

Vertically-Suspended Environmental Enrichment Alters the Velocity Profiles of Circular Fish Rearing Tanks

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Abstract

The inclusion of vertically-suspended environmental enrichment in circular tanks has produced substantial benefits during fish rearing. This study examined the tank water velocity profiles of four different vertically-suspended structures (rod array, extended rod array, single angle array, double angle array) and a control (no environmental enrichment) at two incoming water velocities (18.3 cm/s and 54.9 cm/s) in 1.8-m diameter circular tanks. At both of the incoming water velocities, overall water velocities throughout the tank were significantly reduced with the addition of any environmental enrichment in comparison to the control. In addition, the overall water velocities in the double angle array were significantly lower than the other three enrichment treatments. The pattern of significant reductions in velocity with the use of any environmental enrichment, with further significant velocity reductions in the double angle treatment, was repeated when the data were combined for each sampling depth, radius from the center, and degree (circular arc). Although considerable variation in water velocity was observed at each specific sampling location with both incoming velocities, significantly lower velocities were observed at nearly every sampling location with the addition of any environmental enrichment to the circular tank. In addition, the double angle array consistently produced the lowest velocities among the environmental enrichment treatments. The changes in velocity profiles from vertically-suspended environmental enrichment may be at least partially-responsible for the frequently-observed improvements in fish growth.

Keywords

Environmental Enrichment, Vertically-Suspended Structure, Circular Tank, Water Velocity

1. Introduction

The ideal fish rearing tank would have uniform water quality, be self-cleaning, provide water velocity for fish exercise, and efficiently use the available floor plan. It is also important that all of the fish in the tank contact flowing water [1]. Circular tanks excel at homogeneously distributing dissolved oxygen, and eliminating biosolids [2] [3] [4], as well as providing adequate velocity for exercise [5] [6] [7] [8]. However, they cannot share tank sidewalls, precluding optimum space management [9]. Despite these floor plan limitations, circular tanks are commonly used in production aquaculture [10].

Water typically enters a circular tank through a tangential inlet, such as a spray bar, and exits through a screened central bottom outlet [4]. Compared to angular tanks, circular tanks have higher velocities and more stable flow patterns, resulting in self-cleaning and improved water quality benefits [2] [4] [11]. Several studies have generally described flow patterns in circular tanks [1] [2] [4] [12] [13] [14]. Circular tank velocity profiles are primarily affected by the size of the tank, the geometry of the water inlet structure, the number and location of outlet structures, the number and size of fish in the tank, and the flow and velocity of the incoming water [4] [9] [12] [13] [14]. Flow patterns are also significantly affected by the addition of environmental enrichment structures to the tanks [10].

Environmental enrichment is the placement of material or structure within otherwise-sterile hatchery rearing units to try and imitate the natural environment [15]. Some enrichment techniques include placing woody or stony debris, plant or root material, plastic plants, or concrete blocks directly into the rearing tank [16]-[23]. However, placing structures within a circular tank can be problematic because they can interfere with hydraulic self-cleaning, increasing labor requirements and the risk of disease from trapped food and feces [2] [4] [12] [23] [24] [25] [26]. In order to avert these hazards, an environmental enrichment technique using vertically-suspended aluminum rods that did not affect the hydraulic self-cleaning of circular tanks was created [27]. These vertically-suspended structures were shown to significantly improve rainbow trout (*Oncorhynchus mykiss*) rearing performance [27]. Subsequent investigations evaluating various types of vertically-suspended structures, including strings of spheres, plastic pipes, and aluminum angles, have also indicated positive effects during the rearing of multiple salmonid species [28] [29] [30] [31].

Little research has been published describing the flow profile of a circular tank with vertically-suspended environmental enrichment. The lone published study used only one type of suspended structure (a small aluminum rod array), and two different incoming water flow rates, but did not describe the actual water velocities [10]. Given that incoming water velocities influence circular tank flow patterns [4], and the positive effects observed when using velocity manipulation to exercise fish during hatchery rearing [5] [6] [7] [8] [32] [33] [34], there is a need to evaluate the flow dynamics of circular tanks containing suspended

enrichment at different incoming water velocities. In addition, there is a need to describe the impacts of circular tank flow patterns for a variety of suspended structures beyond just the small array used previously [10]. As such, the objective of this study was to describe the flow patterns of circular tanks containing a number of different vertically-suspended enrichment structures at two different water velocities.

2. Materials and Methods

All measurements were recorded in a 1.82-m diameter and 0.8-m deep fiberglass circular tank fitted with a central drain and a spray bar at McNenny State Fish Hatchery, rural Spearfish, South Dakota, USA and filled with water to a depth of 0.585 m (**Figure 1**). The incoming flow rate of water through the spray bar was set at 22 L/min throughout the experiment. Water entered from the spray bar, rotated in a counterclockwise direction, and exited the tank via the drain screen. The spray bar was adjusted to create two water velocities, 18.3 cm/s and 54.9 cm/s. Velocity measurements were taken with a FP111 Flow Probe (Global Water Instrumentation, College Station, Texas, USA).

In addition to the two velocities, four types of environmental enrichment (rod array, extended rod array, single angle array, double angle array), along with a control scenario with no enrichment, were included in this study. The structures used are described in **Table 1** and illustrated in **Figure 2(a)-(d)**. The rods were made of aluminum (1.0 cm diameter, 57.2 cm length) as were the angles (2.5 cm width on each side, 55.9 cm long). The rods or angles were inserted into rectangles of corrugated plastic suspended above the surface of the water. **Figure 3(a)-(c)** shows close-up views of the rod or angle arrays used, while **Figure 4(a)** & **Figure 4(b)** show individual angle dimensions.

The locations of the velocity measurements were determined by imposing a grid system across the top of the tank, forming equal quadrants. Each radial

