

Textile Dye Removal Using Photocatalytic Cascade Disk Reactor Coated by ZnO Nanoparticles

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Abstract

Dye effluents with low BOD/COD ratio and varied chemical structures are usually very recalcitrant to microbial degradation. Therefore, different process was used for the treatment of dye effluent. Heterogeneous photocatalyst process has been widely used as leading green technology for dye removal. The process utilizes a semiconductor photocatalyst (such as TiO_2 or ZnO) and UV light to oxidize the recalcitrant organic compounds to inorganic ions, carbon dioxide and water. Photocatalytic process needs to photoreactors and hydraulic parameters play an important role in mass transfer phenomenon in photocatalytic reactors. These fundamental parameters are flow rate, relative roughness and Reynolds number. This research experimentally evaluates flow rate and artificial relative roughness in order to determine the factors influencing the removal efficiency and reaction rate. For this purpose, a cascade photocatalytic reactor is constructed which consists of similar Plexiglas plates coated by various roughness. Numerical simulation usually overcomes complex reactor models which takes reasonable cost respect to experimental study. Here, OpenFOAM software is also utilized to perform a numerical study. Regime and velocity of sewage are simulated in photocatalytic flow with/without considering relative roughness.

Keywords

Cascade Disc Reactor, M5P, Reactive Yellow 81, Zinc Oxide, Artificial Roughness

1. Introduction

The use of different synthetic dyes in textile industries has increased in recent decay, resulting in the release of dye-containing industrial effluents into natural aquatic ecosystem [1]. Dye effluents with low BOD/COD ratio and varied chemical structures are usually very recalcitrant to microbial degradation. Therefore, dye removal from effluent

is a main concern in many studies. Different process was used for the treatment of dye effluent. In the last few years, studies were focused on advanced oxidation process (AOPs) methods such as UV-ZnO, UV-H₂O₂, UV-O₃ and UV-TiO₂ [2] [3]. Photocatalytic process such as UV-ZnO is an efficient method that treats nondegradable wastewater by active radicals. The photocatalysis needs a photoreactor that contacts reactant, products and light. In recent years, different types of photoreactors have been used for wastewater treatment. In some reactors, nano-photocatalysts are utilized in slurry form, and the other particles are coated on bed. In Photocatalytic reactors with fixed bed, nano-photocatalysts are immobilized on bed and do not need the separation unit, but the main disadvantage of this photoreactors is the low mass transfer rate between wastewater and nano-photocatalysts [4]. Consequently, Different optimal photoreactors were developed for increasing mass transfer rate. Dionysiou *et al.* investigated the effect of rotational speed on 4-chlorophenol degradation using rotating disk photocatalytic reactor. They concluded that the rate of 4-chlorophenol degradation increased with rotating speed change from 5 to 20 rpm. Similarity, Son *et al.* used rotating drum photocatalytic reactor for Bisphenol degradation. The treatment efficiency of 97 and 99% were reported in the rotational speed of 60 and 120 rpm, respectively. Vezzoli, *et al.* studied the effect of flow rate on mass transfer rate in photocatalytic reactor with immobilized bed in which Reynolds number is limited to the domain of 350 - 3050, and therefore they revealed that flow rate increasing and large Reynolds number lead to increasing of mass transfer rate in a photocatalytic process [5]. Therefore, there are several ways for improving mass transfer of the photocatalytic reactors. The aforementioned literature review emphasizes that the studies had focused on mechanical methods such as rotational speed, agitation speed and flow rate for increasing mass transfer rate in photocatalytic process. In this study, in order to overcoming mass transfer limitation in photocatalytic process, a novel photocatalytic cascade disc reactor coated with ZnO nano-photocatalysts was applied and artificial roughness were created on the surface of disks.

This photoreactor has a number of advantages that include eliminating the need for catalyst separation units as the catalyst is immobilized, creating the flow mixing by non-mechanical method, increasing the transport of oxygen from the gas phase to the photocatalyst surface by providing the flow cascade pattern. The photoreactor was used in order to remove Reactive Yellow 81 (RY81) dye from textile industry effluent, by means of UV-ZnO process. RY81 is a reactive dye composed of 10 Benzene rings and two -N=N azo bonds. The effect of different artificial roughness and recirculation flow rate in removal efficiency was investigated.

2. Applied Materials and Methods

2.1. Cascade Disc Reactor Setup

In order to remove the RY81 dye, a photocatalytic cascade disc reactor is constructed, which consists of four 34 cm diameter circular disc made of Plexiglas and immobilized by ZnO nanoparticles (**Figure 1**).

