

Development of High Torque and High Power Density Hybrid Excitation Flux Switching Motor for Traction Drive in Hybrid Electric Vehicles

Erwan Sulaiman^{1,2*}, Takashi Kosaka²

¹MyEV, Department of Electrical Power Engineering, University Tun Hussein Onn Malaysia, Johor, Malaysia

²Department of Electrical & Computer Science Engineering, Nagoya Institute of Technology, Nagoya, Japan
Email: *erwan@uthm.edu.my

Received February 15, 2012; revised January 2, 2013; accepted January 9, 2013

Copyright © 2013 Erwan Sulaiman, Takashi Kosaka. This is an open access article distributed under the Creative Commons Attribution License, which permits unrestricted use, distribution, and reproduction in any medium, provided the original work is properly cited.

ABSTRACT

This paper presents design feasibility study and development of a new hybrid excitation flux switching motor (HEFSM) as a contender for traction drives in hybrid electric vehicles (HEVs). Initially, the motor general construction, the basic working principle and the design concept of the proposed HEFSM are outlined. Then, the initial drive performances of the proposed HEFSM are evaluated based on 2D-FEA, in which the design restrictions, specifications and target performances are similar with conventional interior permanent magnet synchronous motor (IPMSM) used in HEV. Since the initial results fail to achieve the target performances, deterministic design optimization approach is used to treat several design parameters. After several cycles of optimization, the proposed motor makes it possible to obtain the target torque and power of 333 Nm and 123 kW, respectively. In addition, due to definite advantage of robust rotor structure of HEFSM, rotor mechanical stress prediction at maximum speed of 12,400 r/min is much lower than the mechanical stress in conventional IPMSM. Finally, the maximum torque and power density of the final design HEFSM are approximately 11.41 Nm/kg and 5.55 kW/kg, respectively, which is 19.98% and 58.12% more than the torque and power density in existing IPMSM for Lexus RX400h.

Keywords: Hybrid Excitation Flux Switching Machine (HEFSM); Field Excitation Coil (FEC); Permanent Magnet (PM); Hybrid Electric Vehicle (HEV)

1. Introduction

Hybrid excitation machine (HEM) which consists of permanent magnet (PM) and field excitation coil (FEC) as their combined flux sources, has several unique features that can be applied in HEV drive system. In general HEM can be classified into four categories based on the location of PM and FEC such as 1) both PM and FEC are located at rotor side [1-3], 2) the PM is in the rotor while the FEC is in the stator [4], 3) the PM is in the rotor while the FEC is in the machine end [5,6], and 4) both PM and FEC are located in the stator [7-9]. All HEMs mentioned in the first three consist of a PM in the rotor and can be categorized as “hybrid rotor-PM with FEC machines” while the final machine can be referred as “hybrid stator-PM with FEC machines”. Based on its principles of operation, in which the fluxes sources are

generated in stator side and moved into the rotor, the fourth machine is also known as “hybrid excitation flux switching machine” (HEFSM) which is getting more popular recently [10,11]. With all active parts located on the stator, HEFSM has the advantages of 1) robust rotor structure which is becoming more suitable to be applied for high-speed drive applications, 2) due to the fact that the all major heats are accumulated in stator part, a simple cooling system can be applied compared with a complex water jacket system used in IPMSM for Lexus RX400h, and 3) the additional FEC can be used to control flux with variable flux capabilities.

Various combinations of stator slot and rotor pole for HEFSM have been developed for high speed applications. For example, 12Slot-10Pole HEFSM has been proposed such as in [12,13]. However, the machine in [12] has a separated PM and C-type stator core that makes it difficult to manufacture, and the design is not yet optimized

*Corresponding author.

for HEV applications while the machine in [13] has a limitation of torque and power production in high current density condition. This is due to insufficient stator yoke width between FEC and armature coil slots resulting in magnetic saturation and negative torque production. To reduce the supply frequency of inverter, 6Slot-5Pole HEFSM has been proposed by the authors. Although the proposed machine has met the target performances, the problem of unbalanced pulling force due to odd number of poles is difficult to overcome [14]. In addition, some researchers have proposed 6Slot-8Pole machines but these types of machines have problems of high torque ripple and back-emf waveforms, which are usual concerns for this type of eight pole machine [15,16].

In this paper, design feasibility and optimization studies are conducted to 12Slot-10Pole HEFSM in effort to achieve the target performances for HEV applications. **Figure 1** illustrates the cross-sectional view of the main machine part of the initial HEFSM. The motor is composed of 12 PMs and 12 FECs distributed uniformly in the midst of each armature coil while the three-phase armature coils are accommodated in the 12 slots for each 1/4 stator body periodically. In this motor, the PMs and FECs produce six north poles interspersed between six south poles. The flux paths caused by both PM and mmf of FEC under open circuit condition are demonstrated in **Figure 2**. The term, “flux switching”, is created based on the changes in polarity of each flux in each stator tooth, depending on the motion of the rotor. When the rotor rotates, the fluxes generated by PM and FEC link with the armature coil flux alternately. For the rotor rotation through 1/10 of a revolution, the flux linkage of the armature coil has one periodic cycle and thus, the frequency of back-emf induced in the armature coil becomes ten times of the mechanical rotational frequency.