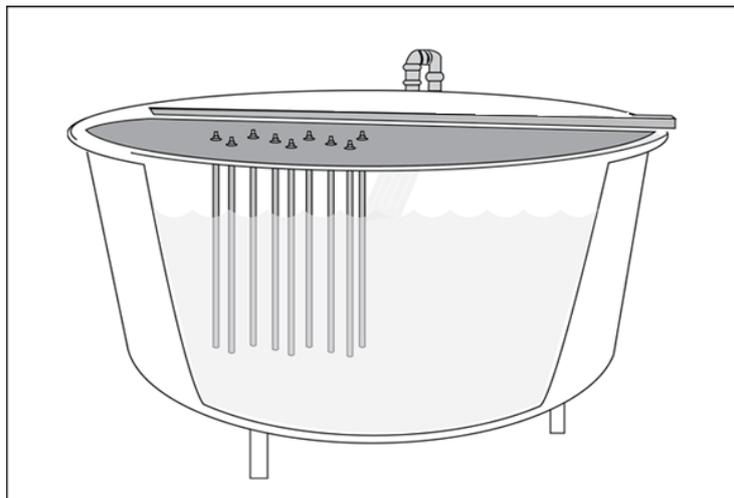
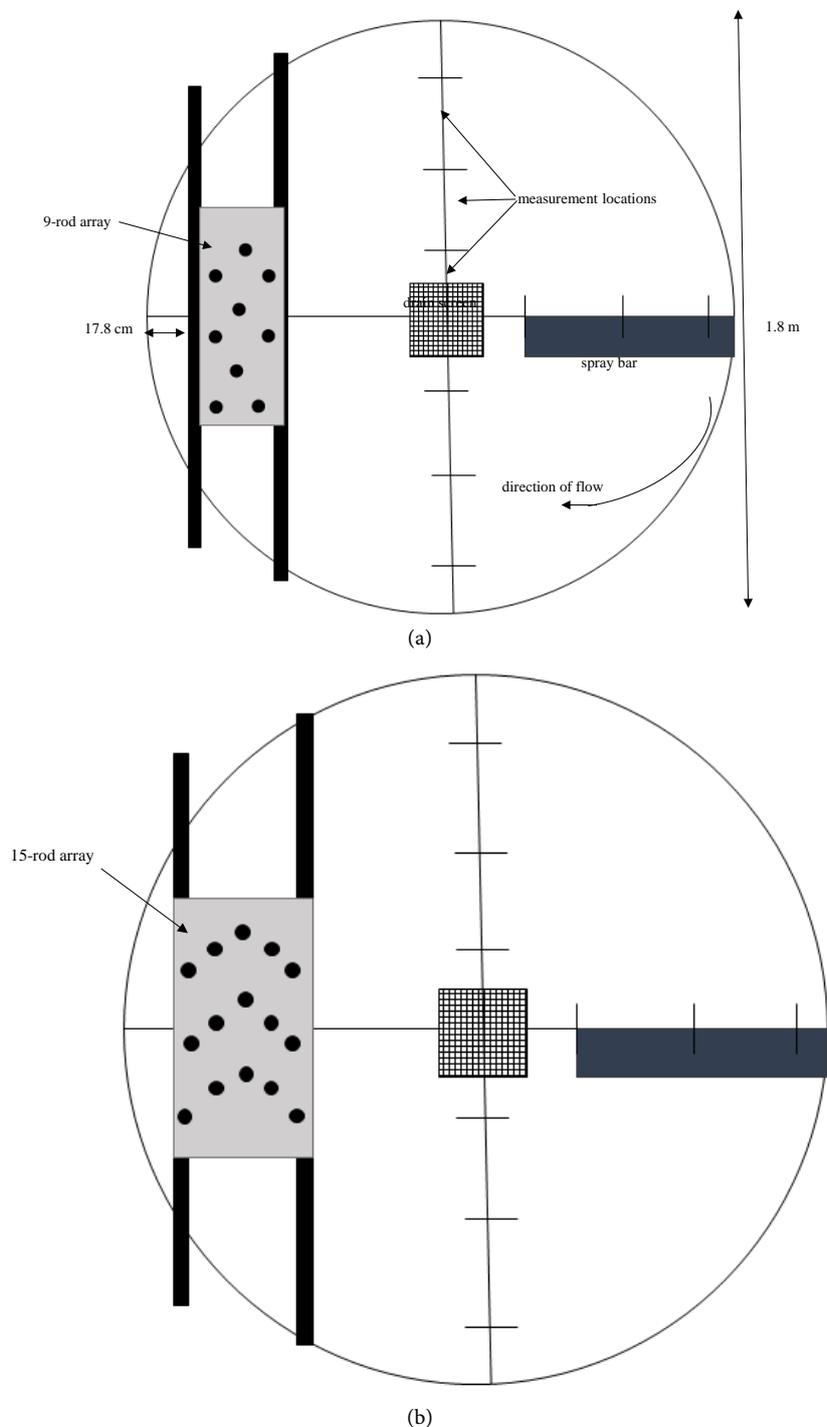


Figure 1. Schematic of circular tank, shown with nine vertical rods suspended from a tank cover.

Table 1. Environmental enrichment structures used during an evaluation of flow dynamics in a 1.8-meter diameter circular tank.

Structure	Description	Source	Figure
Rod array	Nine rods equally spaced in a 27.3 cm by 47.0 cm rectangle.	Kientz and Barnes 2016	3(a)
Extended rod array	Fifteen rods evenly spaced in a 43.2 cm by 54.6 cm rectangle.	Barnes, pers. comm.	3(b)
Single angle array	Four angles evenly spaced in a 40.6 cm by 32.4 cm rectangle.	Krebs <i>et al.</i> 2018	3(c)
Double angle array	Two aluminum angle arrays (described previously).	Krebs <i>et al.</i> 2018	3(c), 5



