ \tilde{N}_{L1}^1 \\ \vdots \\ \tilde{N}_{L1}^{nG} \\ \tilde{N}_{E1}^1 \\ \vdots \\ \tilde{N}_{E1}^{nE} \end{bmatrix}_{n+6} \quad (40)$$

where  $n_G$  refers to the number of visible GPS satellites;  $n_E$  refers to the number of visible Galileo satellites;  $n = n_G + n_E$  is the total number of the observed satellites for both GPS and Galileo systems;  $x_0, y_0$  and  $z_0$  are the approximate receiver coordinates;  $X^{jG}, Y^{jG}, Z^{jG}, j=1,2,\dots,n_G$  are the known GPS satellite coordinates;  $X^{kE}, Y^{kE}, Z^{kE}, k=1,2,\dots,n_E$  are the known Galileo satellite coordinates;  $\rho_0$  is the approximate receiver-satellite range. The unknown parameters in the above system are the corrections to the receiver coordinates,  $\Delta x$ ,  $\Delta y$ , and  $\Delta z$ , the biased receiver clock error  $\hat{d}t_{rG}$ , the wet component of the tropospheric zenith path delay  $zpd_w$ , the inter-system bias  $ISB$ , and the non-integer ambiguity parameters  $\tilde{N}$ . It should be pointed out that the number of unknown parameters in the above system equals  $n_G + n_E + 6$ , while the number of equations equals  $2n_G + 2n_E$ . This means that the redundancy equals  $n_G + n_E - 6$ . In other words, at least 6 mixed satellites are needed for the solution to exist. In comparison with the GPS-only un-differenced scenario, which requires a minimum of 5 satellites for the solution to exist, the addition of Galileo satellites increases the redundancy by  $n_E - 1$ . In other words, we need a minimum of two Galileo satellites in order to contribute to the solution.

When a GPS satellite is selected as a reference to form the BSSD for both GPS and Galileo observations, the design matrix  $\mathbf{A}$  and the vector of corrections  $\Delta \mathbf{u}$  take the form:

$$\mathbf{A} = \begin{bmatrix} \left(\frac{x_0 - X^{2G}}{\rho_0^{2G}}\right) - \left(\frac{x_0 - X^{1G}}{\rho_0^{1G}}\right) & \left(\frac{y_0 - Y^{2G}}{\rho_0^{2G}}\right) - \left(\frac{y_0 - Y^{1G}}{\rho_0^{1G}}\right) & \left(\frac{z_0 - Z^{2G}}{\rho_0^{2G}}\right) - \left(\frac{z_0 - Z^{1G}}{\rho_0^{1G}}\right) & m_f^{2G1G} & 0 & 0 & \cdots & 0 & 0 & \cdots & 0 \\ \left(\frac{x_0 - X^{2G}}{\rho_0^{2G}}\right) - \left(\frac{x_0 - X^{1G}}{\rho_0^{1G}}\right) & \left(\frac{y_0 - Y^{2G}}{\rho_0^{2G}}\right) - \left(\frac{y_0 - Y^{1G}}{\rho_0^{1G}}\right) & \left(\frac{z_0 - Z^{2G}}{\rho_0^{2G}}\right) - \left(\frac{z_0 - Z^{1G}}{\rho_0^{1G}}\right) & m_f^{2G1G} & 0 & 1 & \cdots & 0 & 0 & \cdots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \ddots & \vdots \\ \left(\frac{x_0 - X^{nG}}{\rho_0^{nG}}\right) - \left(\frac{x_0 - X^{1G}}{\rho_0^{1G}}\right) & \left(\frac{y_0 - Y^{nG}}{\rho_0^{nG}}\right) - \left(\frac{y_0 - Y^{1G}}{\rho_0^{1G}}\right) & \left(\frac{z_0 - Z^{nG}}{\rho_0^{nG}}\right) - \left(\frac{z_0 - Z^{1G}}{\rho_0^{1G}}\right) & m_f^{nG1G} & 0 & 0 & \cdots & 0 & 0 & \cdots & 0 \\ \left(\frac{x_0 - X^{nG}}{\rho_0^{nG}}\right) - \left(\frac{x_0 - X^{1G}}{\rho_0^{1G}}\right) & \left(\frac{y_0 - Y^{nG}}{\rho_0^{nG}}\right) - \left(\frac{y_0 - Y^{1G}}{\rho_0^{1G}}\right) & \left(\frac{z_0 - Z^{nG}}{\rho_0^{nG}}\right) - \left(\frac{z_0 - Z^{1G}}{\rho_0^{1G}}\right) & m_f^{nG1G} & 0 & 0 & \cdots & 1 & 0 & \cdots & 0 \\ \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) - \left(\frac{x_0 - X^{1G}}{\rho_0^{1G}}\right) & \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) - \left(\frac{y_0 - Y^{1G}}{\rho_0^{1G}}\right) & \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) - \left(\frac{z_0 - Z^{1G}}{\rho_0^{1G}}\right) & m_f^{1E1G} & 1 & 0 & \cdots & 0 & 0 & \cdots & 0 \\ \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) - \left(\frac{x_0 - X^{1G}}{\rho_0^{1G}}\right) & \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) - \left(\frac{y_0 - Y^{1G}}{\rho_0^{1G}}\right) & \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) - \left(\frac{z_0 - Z^{1G}}{\rho_0^{1G}}\right) & m_f^{1E1G} & 1 & 0 & \cdots & 0 & 1 & \cdots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \ddots & \vdots \\ \left(\frac{x_0 - X^{nE}}{\rho_0^{nE}}\right) - \left(\frac{x_0 - X^{1G}}{\rho_0^{1G}}\right) & \left(\frac{y_0 - Y^{nE}}{\rho_0^{nE}}\right) - \left(\frac{y_0 - Y^{1G}}{\rho_0^{1G}}\right) & \left(\frac{z_0 - Z^{nE}}{\rho_0^{nE}}\right) - \left(\frac{z_0 - Z^{1G}}{\rho_0^{1G}}\right) & m_f^{nE1G} & 1 & 0 & \cdots & 0 & 0 & \cdots & 0 \\ \left(\frac{x_0 - X^{nE}}{\rho_0^{nE}}\right) - \left(\frac{x_0 - X^{1G}}{\rho_0^{1G}}\right) & \left(\frac{y_0 - Y^{nE}}{\rho_0^{nE}}\right) - \left(\frac{y_0 - Y^{1G}}{\rho_0^{1G}}\right) & \left(\frac{z_0 - Z^{nE}}{\rho_0^{nE}}\right) - \left(\frac{z_0 - Z^{1G}}{\rho_0^{1G}}\right) & m_f^{nE1G} & 1 & 0 & \cdots & 0 & 0 & \cdots & 1 \end{bmatrix}_{2(n-1) \times (n+4)}$$