2. Design Requirements, Restrictions and Specifications for HEV Applications

The design requirements, restrictions and specifications of the proposed HEFSM for HEV applications are similar with IPMSM for Lexus RX400h listed in **Table 1** [17]. The electrical restrictions related with the inverter such as maximum 650 V DC bus voltage and maximum 360 V inverter current are set. The limit of the armature coil current density, J_a and the FEC current density, J_e is set to $30 \text{ A}_{\text{rms}}/\text{mm}^2$ and $30 \text{ A}/\text{mm}^2$, respectively. The weight of the PM is 1.1kg similar with PM volume in IPMSM. The target torque of 333 Nm with reduction gear ration of 2.478 is set, hence, realizing the maximum axle torque via reduction gear of 825 Nm. The maximum operating speed is set to 12,400 r/min and the target power is set to be more than 123 kW. As the proposed HEFSM consists of very simple structure with concentrated winding in all coils, the target motor weight to be

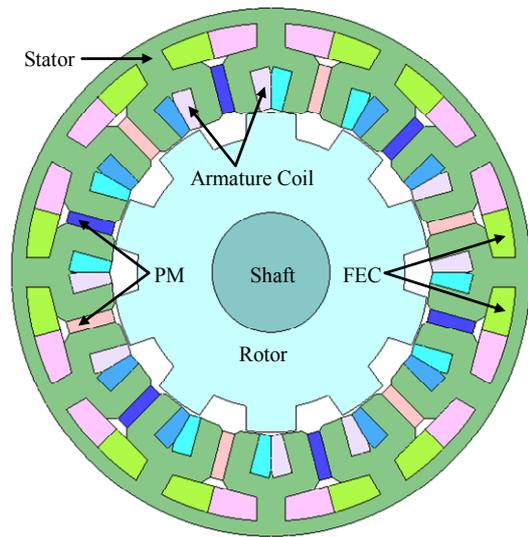


Figure 1. 12Slot-10Pole HEFSM.

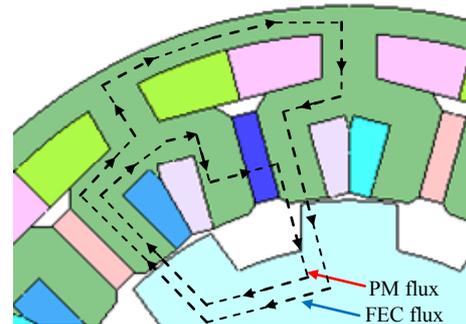


Figure 2. Flux paths of PM and FEC in 12Slot-10Pole HEFSM.

Table 1. HEFSM design restrictions and specifications.

Items	IPMSM	HEFSM
Maximum DC-bus voltage inverter (V)	650	650
Maximum inverter current (A_{rms})	360	360
Maximum J_a ($A_{\text{rms}}/\text{mm}^2$) ^a	31	30
Maximum J_e (A/mm^2) ^b	NA	30
Stator outer diameter (mm)	264	264
Motor stack length (mm)	70	70
Shaft radius (mm)	30	30
Air gap length (mm)	0.8	0.8
PM weight (kg)	1.1	1.1
Maximum speed (r/min)	12,400	12,400
Maximum torque (Nm)	333	333
Reduction gear ratio	2.478	2.478
Max. axle torque via reduction gear (Nm)	825	825
Maximum power (kW)	123	>123
Power density (kW/kg)	3.5	>3.5

J_a = current density in armature coil; J_e = current density in FEC.

designed is set to be less than 35 kg, resulting in that the proposed machine promises to achieve the maximum power density of more than 3.5 kW/kg. Commercial FEA package, JMAG-Studio ver.10.0, released by Japanese Research Institute (JRI) is used as 2D-FEA solver in this design.

3. Initial Performances of the Proposed HEFSM Based on 2D-FEA

Initially, performances of the proposed HEFSM in open circuit condition such as back-emf and cogging torque are analyzed as shown in **Figures 3** and **4**. In **Figure 3**, the amplitude of the fundamental component in which the induced voltage is generated from the flux of PM only is 123.6 V. The back-emf is slightly sinusoidal which results a small amount of cogging torque of approximately 1.06 Nm peak-to-peak. However, when J_c is set to 15 A/mm², the induced voltage is slightly distorted and the amplitude is increased to 263.2 V which is more than double of that under no FEC current. This is due to the field strengthening effect by the additional FEC. For load analysis, performances of the machine at maximum J_a and J_c are analyzed. The torque and power obtained at base speed 5731.4 r/min are 175.9 Nm and 105.6 kW, respectively, which is less than the target value. To investigate this issue, the torque versus J_c at various J_a is plotted as depicted in **Figure 5**. It is obvious that the torque is increased with increasing J_c up to certain J_c and begins to decrease when higher J_c is applied as shown in red circle. For instance, at J_a of 30 A_{rms}/mm², the maximum torque of 181.66 Nm is obtained when J_c is set to 20 A/mm². However, the torque starts to reduce when J_c is set higher than this value. For J_a of 20 A_{rms}/mm² and 25 A_{rms}/mm², the maximum torque obtained are 152.72 Nm and 170.94 Nm respectively, when J_c is set to 15 A/mm². The torque also starts to reduce when J_c is set higher than this value. Similarly, the same phenomenon occurs at the condition of J_a of 5 A_{rms}/mm², 10 A_{rms}/mm² and 15 A_{rms}/mm² where the torque starts to reduce when J_c is set higher than 10 A/mm².