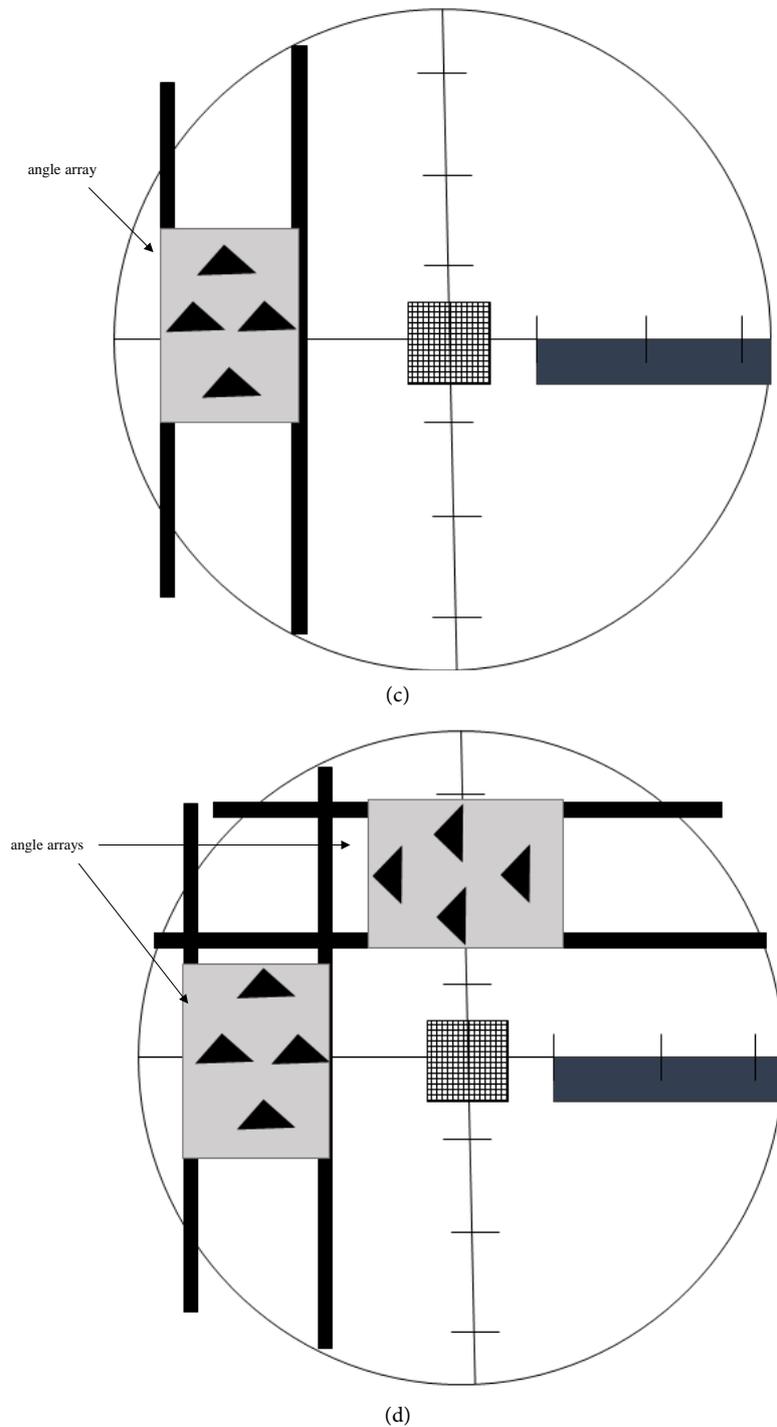


Figure 2. Experimental tanks with separate structure treatments, rod array (a), extended rod array (b), single angle array (c), double angle array (d).

length was labeled as an axis of 0° , 90° , 180° or 270° . The spray bar was directly in front of the 0° axis, and the structure was placed on the 180° axis, on which no measurements were made. Each axis except for 180° was split into three lengths of 30, 60, and 90 cm from the central intersection of the strings. At each of these radii along the 0° , 90° , and 270° axes, three measurements were taken at

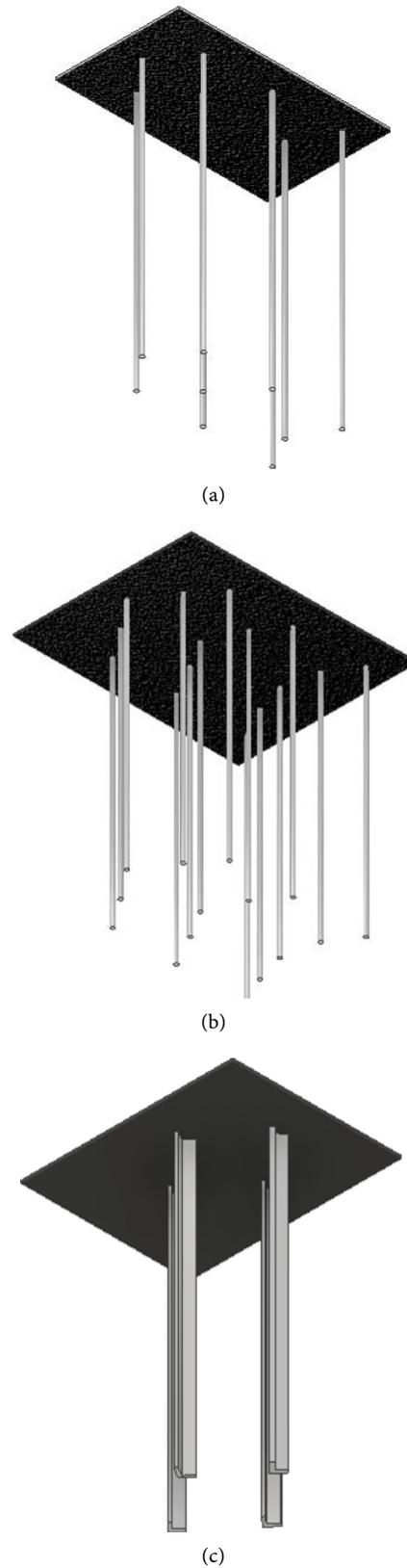


Figure 3. Diagrams of structures used in the tank with corrugated plastic tops. Structure (a) is the rod array (27.30 cm by 46.96 cm), (b) is the extended rod array (43.18 cm by 54.61 cm), and (c) is the angle array (40.64 cm by 32.39 cm).

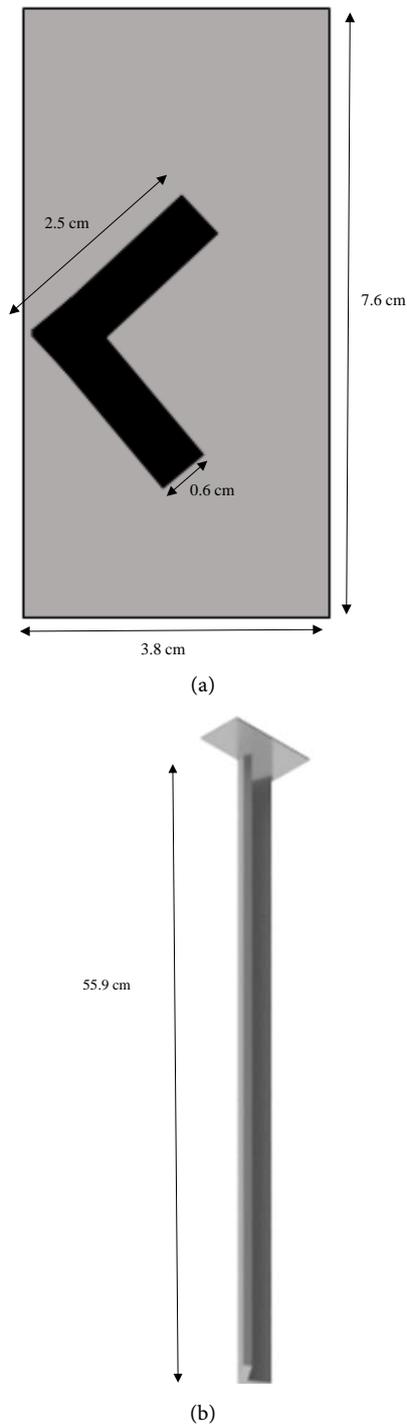


Figure 4. Close-up views of a single angle with dimensions. (a) bottom view of individual angle; (b) full view of angle structure

different depths from the surface: 10 cm, 30.5 cm, and 51.8 cm, as shown in **Figure 5**. Three replicate measurements were recorded at each location.