$$\Delta \mathbf{u} = \begin{bmatrix} \Delta x \\ \Delta y \\ \Delta z \\ zpd_w \\ ISB \\ \nabla \tilde{N}_{L1}^{21G} \\ \vdots \\ \nabla \tilde{N}_{L1}^{nG1G} \\ \nabla \tilde{N}_{E1}^{11G} \\ \vdots \\ \nabla \tilde{N}_{E1}^{nE1G} \end{bmatrix}_{n+4} \quad (41)$$



where  $1_G$  refers to the GPS reference satellite. All other parameters are as defined above. The advantage of the above system (42) is that the number of unknown parameters is reduced by two (*i.e.*, becomes  $n_G + n_E + 4$ ), in comparison with the un-differenced scenario. This, however, comes at the expense of reducing the number of BSSD observation equations to  $2(n_G + n_E - 1)$ . As such, the redundancy remains unchanged and equals  $n_G + n_E - 6$ . Similarly, we need a minimum of two Galileo satellites in order to contribute to the solution. By analogy, the use of a Galileo satellite as a reference to form the BSSD for both GPS and Galileo observations leads to:

$$A = \begin{bmatrix} \left(\frac{x_0 - X^{1G}}{\rho_0^{1G}}\right) - \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) & \left(\frac{y_0 - Y^{1G}}{\rho_0^{1G}}\right) - \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) & \left(\frac{z_0 - Z^{1G}}{\rho_0^{1G}}\right) - \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) & m_f^{1G^{1E}} & 1 & 0 & \dots & 0 & 0 & \dots & 0 \\ \left(\frac{x_0 - X^{1G}}{\rho_0^{1G}}\right) - \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) & \left(\frac{y_0 - Y^{1G}}{\rho_0^{1G}}\right) - \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) & \left(\frac{z_0 - Z^{1G}}{\rho_0^{1G}}\right) - \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) & m_f^{1G^{1E}} & 1 & 1 & \dots & 0 & 0 & \dots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \ddots & \vdots \\ \left(\frac{x_0 - X^{nG}}{\rho_0^{nG}}\right) - \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) & \left(\frac{y_0 - Y^{nG}}{\rho_0^{nG}}\right) - \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) & \left(\frac{z_0 - Z^{nG}}{\rho_0^{nG}}\right) - \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) & m_f^{nG^{1E}} & 1 & 0 & \dots & 0 & 0 & \dots & 0 \\ \left(\frac{x_0 - X^{nG}}{\rho_0^{nG}}\right) - \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) & \left(\frac{y_0 - Y^{nG}}{\rho_0^{nG}}\right) - \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) & \left(\frac{z_0 - Z^{nG}}{\rho_0^{nG}}\right) - \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) & m_f^{nG^{1E}} & 1 & 0 & \dots & 1 & 0 & \dots & 0 \\ \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) - \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) & \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) - \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) & \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) - \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) & m_f^{2E^{1E}} & 0 & 0 & \dots & 0 & 0 & \dots & 0 \\ \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) - \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) & \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) - \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) & \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) - \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) & m_f^{2E^{1E}} & 0 & 0 & \dots & 0 & 1 & \dots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \ddots & \vdots \\ \left(\frac{x_0 - X^{nE}}{\rho_0^{nE}}\right) - \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) & \left(\frac{y_0 - Y^{nE}}{\rho_0^{nE}}\right) - \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) & \left(\frac{z_0 - Z^{nE}}{\rho_0^{nE}}\right) - \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) & m_f^{nE^{1E}} & 0 & 0 & \dots & 0 & 0 & \dots & 0 \\ \left(\frac{x_0 - X^{nE}}{\rho_0^{nE}}\right) - \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) & \left(\frac{y_0 - Y^{nE}}{\rho_0^{nE}}\right) - \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) & \left(\frac{z_0 - Z^{nE}}{\rho_0^{nE}}\right) - \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) & m_f^{nE^{1E}} & 0 & 0 & \dots & 0 & 0 & \dots & 1 \end{bmatrix}_{2(n-1) \times (n+4)}$$

$$\Delta \mathbf{u} = \begin{bmatrix} \Delta x \\ \Delta y \\ \Delta z \\ zpd_w \\ ISB \\ \nabla \tilde{N}_{L1}^{1E} \\ \vdots \\ \nabla \tilde{N}_{L1}^{nG^{1E}} \\ \nabla \tilde{N}_{E1}^{2E} \\ \vdots \\ \nabla \tilde{N}_{E1}^{nE^{1E}} \end{bmatrix}_{n+4} \quad (42)$$

where  $1_E$  refers to the Galileo reference satellite. All other parameters are as defined above. Similar to the above BSSD scenario, the redundancy remains unchanged and equals  $n_G + n_E - 6$ .

When two reference satellites are selected to form the BSSD, *i.e.*, per-constellation BSSD, the design matrix  $A$  and the vector of corrections  $\Delta \mathbf{u}$  take the form:

$$A = \begin{bmatrix} \left(\frac{x_0 - X^{2G}}{\rho_0^{2G}}\right) - \left(\frac{x_0 - X^{1G}}{\rho_0^{1G}}\right) & \left(\frac{y_0 - Y^{2G}}{\rho_0^{2G}}\right) - \left(\frac{y_0 - Y^{1G}}{\rho_0^{1G}}\right) & \left(\frac{z_0 - Z^{2G}}{\rho_0^{2G}}\right) - \left(\frac{z_0 - Z^{1G}}{\rho_0^{1G}}\right) & m_f^{2G^{1G}} & 0 & \dots & 0 & 0 & \dots & 0 \\ \left(\frac{x_0 - X^{2G}}{\rho_0^{2G}}\right) - \left(\frac{x_0 - X^{1G}}{\rho_0^{1G}}\right) & \left(\frac{y_0 - Y^{2G}}{\rho_0^{2G}}\right) - \left(\frac{y_0 - Y^{1G}}{\rho_0^{1G}}\right) & \left(\frac{z_0 - Z^{2G}}{\rho_0^{2G}}\right) - \left(\frac{z_0 - Z^{1G}}{\rho_0^{1G}}\right) & m_f^{2G^{1G}} & 1 & \dots & 0 & 0 & \dots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \ddots & \vdots \\ \left(\frac{x_0 - X^{nG}}{\rho_0^{nG}}\right) - \left(\frac{x_0 - X^{1G}}{\rho_0^{1G}}\right) & \left(\frac{y_0 - Y^{nG}}{\rho_0^{nG}}\right) - \left(\frac{y_0 - Y^{1G}}{\rho_0^{1G}}\right) & \left(\frac{z_0 - Z^{nG}}{\rho_0^{nG}}\right) - \left(\frac{z_0 - Z^{1G}}{\rho_0^{1G}}\right) & m_f^{nG^{1G}} & 0 & \dots & 0 & 0 & \dots & 0 \\ \left(\frac{x_0 - X^{nG}}{\rho_0^{nG}}\right) - \left(\frac{x_0 - X^{1G}}{\rho_0^{1G}}\right) & \left(\frac{y_0 - Y^{nG}}{\rho_0^{nG}}\right) - \left(\frac{y_0 - Y^{1G}}{\rho_0^{1G}}\right) & \left(\frac{z_0 - Z^{nG}}{\rho_0^{nG}}\right) - \left(\frac{z_0 - Z^{1G}}{\rho_0^{1G}}\right) & m_f^{nG^{1G}} & 0 & \dots & 1 & 0 & \dots & 0 \\ \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) - \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) & \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) - \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) & \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) - \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) & m_f^{2E^{1E}} & 0 & \dots & 0 & 0 & \dots & 0 \\ \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) - \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) & \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) - \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) & \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) - \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) & m_f^{2E^{1E}} & 0 & \dots & 0 & 1 & \dots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \ddots & \vdots \\ \left(\frac{x_0 - X^{nE}}{\rho_0^{nE}}\right) - \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) & \left(\frac{y_0 - Y^{nE}}{\rho_0^{nE}}\right) - \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) & \left(\frac{z_0 - Z^{nE}}{\rho_0^{nE}}\right) - \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) & m_f^{nE^{1E}} & 0 & \dots & 0 & 0 & \dots & 0 \\ \left(\frac{x_0 - X^{nE}}{\rho_0^{nE}}\right) - \left(\frac{x_0 - X^{1E}}{\rho_0^{1E}}\right) & \left(\frac{y_0 - Y^{nE}}{\rho_0^{nE}}\right) - \left(\frac{y_0 - Y^{1E}}{\rho_0^{1E}}\right) & \left(\frac{z_0 - Z^{nE}}{\rho_0^{nE}}\right) - \left(\frac{z_0 - Z^{1E}}{\rho_0^{1E}}\right) & m_f^{nE^{1E}} & 0 & \dots & 0 & 0 & \dots & 1 \end{bmatrix}_{2(n-2) \times (n+2)}$$

$$\Delta \mathbf{u} = \begin{bmatrix} \Delta x \\ \Delta y \\ \Delta z \\ zpd_w \\ \nabla \tilde{N}_{L1}^{2G^{1G}} \\ \vdots \\ \nabla \tilde{N}_{L1}^{nG^{1G}} \\ \nabla \tilde{N}_{E1}^{12E} \\ \vdots \\ \nabla \tilde{N}_{E1}^{nE^{1E}} \end{bmatrix}_{n+2} \quad (43)$$

The major advantage of the above per-constellation (or loose combination) system is that the modified receiver clock error and the inter-system bias are cancelled out. In addition, the total number of unknown parameters is reduced by 4 to become  $n_G + n_E + 2$ , in comparison with the un-differenced scenario. This, however, comes at the expense of reducing the number of BSSD observation equations to  $2(n_G + n_E - 2)$ . This means



that the redundancy remains unchanged and equals  $n_G + n_E - 6$ . Similar to the previous scenarios, the redundancy for the GPS-only scenario is still  $n_G - 5$  and the addition of Galileo satellites increased the overall redundancy to  $n_E - 1$ . As such, we still need a minimum of two Galileo satellites in order to contribute to the solution. However, as indicated by [14], the adjustment model is stronger through the tight combination, *i.e.*, when a single satellite is used as a reference.

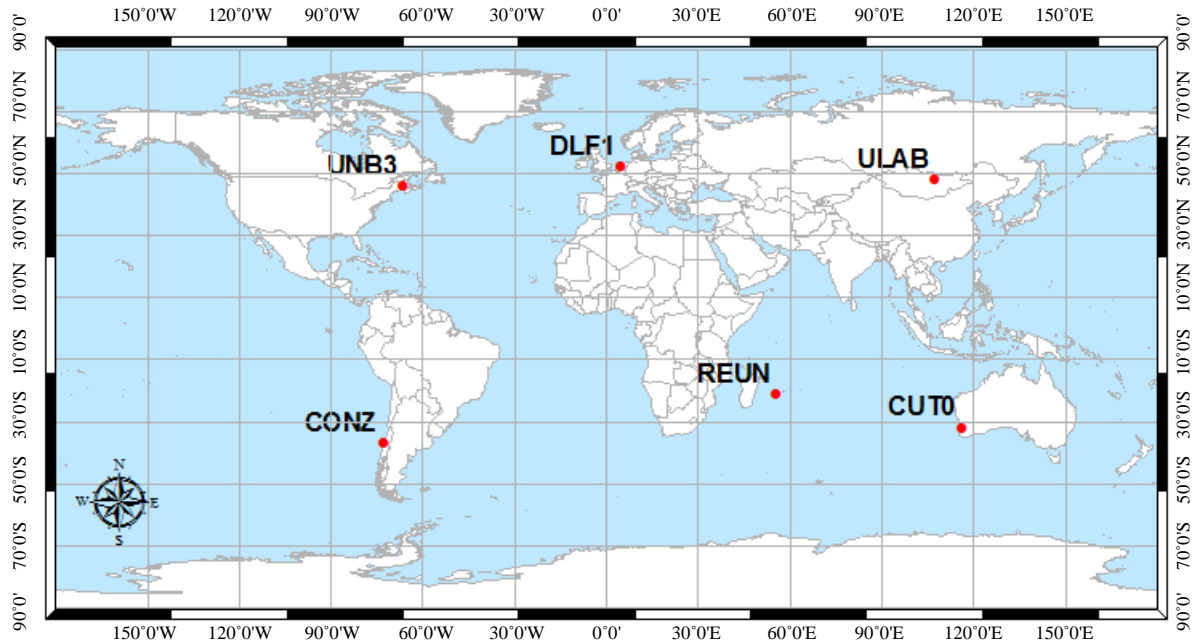
## 5. Results and Discussion

To verify the developed GPS/Galileo PPP model, GPS and Galileo measurements at six well-distributed stations (**Figure 1**) were selected from the IGS tracking network [28]. Those stations are occupied by GNSS receivers, which are capable of simultaneously tracking the GPS and Galileo constellations. The analysis is performed on two different days January 1, 2014 and July 8, 2014 for all stations shown in **Figure 1**.