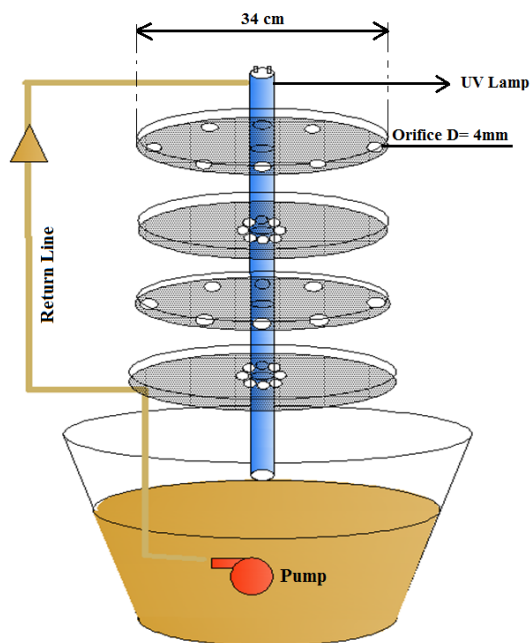
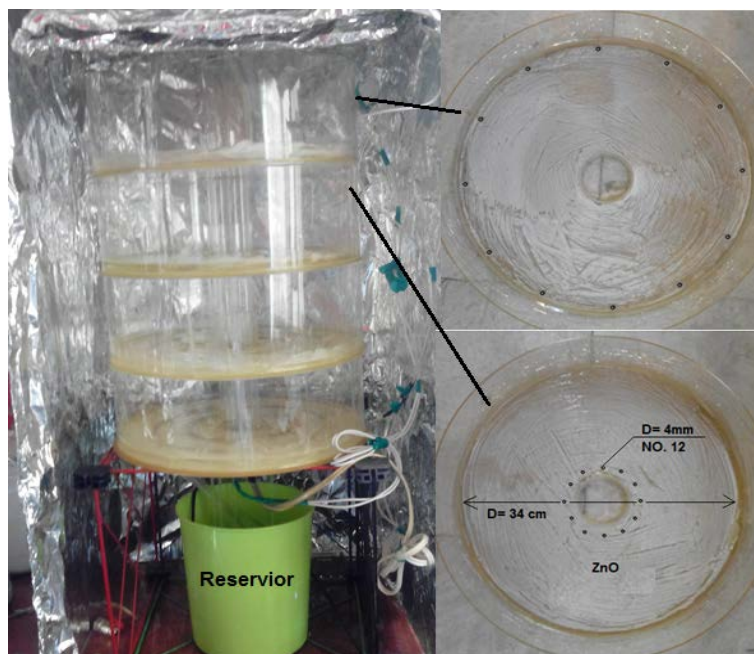


Figure 1. Schematic of the constructed photocatalytic reactor.

In this pilot, sewage flow is pumped to the highest level disc, and then it is transferred as cascade flow to lower level discs by small holes provided on each disc (12 small holes with 4 mm diameter). Also, this turbulence flow is spontaneously aerated. Therefore, mass transfer limitation in the reactors with immobilized bed is reduced significantly. A UVC 20 W lamp is located at the center of the reactor, and disc beds are coated by ZnO nanoparticles with area density of 20 gr/m^2 [6]. In order to create artificial roughness, 5 mm baffles, as shown in **Figure 2** have been used. These baffles are



Figure 2. Disc of the reactor (a) without roughness (b) coated by artificial roughness.

placed at disc radiuses of 7 and 12 cm. Again, sewage flow in storage supply is pumped to the highest level disc. Total volume of sewage treated in this treatment system is 5 liter which is restored with the flow rates of 40, 60 and 80 cc/sec.

2.2. Materials and Equipment

In this study, ZnO nanoparticles with purity of 99% (US research Nanomaterials Inc) are used. Sizes of particles vary from 10 to 90 nm and their surface area and density are 20 - 60 m²/gr and 5.606 gr/cm³, respectively (**Figure 3**).

Other materials including sodium hydroxide and sulfuric acid, made by The Merck Inc, are used for pH adjustment. Spectrophotometer (Hach Dr400) is utilized for determination of absorption ratio and dye concentration. Also, Fungilab Ultrasonic water bath and a digital weighting scale (PLS360-3-Kern) are employed for dispersing the al-gometry nanoparticles and material distribution, respectively. In this experiment, the pump is a submerged Soboti WP 3880 and the lamp is selected as a 20 W Philips (UVC).