To explain this phenomenon, further investigation is examined on the flux density distribution at three conditions 1) before maximum torque, 2) at maximum torque, and 3) after maximum torque. For example, at maximum J_a of 30 A_{rms}/mm², flux distribution at J_c of 10 A/mm², 20 A/mm² and 30 A/mm² are investigated as shown in **Figure 6**. It can be seen that for low J_c of 10 A/mm², the flux can easily flow to the direction according to its principle as shown in **Figure 6(a)**. Nevertheless, the flux flow to the left part starts to saturate between armature coil upper slot and FEC lower slot marked in blue circle when J_c is set to 20 A/mm² as shown in **Figure 6(b)**. In this case, some of the flux from FEC which flow to the right side

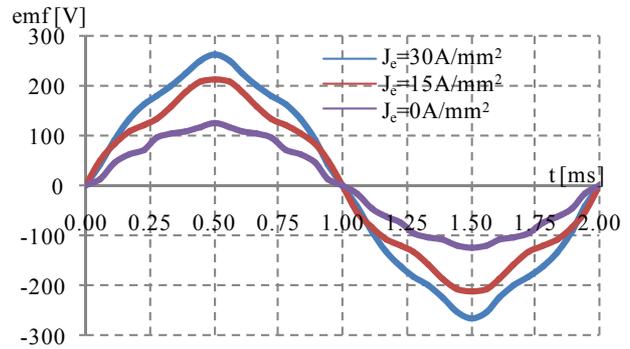


Figure 3. Back-emf at 3000 r/min.

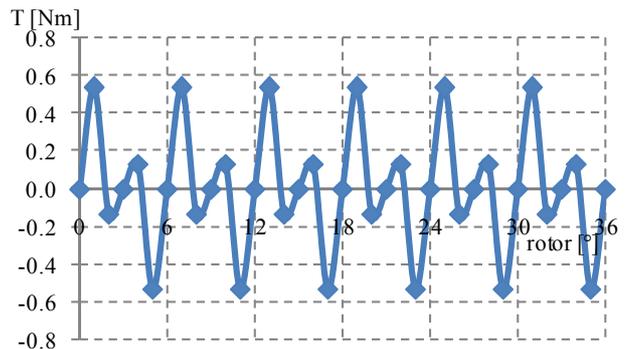


Figure 4. Cogging torque of the original design HEFSM.

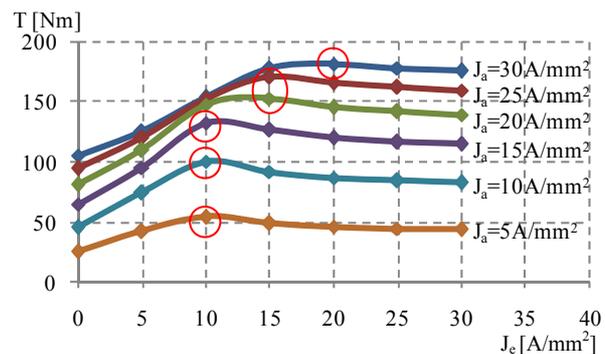


Figure 5. Torque versus J_c at various J_a .

cancelled the flux from PM as shown in red circle which results in reducing the torque production. Hence, for the maximum J_c of 30 A/mm² where much FEC flux is generated, the flux flow to the left part is totally saturated between armature coil upper slot and FEC lower slot marked in blue circle. Therefore, much higher flux from the stator outer yoke passes the FEC pitch move towards the PM in the right side. This flux also cancelled the PM flux and some of the flux is forced to flow into the rotor side producing much negative torque as shown in **Figure 6(c)**, hence reducing the torque production. Thus, one of the methods that can be used to overcome this problem is by investigating the suitable length between armature coil upper slot and FEC lower slot to avoid flux saturation.