The sampling interval for all data sets is 30 seconds, while the time span used in the analysis is three hours, which is selected at different times of the day to ensure that the four Galileo satellites are visible at each station. GPSpace PPP software of Natural Resources Canada (NRCAN) was modified to enable a GPS/Galileo PPP solution as described above. The positioning results for stations CONZ, and CUT0 (January 1, 2014) and stations DLF1, and UNB3 (July 8, 2014) are presented below. Similar results are obtained from the other stations. However, a summary of the convergence times is presented below for all stations.

The single-frequency GPS/Galileo PPP solution is implemented through combining the GPS L1 signal with the Galileo E1 signal. As mentioned earlier, three different scenarios are considered when processing the data sets with the BSSD model, namely (1) a GPS satellite is selected as a reference satellite for both GPS and Galileo observables; (2) a Galileo satellite is selected as a reference satellite for both GPS and Galileo observables; and (3) two reference satellites are selected: a GPS reference satellite for the GPS observables and a Galileo satellite for the Galileo observables. To assess the PPP solution accuracy of the developed single-frequency model, un-differenced dual-frequency ionosphere-free linear combination of GPS/Galileo PPP is used as a reference. **Figure 2** shows the reference solution for July 8, 2014, as an example. As can be seen, the dual-frequency GPS/Galileo PPP solution has a sub-decimeter positioning accuracy with approximately 15 minutes convergence time (*i.e.*, the time that the solution takes to converge to a decimetre-level positioning accuracy).

**Figure 3** shows the PPP results for the un-differenced single-frequency GPS/Galileo model. As can be seen, the single-frequency GPS/Galileo PPP solution shows a decimetre level accuracy and approximately 100 minutes convergence time. It should be emphasized that the exponential function is used to model the stochastic



**Figure 1.** Analysis stations.

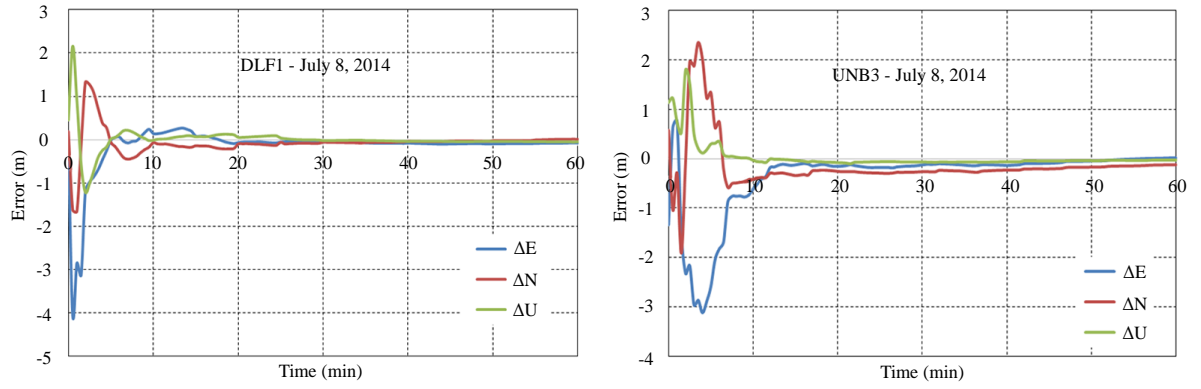


Figure 2. Un-differenced ionosphere-free GPS/Galileo PPP solution.

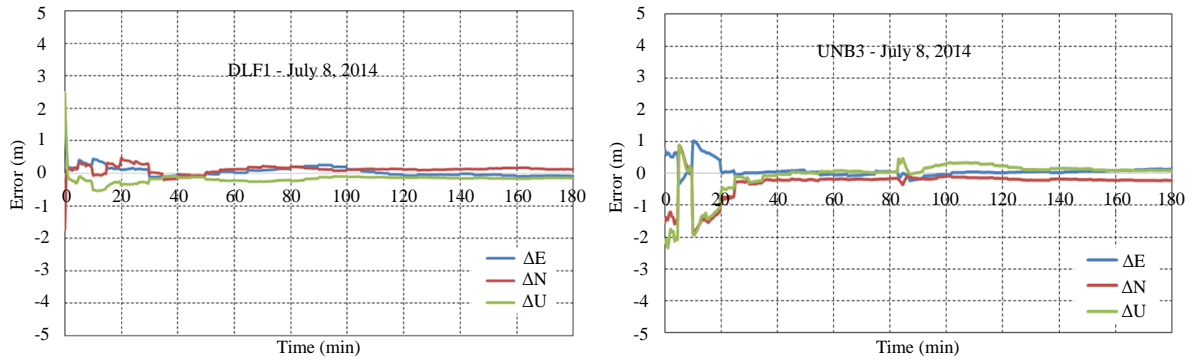


Figure 3. Un-differenced single-frequency GPS/Galileo PPP solution.

part of the mathematical model. As shown in [6], the use of the exponential function improves the precision of the PPP solution by about 30%, in comparison with the sine function.

**Figure 4** shows the results of the single-frequency BSSD GPS/Galileo PPP model, when a GPS satellite is selected as a reference for both GPS and Galileo observables. As can be seen, similar to the un-differenced counterpart, a sub-decimeter level positioning accuracy is obtained. However, a reduction of about 35% in the convergence time is obtained through the BSSD model, in comparison with the un-differenced single-frequency GPS/Galileo solution.

**Figure 5** shows the results of the BSSD GPS/Galileo PPP solution when a Galileo satellite is selected as a reference for both GPS and Galileo observables. As expected, similar results to the previous scenario are obtained. This similarity is due mainly to the fact that both BSSD models use tight combination with similar relative satellite geometry and same redundancy number.