2.3. Numerical Model

A two dimensional model is implemented by OpenFOAM software which is a finite volume based open-source computational fluid dynamic (CFD) package. **Figure 4** depicts the geometry of the model that is a sector with diameter of 34 cm and the apex angle of 30 deg (1/12 of a complete disc). 5 cc/sec flow rate is considered for the model and non-slip condition for baffles and the model body is imposed. A 280 × 30 × 14 mesh is defined for the domain at radial, angular and height directions as shown in **Figure 4**.

3. Results and Discussion

3.1. Effect of Initial Concentration on Photocatalytic Process

Initial dye concentration is one of important parameter in photocatalytic process. **Figure 5** shows the effect of various initial dye concentrations from 5 to 100 mg/L on photocatalytic process. The results shown in **Figure 5** illustrates that an increase in the dye concentration will lower the removal rate. When the initial dye concentration in-

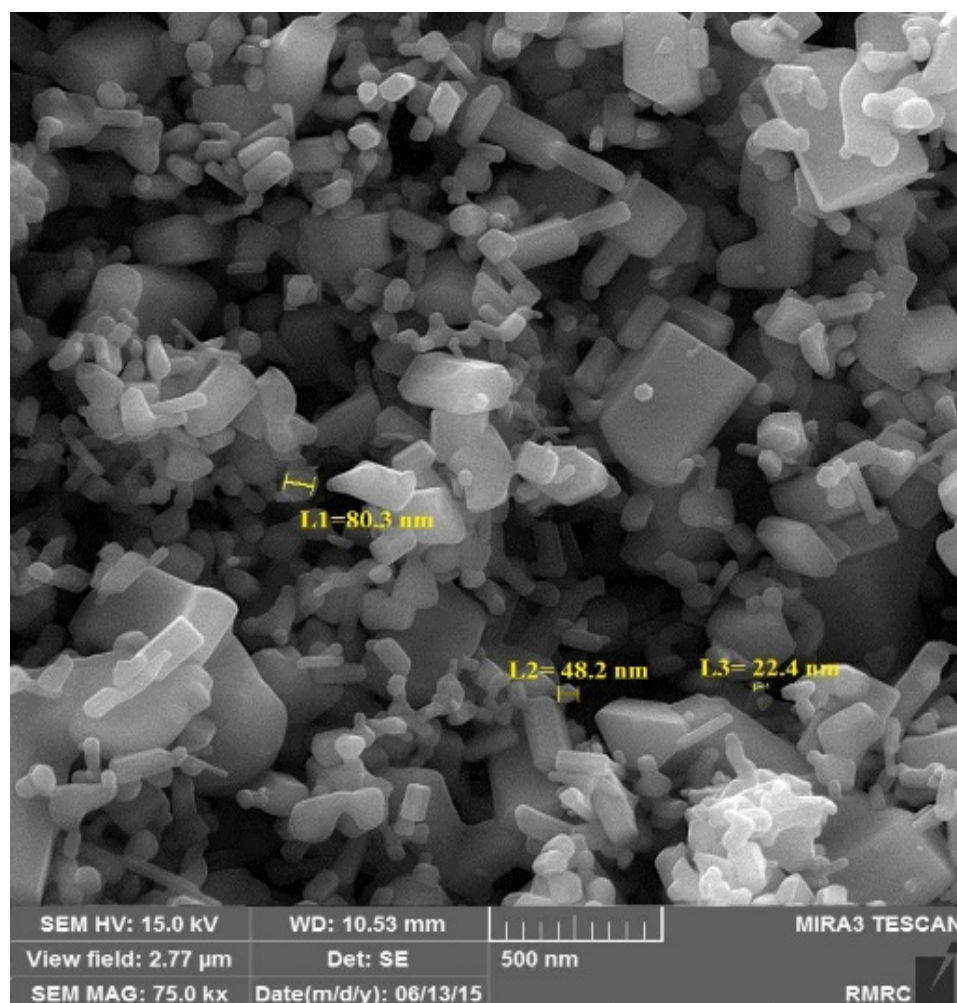


Figure 3. FESEM image of ZnO nanoparticles coated on surface.