Data were initially analyzed by analysis of variance and covariance using the SPSS (9.0) statistical analysis program (SPSS, Chicago, Illinois, USA). Because of the large number of interactions, subsequent analysis used one-way analysis of

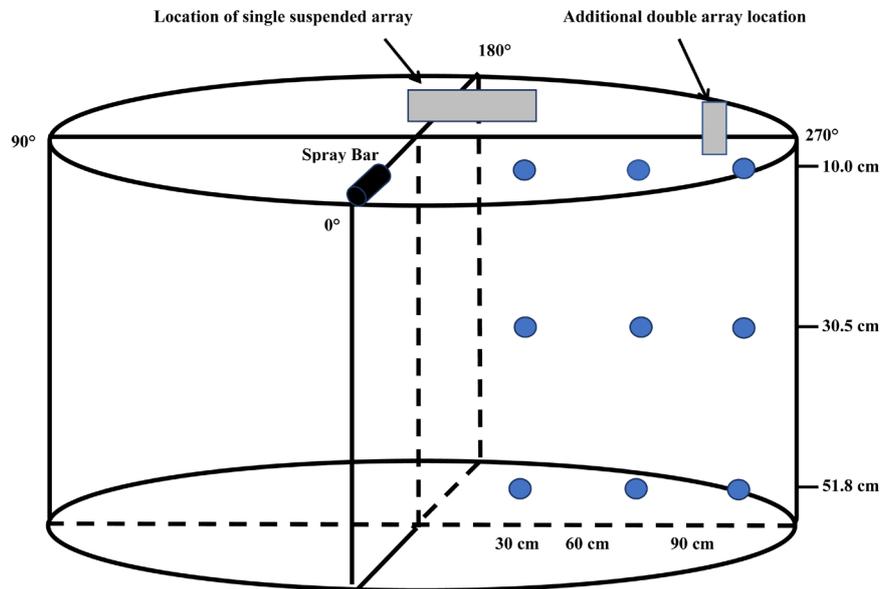


Figure 5. Diagram of a circular tank showing the location of the spray bar and sampling locations for one section (indicated by the blue circles).

variance and t-tests to examine just the effects of suspended arrays at each incoming water velocity. Tukey's mean comparison procedure was used for post-hoc analysis. The significance level for all tests was predetermined at $P < 0.05$.

3. Results

At both of the incoming water velocities (18.3 cm/s and 54.9 cm/s), overall water velocities throughout the tank were significantly reduced with the addition of any form of environmental enrichment in comparison to the control tanks devoid of structure (Table 2). In addition, the double angle enrichment treatment overall water velocities were significantly lower than the other three enrichment treatments. The lowest record velocity values of 1.0 cm/s were observed in the extended rod and double angle enrichment treatments at an incoming velocity of 18.3 cm/s. The lowest recorded velocities at an incoming velocity of 54.9 cm/s were 3.0 cm/s in the extended rod and double angle treatments.

At both incoming velocities, water velocities at all depths were highest in the control treatment, with significant reductions in water velocities at all depths observed in the environmental enrichment treatments (Table 3). While there was considerable overlap, in general the lowest velocity readings at each depth were recorded in the double angle treatment. The pattern of significant reductions in velocity with the use of any environmental enrichment, with further significant reductions in the double angle treatment, was repeated when the data was combined for each radius (Table 4) and for each degree sampling location (Table 5).

Considerable variation in water velocity was observed at each specific sampling location in both the lower incoming velocity of 18.3 cm/s (Table 6) and the higher incoming velocity of 54.9 cm/s (Table 7). Despite this variation,

Table 2. Mean (SE), minimum, and maximum water velocities (cm/s) from multiple sampling points within circular tanks containing different suspended environmental enrichment structures at two different incoming water velocities (means within each incoming velocity with different letters are significantly different, $P < 0.05$).

Incoming Velocity	Structure	N	Tank Velocity		
			Overall	Minimum	Maximum
18.3 cm/s	None	81	21.6 (0.8) z	3.0	36.6
	Rod	81	15.1 (0.6) x	3.0	24.4
	Extended rod	81	13.4 (0.6) x	0.0	24.4
	Single angle	81	12.7 (0.6) x	0.0	24.4
	Double angle	63	8.9 (0.6) y	0.0	21.3
$F_{(4,382)} = 49.971; P = 0.001$					
54.9 cm/s	None	81	44.5 (1.2) z	18.3	67.1
	Rod	81	29.7 (0.8) y	12.2	42.7
	Extended rod	81	25.4 (0.8) x	3.0	39.6
	Single angle	81	25.4 (0.9) x	6.1	36.6
	Double angle	63	17.5 (0.6) w	3.0	30.5
$F_{(4,382)} = 120.343; P = 0.001$					

Table 3. Mean (SE) water velocities (cm/s) at three depths within circular tanks containing different suspended environmental enrichment structures at two different incoming water velocities ($N = 27$ except for Double Angle where $N = 24$; means within each incoming velocity in a row with different letters are significantly different, $P < 0.05$).

Incoming Velocity	Depth	Structure					$F_{(4,124)}$	P
		None	Rod	Extended Rod	Single Angle	Double Angle		
18.9 cm/s	Surface	21.4 (1.3) z	16.0 (1.2) y	14.6 (1.0) y	14.3 (1.0) y	8.7 (0.9) x	15.105	0.001
	Middle	22.4 (1.3) z	15.5 (0.8) y	14.4 (0.9) y	13.3 (0.7) yx	10.0 (1.1) x	20.677	0.001
	Bottom	21.0 (1.4) z	13.7 (1.1) y	11.1 (1.1) yx	10.4 (1.2) yx	7.8 (1.1) x	17.267	0.001
54.9 cm/s	Surface	46.1 (2.1) z	33.1 (1.1) y	26.5 (1.3) x	27.5 (1.4) yx	19.0 (1.0) w	44.280	0.001
	Middle	44.9 (2.3) z	30.7 (1.0) y	27.3 (0.9) y	26.9 (0.8) y	18.7 (0.6) x	50.690	0.001
	Bottom	42.4 (1.6) z	25.4 (1.4) y	22.4 (1.8) yx	21.8 (1.8) yx	14.8 (1.6) x	37.792	0.001

Table 4. Mean (SE) water velocities (cm/s) at three radial locations within circular tanks containing different suspended environmental enrichment structures at two different incoming water velocities ($N = 27$ except for Double Angle at radius = 60 and 90 where $N = 18$; means within each incoming velocity in a row with different letters are significantly different, $P < 0.05$).

Incoming Velocity	Radius	Structure					F	P
		None	Rod	Extended Rod	Single Angle	Double Angle		
18.9 cm/s	30	15.5 (1.2) z	10.8 (0.7) y	9.1 (0.9) yx	9.4 (1.0) yx	6.2 (0.9) x	12.997	0.001
	60	28.2 (0.6) z	16.8 (0.9) y	14.8 (0.9) y	13.8 (0.9) y	8.6 (0.9) x	64.895	0.001
	90	21.1 (0.7) z	17.5 (0.9) y	16.1 (0.9) yx	14.9 (0.9) yx	13.0 (0.7) x	11.582	0.001
54.9 cm/s	30	52.8 (2.0) z	26.4 (1.3) y	21.1 (1.3) x	22.7 (1.4) x	17.7 (1.0) wx	96.558	0.001
	60	47.0 (0.5) z	32.4 (1.2) y	28.1 (1.4) yx	25.9 (1.6) x	16.6 (1.7) w	67.898	0.001
	90	33.7 (1.0) z	30.4 (1.3) zy	27.0 (1.2) y	27.7 (1.3) y	18.1 (1.2) x	19.223	0.001

Table 5. Mean (SE) water velocities (cm/s) at three degree locations within circular tanks containing different suspended environmental enrichment structures at two different incoming water velocities (N = 27 except for Double Angle at 270 where N = 9; means within each incoming velocity in a row with different letters are significantly different, P < 0.05).