The results of the third BSSD model scenario, *i.e.*, when a GPS satellite and a Galileo satellite are selected as references for the GPS and Galileo observables, respectively, are shown in **Figure 6**. As can be seen, similar to the previous two scenarios, a sub-decimeter level positioning accuracy is obtained. However, only a 15% reduction in the convergence time is obtained, in comparison with the un-differenced model solution. This moderate improvement in the convergence time is likely attributed to the fact that the loose combination is weaker than the tight combination, as indicated above. In addition, as the ionospheric delay would not be modelled sufficiently through the GIM, a residual component remains, which would be mapped differently into the unknown parameters of the BSSD models.

**Figure 7** shows a summary of the standard deviations (STD) for the obtained station coordinates, which are extracted from the solution every 20 minutes. A solution is said to have been converged when the three-dimensional positioning standard deviation reaches 10 cm. The results of the STD show that the un-differenced GPS/Galileo solution takes approximately 100 minutes to reach the decimetre level accuracy. However, this is reduced to about 65 minutes when BSSD with one reference satellite is used. On the other hand, when BSSD with two reference satellites is used, the solution takes 85 minutes to reach the decimetre level accuracy. As

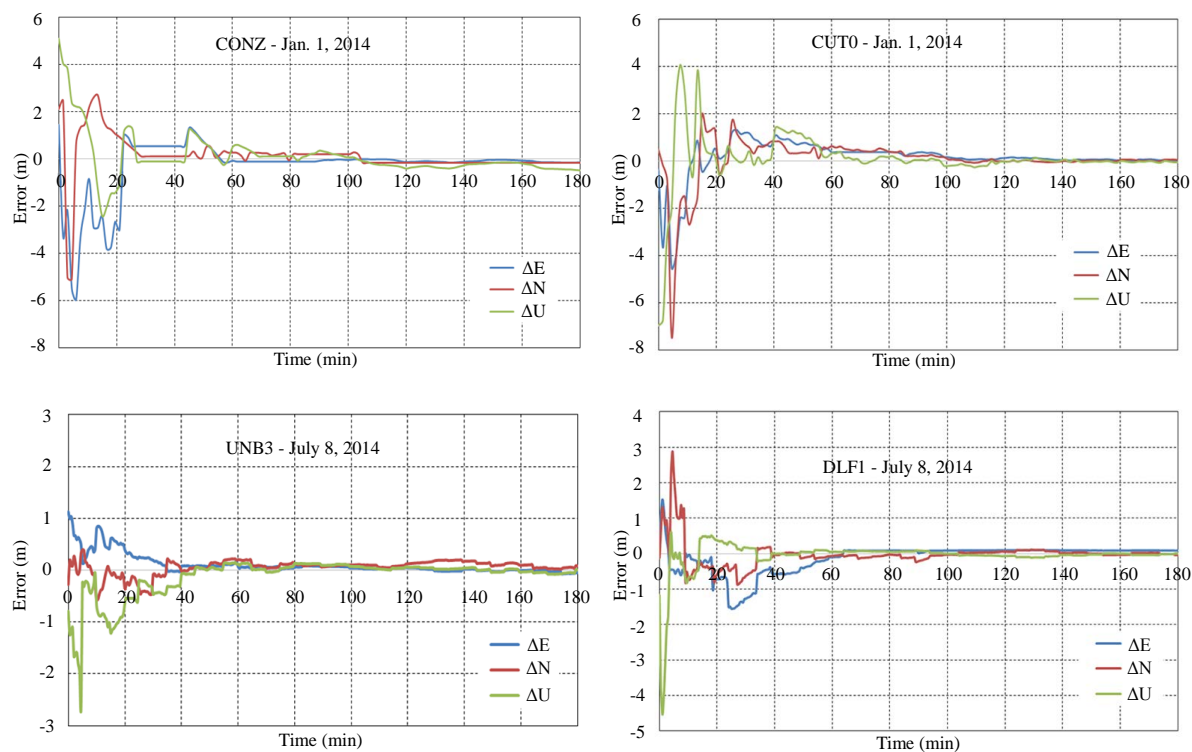


Figure 4. BSSD GPS/Galileo PPP solution using a GPS reference satellite.