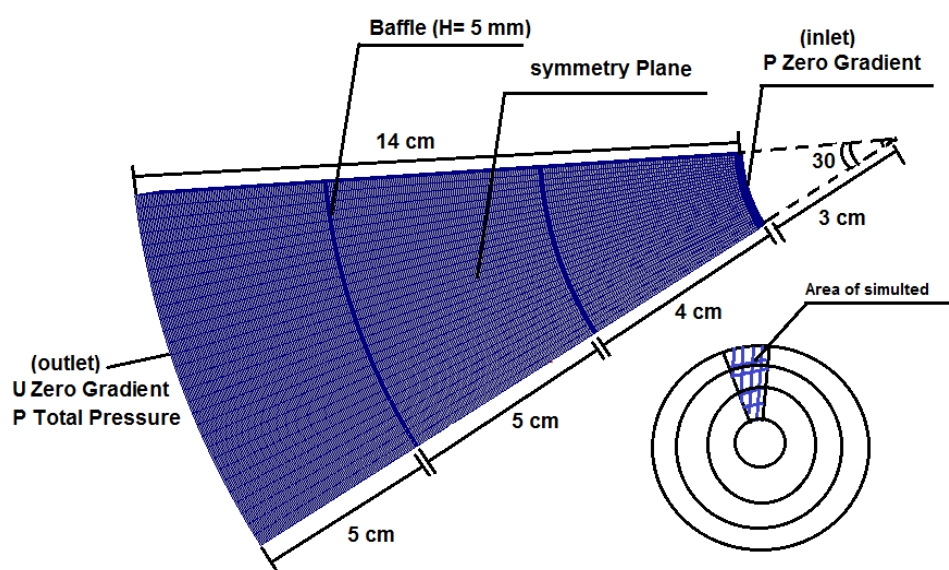


Figure 4. Domain of the numerical model and its generated grid.

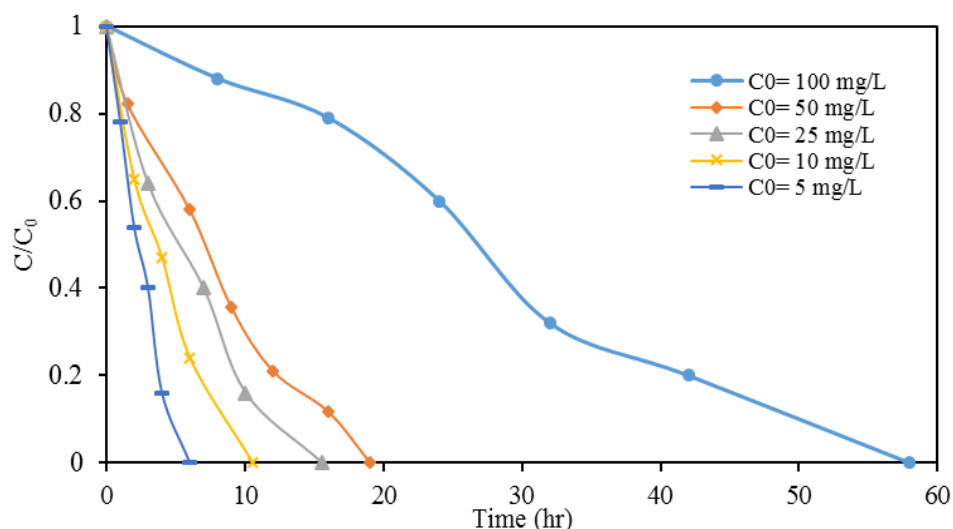


Figure 5. Effect of initial concentration on of photocatalytic decolorization of RY 81 ($Q = 40$ cc/s, without roughness, $pH = 7$).

creases from 5 to 100, the total time for complete degradation of RY81 increased from 6 to 57 hr. This affects the catalytic activity of ZnO nanoparticles and the number of active site on disk surface. Another impact of increasing dye concentration is related to changing of path length of photons entering the dye solution.

3.2. Flow Rate Effects on Photocatalytic Process

This research also evaluates the effects of flow rate on the RY81 removal. These experiments use dye concentrations of 10, 50 and 100 mg/L; and flow rates of 40, 60 and 80 cc/sec; pH of 7; and a 20W UV lamp. In these experiments, Reynolds numbers are adjusted to be different. Figure 6 indicates the effect of flow rate, which varies from 40 to 80 cc/sec, on the first order reaction rate in cascade disk reactor without roughness. Furthermore, final run-time for complete dye removal with different concentrations is reduced when flow rate is increased, **Figure 6** indicates that flow rate increasing results in Reynolds number increasing and turbulence flow is formed. Probability of catalyst and pollution collision is increased and time of dye removal process is improved as turbulence effect enhances the collision [5]. This flow rate increasing (Reynolds number increasing) causes diffusion phenomenon to be happen between catalyst surface and dye molecules, and increases convection mass transfer rate [7].