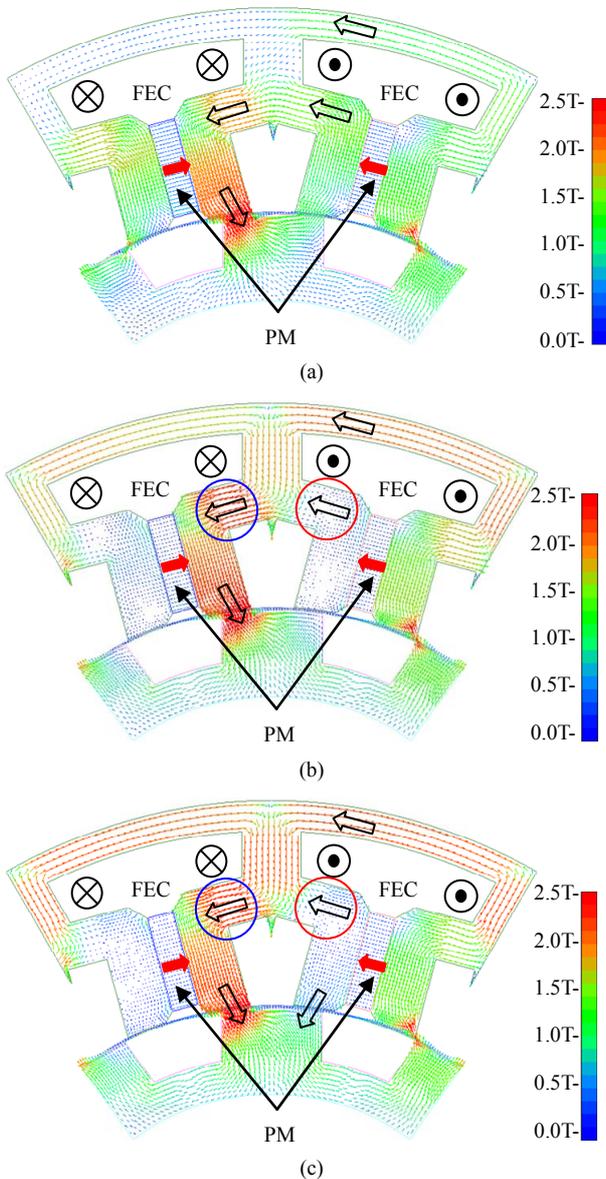


Figure 6. Flux vector diagram of various J_e at maximum J_a of $30 \text{ A}_{\text{rms}}/\text{mm}^2$ (a) $J_e = 10 \text{ A}/\text{mm}^2$, $T = 153.4 \text{ Nm}$ (b) $J_e = 20 \text{ A}/\text{mm}^2$, $T_{\text{max}} = 181.7 \text{ Nm}$ (c) $J_e = 30 \text{ A}/\text{mm}^2$, $T = 175.9 \text{ Nm}$.

4. Design Methodology for Improvements

To make a simple design, the shape of armature coil slot and air gap between the inner and outer PM are redesign, so that design free parameters of D_1 to D_{10} can be defined as illustrated in **Figure 7**. The first step is carried out by updating the rotor parameters, D_1 , D_2 and D_3 while keeping D_4 to D_{10} as constant. As the torque increases with the increase in rotor radius, D_1 which is considered as the dominant parameter that can improve the torque is firstly treated. In this condition, D_4 , D_6 , D_8 , D_9 and D_{10} are simply shifted to the new position by following the movement of D_1 , while D_5 and D_7 are kept constant. Then, by selecting D_1 at its maximum performance, both

rotor pole width D_2 and rotor pole depth D_3 are varied. Once the maximum performance from the combination of D_2 and D_3 is determined, the second step is carried out by changing the FEC slot parameters D_4 , D_5 and D_6 while keeping the other parameters constant. Then, by using the combination of D_4 to D_6 that bring out the maximum performance at the second step, the third step is carried out by varying the armature coil slot parameters D_7 and D_8 with keeping other parameters constant. The necessary armature coil slot area, S_a is determined by varying armature coil depth, D_7 and armature coil width, D_8 to accommodate natural number of turns, N_a for armature coil. Furthermore, to ensure the PM is not demagnetized at temperatures as high as 180°C , D_9 and D_{10} are adjusted with keeping the same PM volume. The method of changing D_1 to D_{10} is treated repeatedly until the target performances are achieved.

All design parameters are adjusted with keeping air gap length of 0.8 mm constant under maximum J_a and J_e . In addition, at the final design, the corners circled in **Figure 7** are designed as a curve to ensure all flux at the edge of the shape flow more smoothly, hence increases the performance of the machine. For the rotor inner pole, the curve designed not only increased the flux flows but also increase the rotor mechanical strength of the machine, make it more robust to work in high speed condition. Finally, after few cycle of optimization, the machine satisfied the target requirements and performances for HEV applications. The cross sectional views of the final design HEFSM is depicted in **Figure 8**, while details of final parameters are listed in **Table 2**. The differences between the initial and the final design HEFSM are 1)

Table 2. Initial and final design parameters.

	Details	Initial	Final
	PM volume (kg)	1.1	1.1
D_1	Rotor radius (mm)	80.2	88.2
D_2	Rotor pole width (mm)	12.5	9.5
D_3	Rotor pole depth (mm)	12.2	23.2
D_4	Permanent magnet height (mm)	24.0	15.0
D_5	FEC slot pitch (mm)	7.4	20.0
D_6	Stator outer core thickness (mm)	7.4	8.0
D_7	Armature coil width (mm)	8.0	6.0
D_8	Armature coil depth (mm)	19.1	32.71
D_9	Distance between air gap and PM (mm)	2.0	0.5
D_{10}	Distance between FEC and PM (mm)	4.0	0.5
N_a	No. of turns of armature coil	7	9
T	Torque (Nm)	175.86	334.5
N	Speed (r/min)	5731.4	3701.2
P	Power (kW)	105.55	129.6
pf	Power factor	0.368	0.452

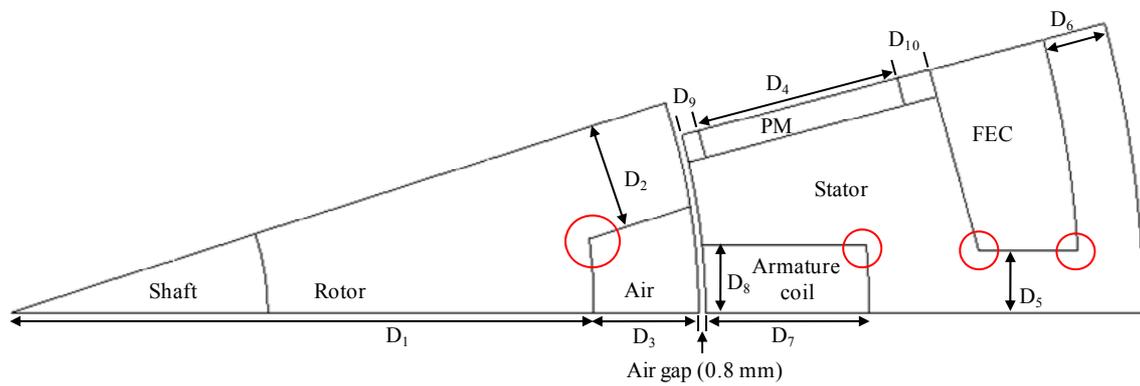


Figure 7. Design parameter defined as D_1 to D_{10} .