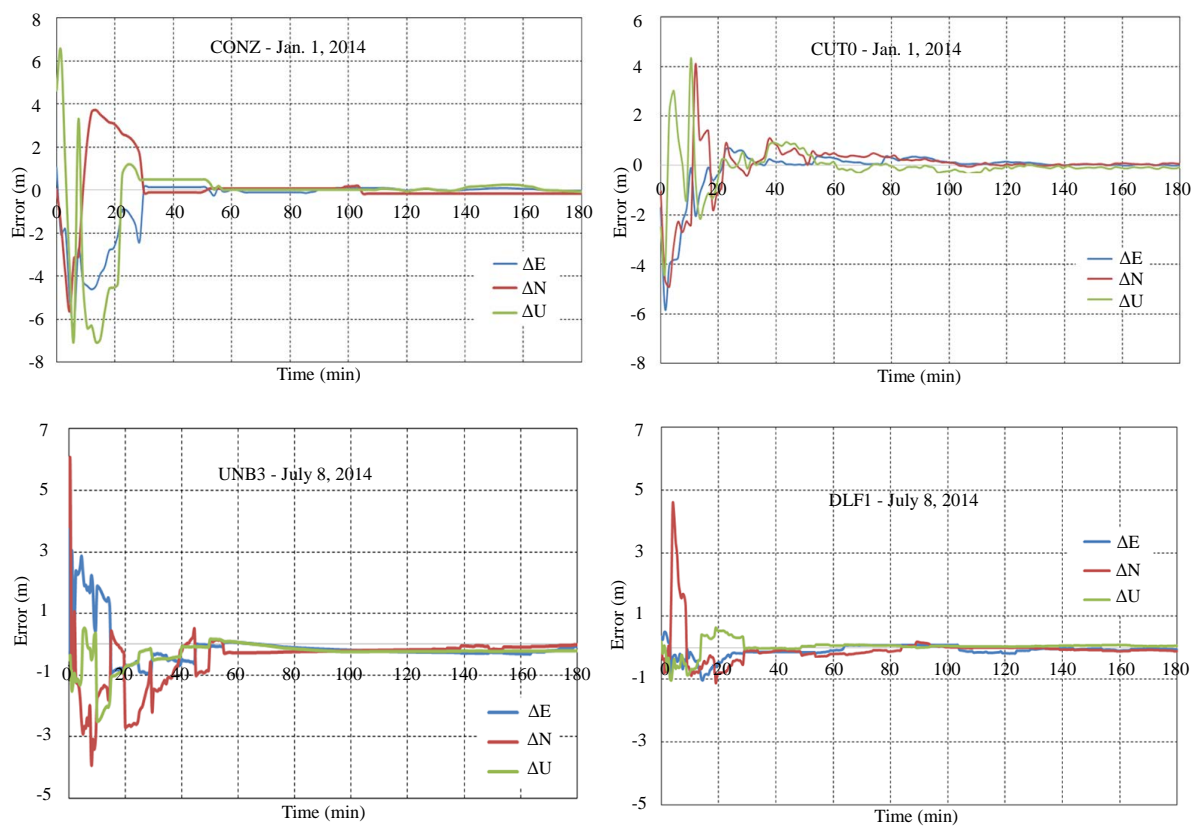


Figure 5. BSSD GPS/Galileo PPP solution using a Galileo reference satellite.

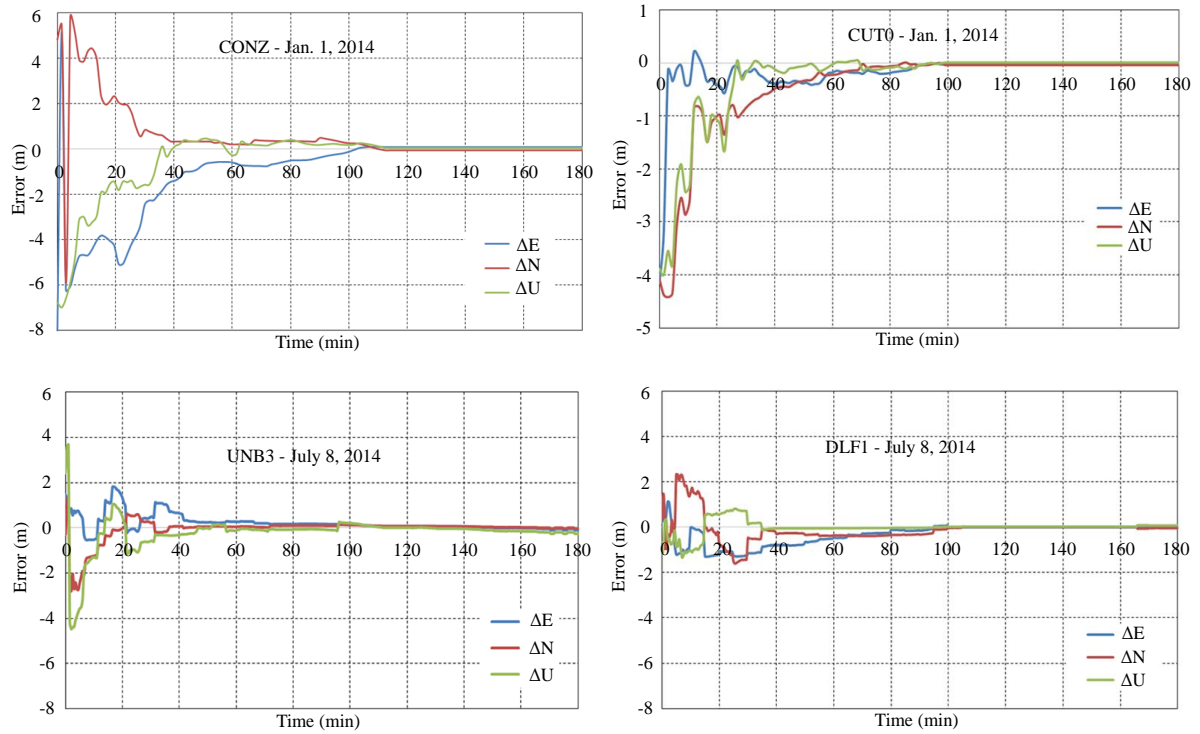


Figure 6. BSSD GPS/Galileo PPP solution using two reference satellites.

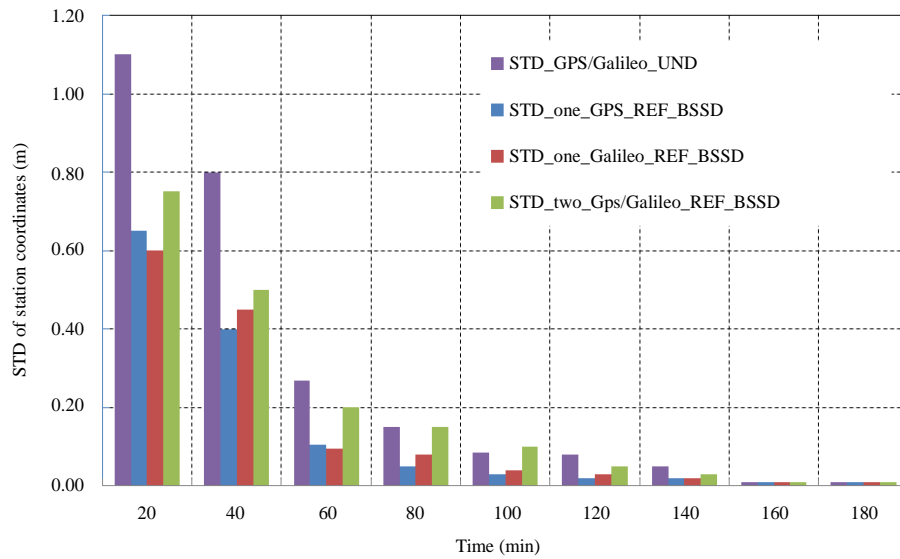
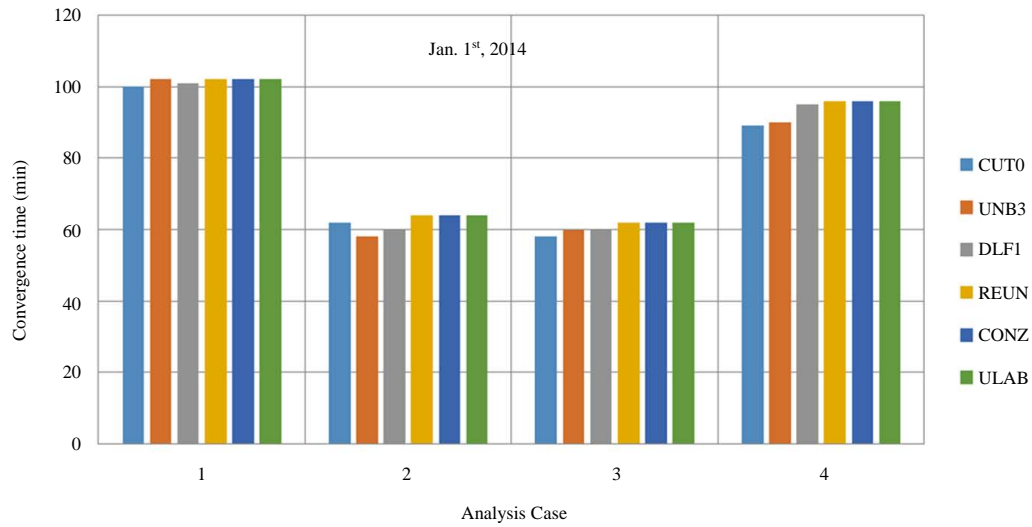