Incoming Velocity	Degree	Structure					F	P
		None	Rod	Extended Rod	Single Angle	Double Angle		
18.9 cm/s	0°	21.7 (1.0) z	15.8 (1.0) y	14.2 (0.6) y	13.5 (1.0) yx	10.2 (0.7) x	22.345	0.001
	90°	20.2 (1.5) z	13.3 (1.2) y	11.0 (1.4) y	11.1 (1.3) y	8.4 (1.2) y	11.491	0.001
	270°	22.9 (1.4) z	16.0 (0.8) y	14.9 (0.8) y	13.4 (0.8) y	6.4 (0.8) x	24.002	0.001
54.9 cm/s	0°	45.8 (2.0) z	31.2 (1.2) y	26.4 (0.9) y	27.4 (0.6) y	18.6 (1.0) x	67.800	0.001
	90°	40.5 (2.0) z	25.7 (1.3) y	21.9 (1.7) yx	21.4 (1.8) yx	16.1 (1.2) x	31.844	0.001
	270°	47.1 (2.0) z	32.3 (1.2) y	27.9 (1.2) y	27.3 (1.5) y	18.2 (1.4) x	38.039	0.001

Table 6. Mean (SE) water velocities (cm/s) at multiple locations within circular tanks containing different suspended environmental enrichment structures at an incoming water velocity of 18.3 cm/s (means in a row with different letters are significantly different, N = 3; P < 0.05).

Depth	Measurement Location		Structure					F	P	
	Axis	Radii (cm)	None	Rod	Extended Rod	Single Angle	Double Angle			
Surface	0°	30	16.3 (2.0) z	15.2 (1.8) z	14.2 (1.0) z	15.2 (0.0) z	14.2 (1.0) z	0.389	0.812	
		60	24.4 (0.0) z	24.4 (0.0) z	17.3 (1.0) y	19.3 (1.0) y	7.1 (1.0) x	81.167	0.001	
		90	18.3 (0.0) z	18.3 (0.0) z	15.2 (0.0) y	18.3 (0.0) z	11.2 (1.0) x	47.500	0.001	
	90°	30	10.2 (2.0) z	8.1 (2.7) z	7.1 (1.0) z	7.1 (2.7) z	3.0 (1.8) z	1.477	0.280	
		60	33.5 (1.8) z	9.1 (0.0) y	6.1 (1.8) y	8.1 (2.0) y	6.1 (1.8) y	51.654	0.001	
		90	18.3 (0.0) z	24.4 (0.0) y	23.4 (1.0) y	21.3 (1.8) zy	12.2 (0.0) x	29.125	0.001	
	270°	30	22.4 (2.0) z	10.2 (1.0) yx	12.2 (0.0) yx	14.2 (1.0) y	7.1 (1.0) x	22.857	0.001	
		60	28.4 (1.0) z	18.3 (0.0) y	19.3 (1.0) y	16.3 (1.0) y	-	37.667	0.001	
		90	21.3 (0.0) z	16.3 (1.0) z	16.3 (1.0) z	9.1 (1.8) y	-	19.467	0.001	
	Middle	0°	30	21.3 (1.8) z	10.2 (2.0) y	13.2 (2.0) y	9.1 (3.0) y	10.2 (1.0) y	5.786	0.011
			60	28.4 (1.0) z	17.3 (1.0) y	15.2 (1.8) y	15.2 (1.8) y	9.1 (0.0) x	30.125	0.001
			90	24.4 (0.0) z	20.3 (1.0) zy	17.3 (1.0) yx	17.3 (1.0) yx	14.2 (1.0) x	17.875	0.001
90°		30	10.2 (1.0) z	10.2 (1.0) z	5.1 (1.0) yx	7.1 (1.0) z	1.0 (1.0) x	14.300	0.001	
		60	30.5 (0.0) z	18.3 (0.0) y	18.3 (1.8) y	15.2 (0.0) y	9.1 (0.0) x	97.505	0.001	
		90	15.2 (0.0) zx	11.2 (1.0) y	14.2 (1.0) yx	11.2 (1.0) y	18.3 (0.0) z	14.500	0.001	
270°		30	20.3 (2.0) z	16.3 (1.0) zy	11.2 (2.0) yx	14.2 (1.0) zyx	8.1 (1.0) x	9.636	0.002	
		60	29.5 (1.0) z	16.3 (1.0) y	18.3 (0.0) y	15.2 (0.0) y	-	83.333	0.001	
		90	21.3 (1.8) z	19.3 (1.0) z	17.3 (1.0) z	15.2 (0.0) z	-	5.333	0.026	
Bottom		0°	30	12.2 (1.8) z	10.2 (1.0) z	10.2 (1.0) z	6.1 (3.5) z	7.1 (2.7) z	1.250	0.351
			60	24.4 (0.0) z	9.1 (0.0) y	9.1 (0.0) y	7.1 (1.0) yx	5.1 (1.0) x	143.000	0.001
			90	25.4 (1.0) z	17.3 (1.0) y	16.3 (1.0) y	14.2 (1.0) y	13.2 (1.0) y	22.500	0.001
	90°	30	19.3 (1.0) z	8.1 (1.0) y	1.0 (1.0) x	2.0 (2.0) x	1.0 (1.0) x	37.313	0.001	
		60	24.4 (0.0) z	21.3 (0.0) y	17.3 (1.0) xw	19.3 (1.0) yx	15.2 (0.0) w	30.500	0.001	
		90	20.3 (1.0) z	9.1 (1.8) y	6.1 (1.8) y	8.1 (2.0) y	9.1 (0.0) y	13.773	0.001	
	270°	30	7.1 (2.7) z	9.1 (1.8) z	8.1 (1.0) z	9.1 (1.8) z	4.1 (1.0) z	1.433	0.293	
		60	30.5 (0.0) z	17.3 (1.0) y	12.2 (1.8) yx	8.1 (1.0) x	-	73.267	0.001	
		90	25.4 (1.0) z	21.3 (1.8) zy	19.3 (1.0) y	19.3 (1.0) y	-	5.333	0.026	

Table 7. Mean (SE) water velocities (cm/s) at multiple locations within circular tanks containing different suspended environmental enrichment structures at an incoming water velocity of 54.9 cm/s (means in a row with different letters are significantly different, N = 3; P < 0.05).