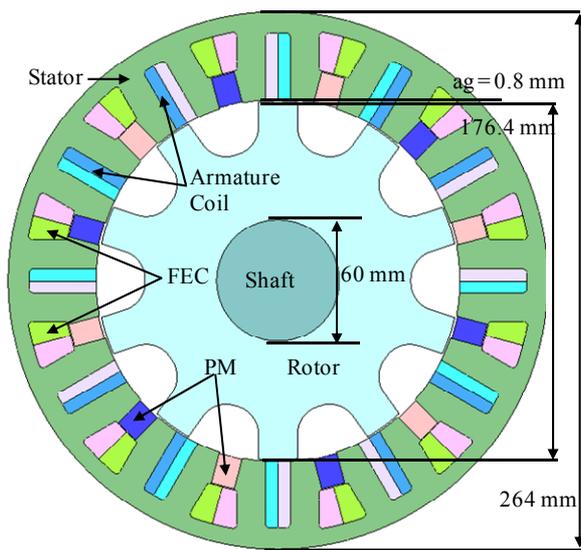


Figure 8. Final Design HEFSM.

the rotor radius of the final design is longer than the initial rotor radius which gives more torque as had been expected, 2) the armature coil width of the final design is less than the initial design, but has high armature coil depth which results in more number of turns, 3) the FEC slot area is reduced approximately 40% from the initial design to cover some volume of stator yoke used for armature coil, 4) the final design has less PM depth with high PM width to keep the same PM volume of 1.1 kg, 5) the final design has no gap between armature coil upper slot and FEC lower slot which solved the flux saturation problem, 6) the stator outer core thickness is higher than the initial design to allow more flux to flow smoothly, and 7) the final design has a stator yoke with a straight “I shape” that makes the flux flow more easily into the rotor. As a proof, **Figure 9** illustrates the flux distribution of the final design HEFSM for J_e of 20 A/mm^2 and 30 A/mm^2 with maximum J_a of $30 \text{ A}_{rms}/\text{mm}^2$. As the gap between armature coil upper slot and FEC lower slot in the final design HEFSM is expanded and considered

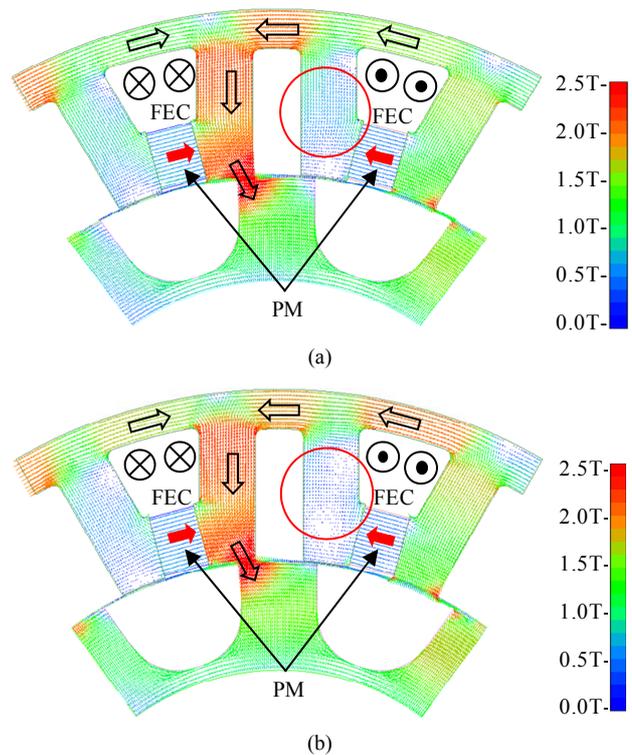


Figure 9. Flux vector diagram of various J_c at maximum J_a of $30 \text{ A}_{rms}/\text{mm}^2$ (a) $J_c = 20 \text{ A/mm}^2$, $T = 280.4 \text{ Nm}$ (b) $J_c = 30 \text{ A/mm}^2$, $T = 334.4 \text{ Nm}$.

negligible, the magnetic saturation caused by higher FEC current is relaxed. Thus, the improved design maintains the same torque for both current density conditions and enables to extract higher power factor.