Figure 7. Summary of standard deviations of obtained station coordinates.

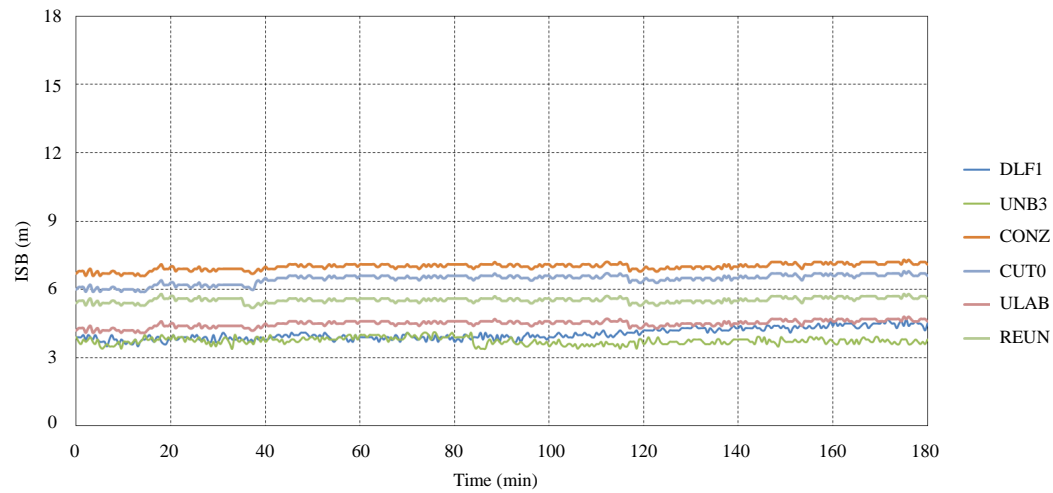
discussed above, this is likely attributed to the relatively weaker adjustment model of the loose combination.

Figure 8 summarizes the convergence times of all 24 cases considered in our analysis. As shown in Figure 9, as far as the solution convergence time is concerned, the best results are obtained when the BSSD model with one reference satellite (*i.e.*, a tight combination) is used.

The inter-system bias for the various receivers is obtained as a by-product of the PPP solution of the un-differenced and tight combination scenarios. Figure 9 summarises the results of the ISB for all stations, based on the BSSD single-frequency GPS/Galileo PPP model. The results are almost identical to those obtained through the un-differenced single-frequency GPS/Galileo PPP model.



**Figure 8.** Summary of convergence times for all data sets analysed. (1) Un-differenced model; (2) BSSD model with a GPS satellite as a reference; (3) BSSD model with a Galileo satellite as a reference; (4) BSSD model with both a GPS and a Galileo as reference satellites.



**Figure 9.** Summary of ISB results.

As shown in **Figure 9**, the values of the ISB are stable over the observation time spans. Differences of up to 3 m can be observed, which indicate that the ISB is receiver/firmware dependent.

## 6. Conclusions

A new PPP model, which combines single-frequency GPS and Galileo system observations in BSSD mode, has been introduced in this paper. Three scenarios have been considered when forming BSSD; namely a GPS satellite is selected as a reference, a Galileo satellite is selected as a reference, and two satellites, one GPS and one Galileo, are selected as references. It has been shown that a sub-decimetre level positioning accuracy can be obtained with both of the un-differenced and BSSD single-frequency GPS/Galileo PPP models. However, the PPP solution of the un-differenced model takes about 100 minutes to converge to a decimetre level positioning accuracy. The convergence time of the single-frequency GPS/Galileo PPP solution is improved by 35% and 15% when BSSDs with tight and loose combinations are used, respectively. The moderate improvement in the solution convergence time obtained with the loose combination is likely attributed to its relatively weaker adjustment model in comparison with the tight combination.

The values of the ISB have been obtained for various days and receiver types. Almost identical results have been obtained with both of the un-differenced and BSSD (tight combination) modes. It has been found that the values of the ISB are largely stable over the observation time spans. However, differences of up to 3 m have been observed, which suggest that the ISB is receiver/firmware dependent.