Depth	Measurement Location		Structure						F	P
	Axis	Radii (cm)	None	Rod	Extended Rod	Single Angle	Double Angle			
Surface	0°	30	58.9 (1.0) z	30.5 (3.5) y	21.3 (3.0) y	26.4 (1.0) y	21.3 (0.0) y	51.891	0.001	
		60	48.8 (0.0) z	39.6 (1.8) y	30.5 (3.5) x	30.5 (0.0) x	19.3 (1.0) w	37.094	0.001	
		90	33.5 (0.0) z	34.5 (1.0) z	28.4 (1.0) y	28.4 (1.0) y	26.4 (1.0) y	15.250	0.001	
	90°	30	50.8 (1.0) z	22.4 (1.0) y	19.3 (1.0) y	19.3 (2.0) y	17.3 (1.0) y	120.188	0.001	
		60	9.0 (2.0) z	33.5 (0.0) y	18.3 (1.8) x	13.2 (1.0) xw	9.1 (0.0) w	155.000	0.001	
		90	27.4 (1.8) z	29.5 (1.0) y	29.5 (1.0) y	35.6 (1.0) z	18.3 (0.0) x	31.500	0.001	
	270°	30	61.0 (0.0) z	37.6 (2.0) y	27.4 (1.8) xw	32.5 (2.0)yx	21.3 (1.8) w	80.107	0.000	
		60	48.8 (0.0) z	39.6 (1.8) y	38.6 (1.0) y	35.6 (1.8) y	-	25.067	0.001	
		90	37.6 (1.0) z	30.5 (0.0) y	25.4 (1.0) x	26.4 (1.0) x	-	39.556	0.000	
	Middle	0°	30	63.0 (1.0) z	25.4 (1.0) yx	25.4 (2.0) yx	30.5 (0.0) y	21.3 (0.0) x	233.583	0.001
			60	46.7 (1.0) z	34.5 (4.1) y	29.5 (1.0) y	27.4 (1.8) y	16.3 (1.0) x	27.114	0.001
			90	35.6 (1.0) z	33.5 (1.8) zy	31.5 (1.0) zy	28.4 (1.0) y	20.3 (1.0) x	24.500	0.001
90°		30	46.7 (4.4) z	25.4 (1.0) y	23.4 (2.7) y	23.4 (1.0) y	18.3 (1.8) y	19.724	0.001	
		60	47.8 (1.0) z	31.5 (2.7) y	30.5 (0.0) y	26.4 (1.0) y	18.3 (1.8) x	46.792	0.001	
		90	23.4 (2.7) z	23.4 (2.7) z	18.3 (1.8) z	20.3 (2.7) z	17.3 (1.0) z	1.594	0.264	
270°		30	58.9 (2.0) z	32.5 (1.0) y	27.4 (0.0) yx	24.4 (0.0) xw	19.3 (2.7) w	97.292	0.001	
		60	45.7 (0.0) z	33.5 (1.8) y	29.5 (1.0) y	29.5 (2.0) y	-	28.677	0.001	
		90	36.6 (0.0) z	36.6 (0.0) z	30.5 (0.0) y	31.5 (1.0) y	-	41.000	0.001	
Bottom		0°	30	42.7 (5.3) z	25.4 (3.7) y	20.3 (1.0) y	22.4 (2.0) y	19.3 (1.0) y	9.707	0.002
			60	44.7 (1.0) z	23.4 (2.0) y	22.4 (1.0) y	24.4 (0.0) y	8.1 (1.8) x	118.000	0.001
			90	38.6 (1.0) z	33.5 (3.0) zy	28.4 (1.0) y	28.4 (1.0) y	15.2 (0.0) x	30.542	0.001
	90°	30	40.6 (7.3) z	17.3 (3.7) y	6.1 (1.8) y	7.1 (1.0) y	7.1 (2.7) y	13.770	0.001	
		60	45.7 (3.5) z	31.5 (1.0) y	35.6 (1.0) y	33.5 (1.8) y	28.4 (1.0) y	11.611	0.001	
		90	34.5 (1.0) z	17.3 (2.0) y	16.3 (1.0) y	14.2 (1.0) y	11.2 (2.0) y	36.955	0.001	
270°	30	52.8 (8.9) z	21.3 (3.0) y	19.3 (1.0) y	18.3 (0.0) y	14.2 (1.0) y	13.661	0.001		
	60	46.7 (2.0) z	24.4 (1.8) y	18.3 (1.8) y	12.2 (1.8) x	-	67.692	0.001		
	90	35.6 (1.0) z	34.5 (1.0) z	34.5 (1.0) z	35.6 (1.0) z	-	0.333	0.802		

significantly lower velocities were observed at nearly every sampling location with the addition of any environmental enrichment to the circular tank, as indicated in the cross-sectional velocity profiles shown in **Figures 6-11**. The double angle array consistently produced the lowest velocities among the environmental enrichment treatments at each incoming velocity, except at 30 cm radii on the surface and middle depths. In addition, the velocities among the enrichment

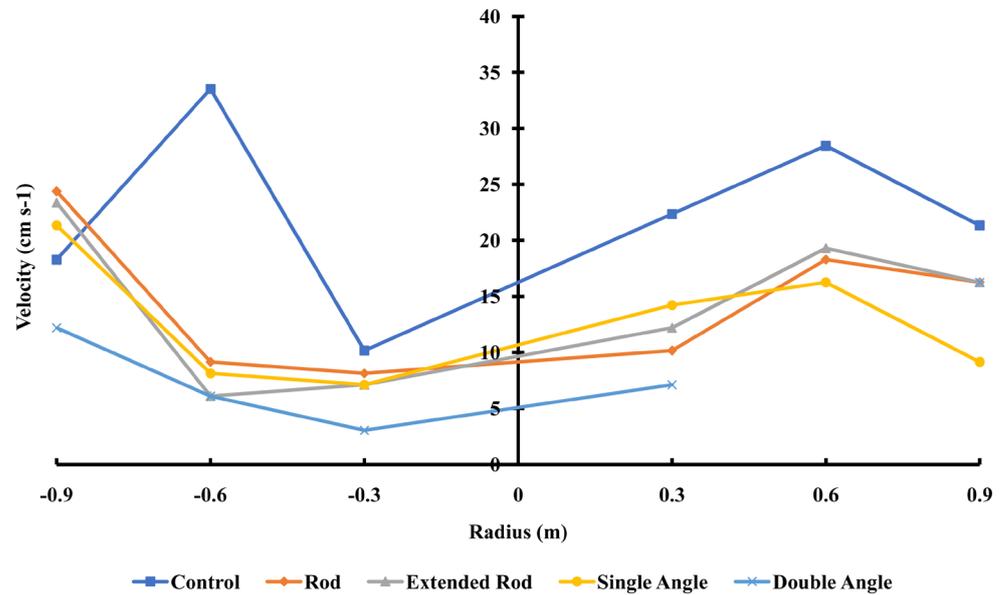


Figure 6. Cross section velocity profiles at a depth of 10 cm (surface) of a 1.8 m diameter circular tank containing different types of suspended environmental enrichment arrays at an incoming velocity of 18.3 cm/s. The cross section was perpendicular to the location of the inlet water spraybar and suspended enrichment. Part of the double angle enrichment was located at 0.6 and 0.9 m, precluding velocity measurement.