5. Results and Performances of the Final Design HEFSM

5.1. Flux Path at Open Circuit Condition

The open circuit field distribution for PM and FEC of the final design HEFSM are investigated based on 2D-FEA as illustrated in **Figure 10**. **Figure 10(a)** illustrates the

flux path due to mmf of PM only, while **Figure 10(b)** represents the combination of flux line from both PM and mmf of FEC at maximum FEC density, J_e of 30 A/mm^2 . In **Figure 10(a)**, it is obvious that almost 100% flux of PM flow in the stator iron around the FEC. This yields negligible cogging torque and almost no back-emf at open-circuit condition under the maximum speed operation, which makes it easy to protect the switching devices when the inverter is shut down due to some failures. In contrast, from **Figure 10(b)**, a large amount of fluxes flow to the rotor side by field strengthening excitation, resulting in the maximum torque production with the aid of hybrid excitation.

Furthermore, **Figures 11** and **12** illustrate the comparison between back-emf and cogging torque of the initial and final design at 3000 r/min, respectively. It is clear that, the back emf of the final design is more sinusoidal and much less by approximately 36% of the initial design. The final cogging torque is also reduced by more than 50% of the initial design.

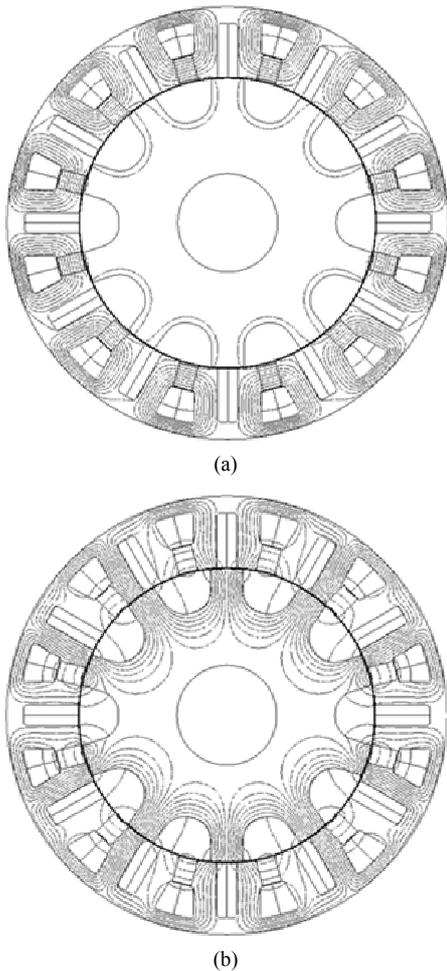


Figure 10. Flux path of the final design HEFSM at open circuit condition (a) PM only (b) PM and maximum FEC current density of 30 A/mm^2 .

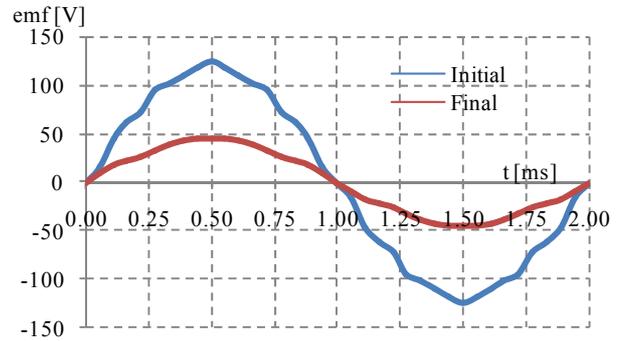


Figure 11. Back-emf.

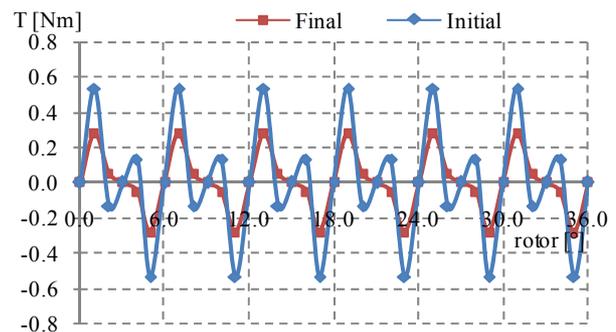


Figure 12. Cogging torque.

5.2. Torque and Power Factor versus J_e Characteristics

The torque and power factor versus J_e characteristics are plotted in **Figures 13** and **14**, respectively. From the plot, it is obvious that increasing J_a will increase the torque but will reduce the power factor. To equilibrate this situation, J_e is increased so that the power factor can be improved and kept constant even if J_a is very high. The plots clearly show that maximum torque of 334.4 NM is obtained when J_a and J_e are set to 30 A/mm^2 as their maximum with the power factor of 0.452. However, for low J_a of less than $15 \text{ A}_{\text{rms}}/\text{mm}^2$, the torque are slightly reduced with the increasing of J_e of more than 20 A/mm^2 . This situation occurs due to excessive FEC flux that generates negative torque thus reducing the performances, similar with the original HEFSM discussed previously. The comparison between the torque and power factor versus J_e under maximum J_a for the initial and final design HEFSM is depicted **Figure 15**. The torque and power factor of the final design HEFSM increased approximately 50% and 23%, respectively compared with the original design.

5.3. Torque and Power versus Speed Characteristics

The torque versus speed characteristics of the IPMSM and the final design HEFSM are plotted in **Figure 16**.