3.3. Effect of Artificial Relative Roughness on the Photocatalytic Process

By coating roughness with height of 0.5 cm on the disc surface, total removal run-time is changed. **Table 1** illustrates the effects of two parameters (relative roughness and flow rate). 10 mg/L dye removal subjected to flow rates of 40, 60 and 80 cc/sec without considering roughness takes 10.5, 9.5, and 8.2 hours, respectively. These times are reduced to 10, 9 and 7.4 hours, respectively, when roughness is considered.

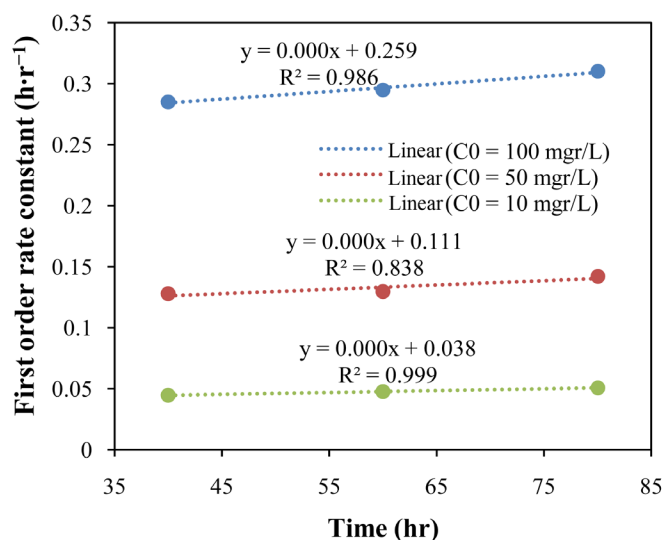


Figure 6. Effect of flow rate on the reaction rate of photocatalytic process without roughness.

Table 1. Total dye removal time of RY81 for initial concentrations and different flow rates with/without roughness

C (mg/L)	Q (cc/s)	Time for Destruction of RY81 without Roughness	Time for Destruction of RY81 with Roughness	Time Reduction (%)
10	40	10.5	10	4.8
10	60	9.5	9	5.3
10	80	8.2	7.7	6.1
50	40	22	21	4.5
50	60	20	18.6	7.0
50	80	19	18	5.3
100	40	57	54	5.3
100	60	52	49	5.8
100	80	50	47	6.0

Therefore, total dye removal time is decreased about 5.6%. Artificial roughness increases flow velocity of the spaces between baffles so that the velocity and Reynolds number become two times greater. **Figure 7** indicates that as Reynolds number increase, overall dye removal time is decreased [8] [9]. Also, artificial roughness makes turbulence flow and the formed vortexes reduce dead space and increase mass transfer rate [10] [11]. As depicted in **Figure 8**, vortex is formed between two baffles, enhancing turbulence effects at the catalyst surface.

Figure 8 compares the effects of flow rates and relative roughness for pollution with concentration of 10 mg/L. Overall removal time is 10.5 hours for flow rate of 40 cc/sec without roughness, while it is 7.7 hours for flow rate of 80 cc/sec when roughness is considered, which the time is reduced to 27%.

Moreover, **Figure 9** compares dye removal times for different flow rates with and without considering roughness. The result shows that increasing flow rates and existence of roughness lead to improve removal time.