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## References

- [1] Zumberge, J.F., Heflin, M.B., Jefferson, D.C., Watkins, M.M. and Webb, F.H. (1997) Precise Point Processing for the Efficient and Robust Analysis of GPS Data from Large Networks. *Journal of Geophysical Research*, **102**, 5005-5017. <http://dx.doi.org/10.1029/96JB03860>
- [2] Heroux, P. and Kouba, J. (2001) GPS Precise Point Positioning Using IGS Orbit Products. *Physics and Chemistry of the Earth, Part A: Solid Earth and Geodesy*, **26**, 573-578. [http://dx.doi.org/10.1016/S1464-1895\(01\)00103-X](http://dx.doi.org/10.1016/S1464-1895(01)00103-X)
- [3] Colombo, O.L., Sutter, A.W. and Evans, A.G. (2004) Evaluation of Precise, Kinematic GPS Point Positioning. *ION GNSS 17th International Technical Meeting of the Satellite Division*, 21-24 September 2004, Long Beach.
- [4] Elsobeiey, M. and El-Rabbany, A. (2014) Efficient Between-Satellite Single-Difference Precise Point Positioning Model. *Journal of Surveying Engineering*, **140**, Article ID: 04014007. [http://dx.doi.org/10.1016/S1464-1895\(01\)00103-X](http://dx.doi.org/10.1016/S1464-1895(01)00103-X)
- [5] Hofmann-Wellenhof, B., Lichtenegger, H. and Wasle, E. (2008) GNSS Global Navigation Satellite Systems: GPS, Glonass, Galileo & More. Springer Wien, New York, 501 p.
- [6] Afifi, A. and El-Rabbany, A. (2013) Stochastic Modeling of Galileo E1 and E5a Signals. *International Journal of Engineering and Innovative Technology (IJEIT)*, **3**, 188-192.
- [7] European Space Agency (ESA) (2013) Galileo and GPS Synchronise Watches: New Time Offset Helps Working Together. [http://www.esa.int/Our\\_Activities/Navigation/Galileo\\_and\\_GPS\\_synchronise\\_watches\\_new\\_time\\_offset\\_helps\\_working\\_together](http://www.esa.int/Our_Activities/Navigation/Galileo_and_GPS_synchronise_watches_new_time_offset_helps_working_together)
- [8] Melgard, T., Tegedor, J., de Jong, K., Lapucha, D. and Lachapelle, G. (2013) Interchangeable Integration of GPS and Galileo by Using a Common System Clock in PPP. *ION GNSS+*, 16-20 September 2013, Institute of Navigation, Nashville.
- [9] Odijk, D. and Teunissen, P.J.G. (2013) Characterization of Between-Receiver GPS-Galileo Inter-System Biases and Their Effect on Mixed Ambiguity Resolution. *GPS Solutions*, **17**, 521-533. <http://dx.doi.org/10.1007/s10291-012-0298-0>
- [10] Paziewski, J. and Wielgosz, P. (2013) Assessment of GPS + Galileo and Multi-Frequency Galileo Single-EPOCH Precise Positioning with Network Corrections. *GPS Solutions*, **18**, 571-579. <http://dx.doi.org/10.1007/s10291-013-0355-3>
- [11] Montenbruck, O., Steigenberger, P., Khachikyan, R., Weber, G., Langley, R.B., Mervart, L. and Hugentobler, U. (2014) IGS-MGEX: Preparing the Ground for Multi-Constellation GNSS Science. *Inside GNSS*, **9**, 42-49.
- [12] Schaer, S., Gurtner, W. and Feltens, J. (1998) IONEX: The IONosphere Map Exchange Format Version 1. <http://igscb.jpl.nasa.gov/igscb/data/format/ionex1.pdf>
- [13] Kouba, J. (2009) A Guide to Using International GNSS Service (IGS) Products. <http://igscb.jpl.nasa.gov/igscb/resource/pubs/UsingIGSProductsVer21.pdf>
- [14] Paziewski, J. and Wielgosz, P. (2014) Accounting for Galileo-GPS Inter-System Biases in Precise Satellite Positioning. *Journal of Geodesy*, **89**, 81-93. <http://dx.doi.org/10.1007/s00190-014-0763-3>
- [15] El-Rabbany, A. (2006) Introduction to GPS: The Global Positioning System. 2nd Edition, Artech House Inc., Norwood, 160 p.
- [16] Steigenberger, P., Hugentobler, U., Loyer, S., Perosanz, F., Prange, L., Dach, R., Uhlemann, M., Gendt, G. and Montenbruck, O. (2014) Galileo Orbit and Clock Quality of the IGS Multi-GNSS Experiment. *Advances in Space Research*, **55**, 269-281. <http://dx.doi.org/10.1016/j.asr.2014.06.030>
- [17] Afifi, A. and El-Rabbany, A. (2015) An Innovative Dual Frequency PPP Model for Combined GPS/Galileo Observations. *Journal of Applied Geodesy*, **9**, 27-34. <http://dx.doi.org/10.1515/jag-2014-0009>
- [18] Klobuchar, J.A. (1991) Ionospheric Effects on GPS. *GPS World*, **2**, 48-51.



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- [19] Chen, K. and Gao, Y. (2005) Real-Time Precise Point Positioning Using Single Frequency Data. *Proceedings of the 18th International Technical Meeting of the Satellite Division of the Institute of Navigation, ION GNSS 2005*, Long Beach, 13-16 September 2005, 1514-1523.
- [20] Abd El-Rahman, M.A. and El-Rabbany, A. (2013) Performance Evaluation of USTEC Product for Single-Frequency Precise Point Positioning. *Geomatica*, **67**, 253-257. <http://dx.doi.org/10.5623/cig2013-049>
- [21] Hopfield, H.S. (1972) Tropospheric Refraction Effects on Satellite Range Measurements. *APL Technical Digest*, **11**, 11-19.
- [22] Boehm, J. and Schuh, H. (2004) Vienna Mapping Functions in VLBI Analyses. *Geophysical Research Letters*, **31**, Article ID: L01603. <http://dx.doi.org/10.1029/2003GL018984>
- [23] Bos, M.S. and Scherneck, H.-G. (2011) Ocean Tide Loading Provider. <http://holt.oso.chalmers.se/loading/>
- [24] IERS (2010) International Earth Rotation and Reference System Services Conventions. IERS Technical Note 36. <http://www.iers.org/ IERS/EN/Publications/TechnicalNotes/tn36.html/>
- [25] Leick, A. (2004) GPS Satellite Surveying. 3rd Edition, John Wiley and Sons, Hoboken.
- [26] Wu, J.T., Wu, S.C., Hajj, G.A., Bertiger, W.I. and Lichten, S.M. (1993) Effects of Antenna Orientation on GPS Carrier Phase. *Manuscripta Geodetica*, **18**, 91-98.
- [27] Kaplan, E. and Hegarty, C. (2006) Understanding GPS Principles and Applications. 2nd Edition, Artech House Inc., Norwood, 683 p.
- [28] Dow, J.M., Neilan, R.E. and Rizos, C. (2009) The International GNSS Service in a Changing Landscape of Global Navigation Satellite Systems. *Journal of Geodesy*, **83**, 191-198. <http://dx.doi.org/10.1007/s00190-008-0300-3>
- [29] Vanicek, P. and Krakiwsky, E.J. (1986) Geodesy: The Concepts. 2nd Edition, North-Holland, Amsterdam.