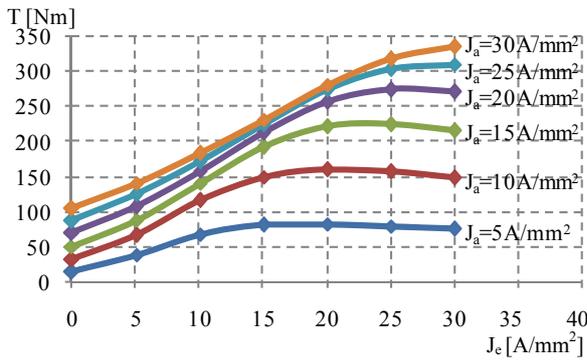


Figure 13. Torque vs J_c .

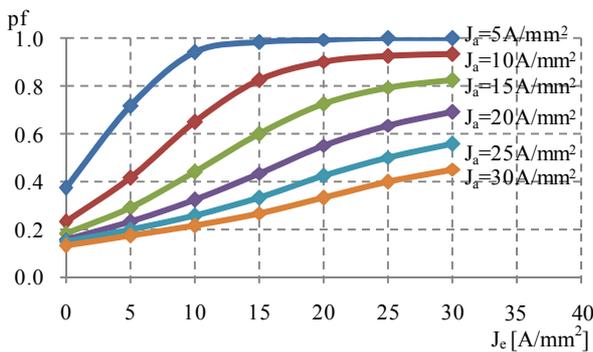


Figure 14. Power factor vs J_c .

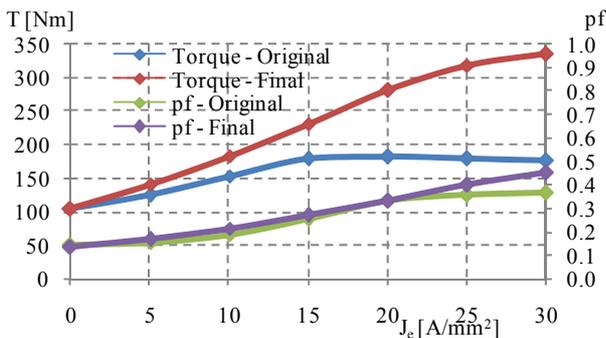


Figure 15. Torque and power factor vs J_c .

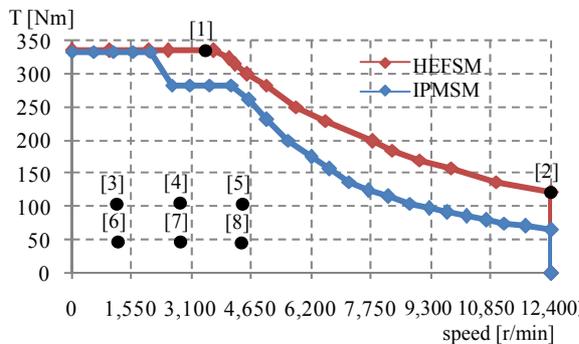


Figure 16. Torque vs speed characteristics.

The maximum torque obtained for IPMSM and HEFMSM are 333 Nm and 334.4 Nm, respectively. It is obvious

that the HEFMSM has better torque condition and produced much higher torque capability in high speed region. Meanwhile, **Figure 17** illustrates the power versus speed characteristics of the IPMSM and the final design HEFMSM. From the graph, 1) at maximum torque, the power achieved for IPMSM and the final design HEFMSM is 72.1 kW and 129.6 kW, at the speed of approximately 2100 r/min and 3701 r/min, respectively, 2) the maximum power obtained is 123 kW for IPMSM and 162.8 kW for HEFMSM 3) the average power of the IPMSM and the HEFMSM at normal driving mode of 3000 - 6000 r/min are 113.7 kW and 133.7 kW, respectively, which proves that the HEFMSM has better performance than IPMSM in frequent driving condition. The total weight of the final design HEFMSM including stator iron, rotor iron, PM, armature coil, FEC, and estimation of both coil ends is 29.3 kg, which is 16.2% less than the estimated of 35 kg for IPMSM. Thus, the maximum torque density and maximum power density are 11.41 Nm/kg and 5.55 kW/kg, respectively, which is much higher than the target requirements for HEV applications. The maximum torque and power density of the final design HEFMSM are increased approximately by 20.0% and 36.9%, respectively compared to 9.51 Nm/kg and 3.51 kW/kg of existing IPMSM.

5.4. Motor Loss and Efficiency

The motor loss and efficiency are calculated considering iron losses in all laminated cores, and copper losses in armature coil and FEC. The detailed loss and motor efficiency of the final design HEFMSM at maximum torque, maximum power, and frequent operating point under light load driving condition noted as No. 1 to No. 8 in **Figure 16** are illustrated in **Figure 18**. At high torque operating points No. 1, the efficiency is slightly degraded due to increase in copper loss while at high-speed operating point No. 2, the motor efficiency is degraded due to increase in iron loss. Furthermore, at frequent driving operation No. 3 to No. 8 under low load condition, the proposed machine achieves relatively high efficiency of more than 93%.

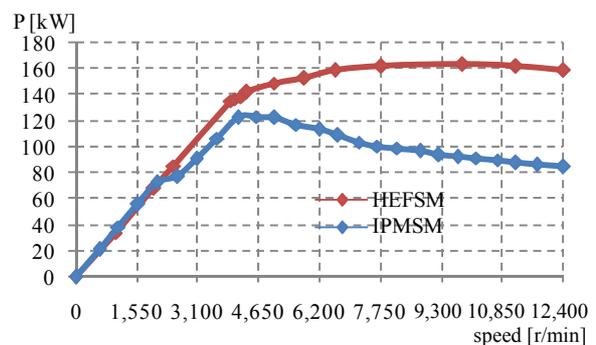


Figure 17. Power versus speed characteristics.