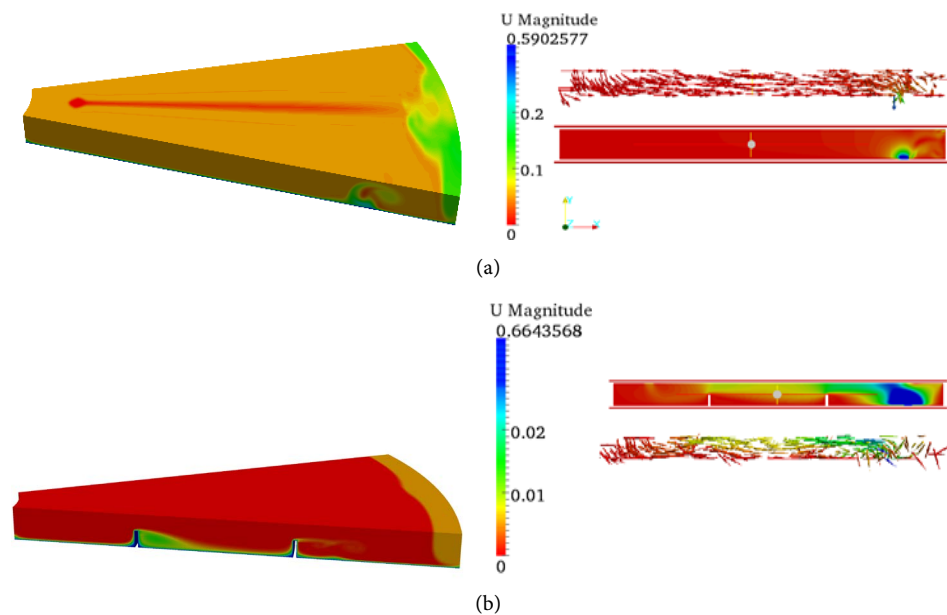


Figure 7. Velocity of hydraulic model of reactor: (a) without roughness; and (b) with roughness.

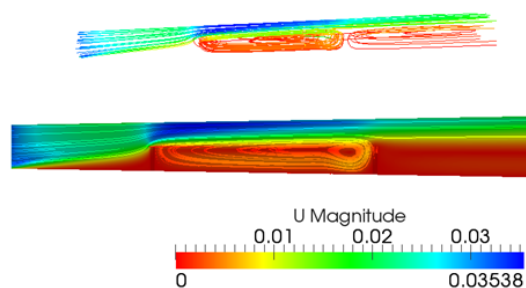


Figure 8. Vortex formed in the hydraulic model.

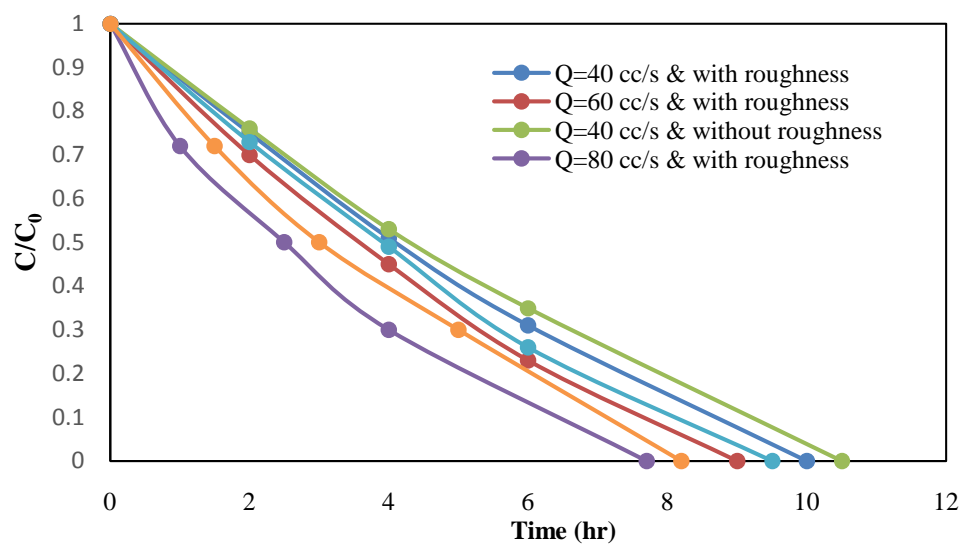


Figure 9. Effects of flow rates and artificial relative roughness on the RY81 dye removal with concentration of 10 mg/L.

4. Conclusions

Efficiency improvement of a reactor by non-mechanical equipment and roughness change due to using baffles is an economical way for sewage treatment and improvement of photocatalytic reaction rate. Mass transfer rate can also be increased by increasing flow rate leading to turbulence flow. A reactor with roughness property is more reliable and requires low maintenance cost.

Effects of relative artificial roughness are assessed in a cascade disc reactor by CFD simulation. The results demonstrate that the imposed roughness, separate the boundary layer at downstream of each barrier and vortex is formed between barrier increasing vertical mixture of the flow. Furthermore, experimental results show that mass transfer phenomenon and photocatalytic rate process can be increased by changing hydraulic parameters such as flow rate and roughness. Because dead space is reduced by increasing the roughness, and Reynolds number and flow velocity becomes two times greater without spending energy. Hydraulic condition modifications increase the photocatalytic reaction rate to 26%.

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