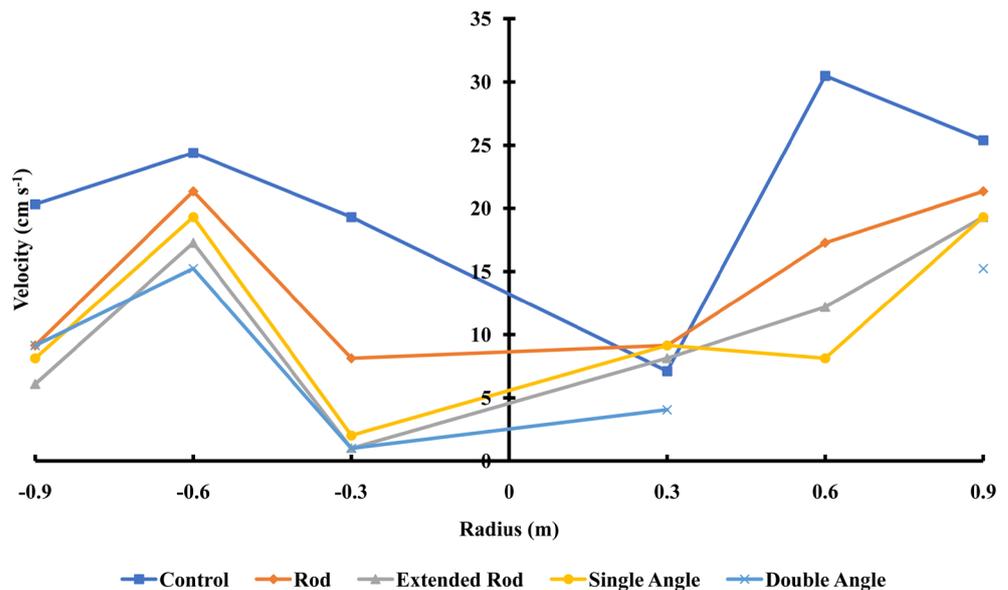


Figure 7. Cross section velocity profiles at a depth of 30.5 cm (mid-depth) of a 1.8 m diameter circular tank containing different types of suspended environmental enrichment arrays at an incoming velocity of 18.3 cm/s. The cross section was perpendicular to the location of the inlet water spraybar and suspended enrichment. Part of the double angle enrichment was located at 0.6 and 0.9 m, precluding velocity measurement.

treatments were similar at both the surface and bottom at 0°, radii 30 cm at the incoming velocity of 18.3 cm/s, and radii 90 cm at 90° at the surface and 270° at the bottom of the 54.9 cm/s incoming velocity.

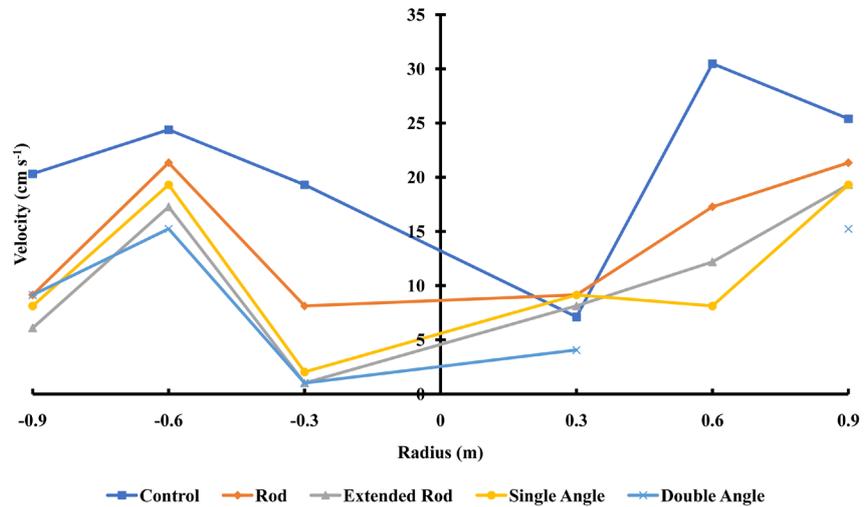


Figure 8. Cross section velocity profiles at a depth of 51.8 cm (bottom) of a 1.8 m diameter circular tank containing different types of suspended environmental enrichment arrays at an incoming velocity of 18.3 cm/s. The cross section was perpendicular to the location of the inlet water spraybar and suspended enrichment. Part of the double angle enrichment was located at 0.6 and 0.9 m, precluding velocity measurement.

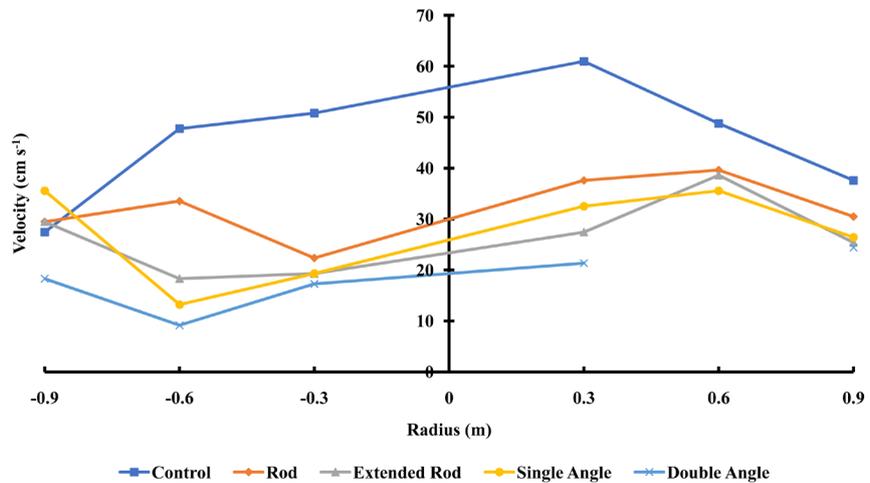


Figure 9. Cross section velocity profiles at a depth of 10 cm (surface) of a 1.8 m diameter circular tank containing different types of suspended environmental enrichment arrays at an incoming velocity of 54.9 cm/s. The cross section was perpendicular to the location of the inlet water spraybar and suspended enrichment. Part of the double angle enrichment was located at 0.6 and 0.9 m, precluding velocity measurement.

4. Discussion

The significant in-tank velocity reductions resulting from the addition of vertically-suspended structures observed in this study support the results previously reported [10]. The decrease in velocity at nearly every sampling location occurred despite the minimal space occupied by the structures in the tank. The most dramatic impacts on velocity were observed with the double angle treatment, yet these two arrays, containing a total of only eight suspended angles, occupied less than 0.009% of the total tank volume.

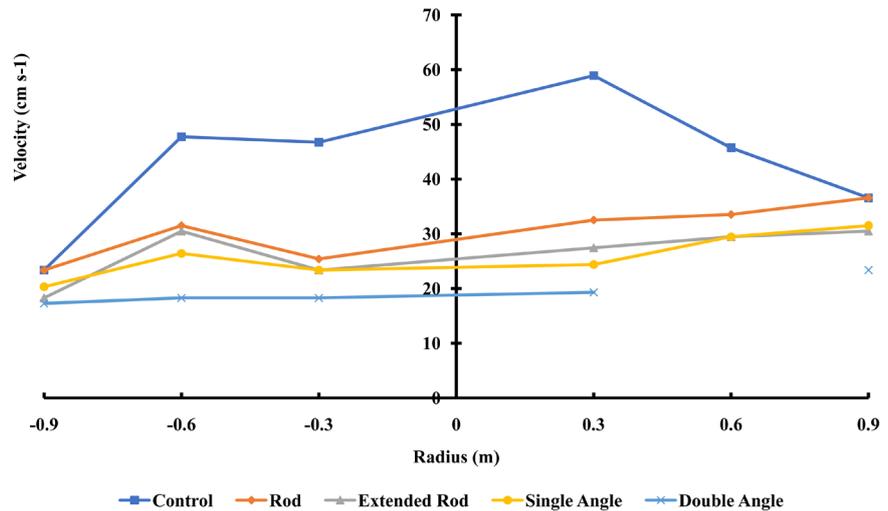


Figure 10. Cross section velocity profiles at a depth of 30.5 cm (mid-depth) of a 1.8 m diameter circular tank containing different types of suspended environmental enrichment arrays at an incoming velocity of 54.9 cm/s. The cross section was perpendicular to the location of the inlet water spraybar and suspended enrichment. Part of the double angle enrichment was located at 0.6 and 0.9 m, precluding velocity measurement.

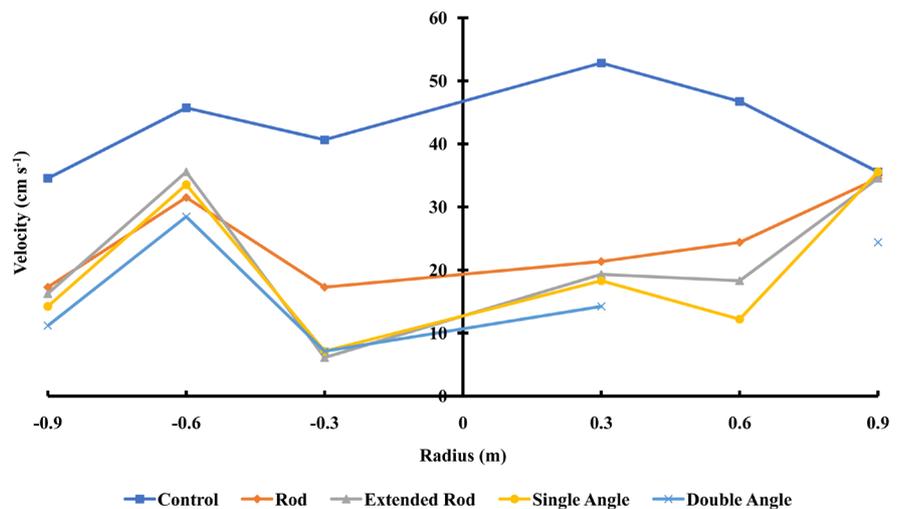


Figure 11. Cross section velocity profiles at a depth of 51.8 cm (bottom) of a 1.8 m diameter circular tank containing different types of suspended environmental enrichment arrays at an incoming velocity of 54.9 cm/s. The cross section was perpendicular to the location of the inlet water spraybar and suspended enrichment. Part of the double angle enrichment was located at 0.6 and 0.9 m, precluding velocity measurement.

At the incoming velocity of 18.9 cm/s, the extended rod, single angle, and double angle treatments all produced in-tank velocities below the limit of 12 to 15 cm/s where tank self-cleaning may start to become affected [1]. Indeed, the bottom velocity of 7.8 cm/s created by the double angle environmental enrichment array was actually below the 8 cm/s threshold where hydraulic self-cleaning completely ceases [1]. At the higher incoming velocity of 54.9 cm/s, the in-tank velocities observed in all of the treatments indicated that the self-cleaning nature

of the circular tanks was not affected by the addition of vertically-suspended environmental enrichment.

Circular tank velocities increase from the center of the tank outward, with the fastest in-tank velocities occurring nearest to the outerwall [4]. Circular tank velocities are highest near the outside of the tank, as well as being higher at the top of the tank [1]. Similar velocity patterns were observed in this study, except with the double angle treatment at the lower incoming water velocity. In this specific treatment, the mean velocity of 8.7 cm/s at the surface was less than the 10.0 cm/s velocity observed at mid-depth.

A large central vortex in the middle of circular tanks has been previously been described [35]. An irrotational zone in the center of circular tanks has also noted [2]. This was observed in this study in all of the treatments at both incoming velocities, despite the in-tank velocity reductions resulting from the inclusion of vertically-suspended environmental enrichment structures.

The increase in fish growth and rearing efficiencies using arrays of suspended objects in circular tanks is well documented [27] [28] [29] [30] [31]. These fish rearing benefits are likely at least partially because of the dramatic in-tank velocity changes due to the suspended environmental enrichment. The lower velocity areas created by the arrays may function as favorable bioenergetic microhabitats, allowing fish to avoid the more energy-consuming, high-velocity areas during non-feeding periods [36]. Fish likely benefit from these rest intervals. Indeed, although higher velocity-induced exercise is generally considered beneficial during fish rearing [5] [6] [32] [33], long-term exposure to higher velocities (continual exercise) has recently been shown to be detrimental to fish growth [7] [8]. Thus, the suspended arrays may be allowing the fish to minimize their energy expenditures during feeding, and also benefit from periodic exercise in the higher-velocity areas within the tank [36] [37].

In addition to the potential bioenergetic benefits, the suspended arrays may also be positively influencing in-tank water chemistry parameters, such as the distribution and concentration of dissolved oxygen. Although velocities and water quality are more uniformly distributed in circular tanks compared to rectangular rearing units [3] [4], there is obviously still within-tank variation [9] [13] [14]. The alterations in circular tank velocity patterns from suspended enrichment observed in this study and previously described [9] may make dissolved oxygen levels more favorable throughout the entire tanks, thereby leading to improved fish growth and feeding efficiency [38] [39].

Circular tank velocity profiles can be influenced by multiple factors, including tank size, water inlets and outlets, incoming water velocities, and the number and size of fish in the tank [4] [9] [12] [13] [14]. Even changing from a horizontal incoming-water spray bar, like that used in this study, to a vertical spray bar would impact the velocity profile [1]. Thus, the results of this study may be unique to the 1.8-m diameter circular tanks, incoming water velocities, and vertically-suspended environmental enrichment arrays used in this study. Addi-

tional research could focus on any of these variables. In addition, velocity profiles with vertically-suspended environmental enrichment while fish are present would be extremely beneficial. However, as yet, no studies have been undertaken to ascertain the impact of vertically-suspended structure on fish behavior; structure-induced changes in foraging, resting, or swimming behavior would likely dramatically influence in-tank velocities

Conflicts of Interest

The authors declare no conflicts of interest regarding the publication of this paper.

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