5.5. Rotor Mechanical Strength

The mechanical stress prediction of rotor structure is calculated by centrifugal force analysis based on 2D-FEA as depicted in **Figure 19**. The maximum stress at 12,400 r/min reaches 46 MPa and 28 MPa for the original and final design, respectively, which is much smaller than allowable maximum stress of 300 MPa in conventional electromagnetic steel. This is a great advantage of the final design HEFSM that makes it more applicable and suitable to operate in high-speed application compare to conventional IPMSM.

6. Conclusion

In this paper, design feasibility studies and performance analysis of 12Slot-10Pole HEFSM for traction drive in the target HEV have been presented. The design refinement has been clearly demonstrated and finally achieved

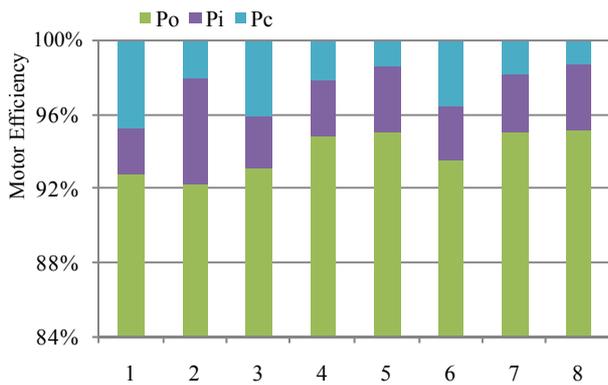


Figure 18. Motor efficiency.

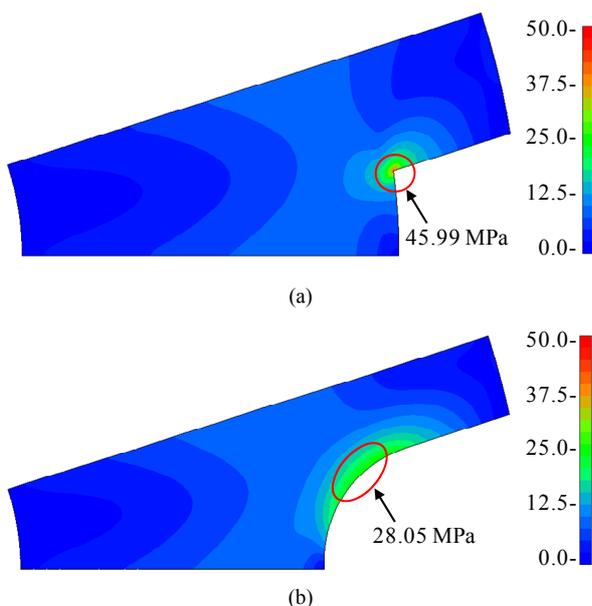


Figure 19. Principal stress distributions of rotor at 12,400 r/min (a) initial design (b) final design.

the target performances. In addition, the rotor mechanical stress predicted is good enough for the machine to run in high-speed region. Finally, the power density of the final design HEFSM has been increased of more than one third when compared with existing IPMSM for LEXUS RX400h. As conclusion, the goal of this research to get maximum performances for HEV applications has been successfully achieved.

REFERENCES

- [1] X. G. Luo and T. A. Lipo, "A Synchronous/Permanent Magnet Hybrid AC Machine," *IEEE Transactions on Energy Conversion*, Vol. 15, No. 2, 2000, pp. 203-210. doi:10.1109/60.867001
- [2] N. Naoe and T. Fukami, "Trial Production of a Hybrid Excitation Type Synchronous Machine," *Proceedings of IEEE International Electric Machines and Drives Conference*, Cambridge, 17-20 June 2001, pp. 545-547. doi:10.1109/IEMDC.2001.939362
- [3] D. Fodorean, A. Djerdir, I. A. Viorel and A. Miraoui, "A Double Excited Synchronous Machine for Direct Drive Application-Design and Prototype Tests," *IEEE Transactions on Energy Conversion*, Vol. 22, No. 3, 2007, pp. 656-665. doi:10.1109/TEC.2007.896279
- [4] J. A. Tapia, F. Leonardi and T. A. Lipo, "Consequent-Pole Permanent-Magnet Machine with Extended Field-Weakening Capability," *IEEE Transactions on Industry Applications*, Vol. 39, No. 6, 2003, pp. 1704-1709. doi:10.1109/TIA.2003.818993
- [5] T. Kosaka and N. Matsui, "Hybrid Excitation Machines with Powdered Iron Core for Electrical Traction Drive Applications," *Proceedings of International Conference on Electrical Machines and Systems*, Wuhan, China, 17-20 October 2008, pp. 2974-979.
- [6] T. Kosaka, M. Sridharbabu, M. Yamamoto and N. Matsui, "Design Studies of Hybrid Excitation Motor for Main Spindle Drive in Machine Tools," *IEEE Transactions on Industrial Electronics*, Vol. 57, No. 11, 2010, pp. 3807-3813. doi:10.1109/TIE.2010.2040560
- [7] Z. Chen, Y. Sun and Y. Yan, "Static Characteristics of A Novel Hybrid Excitation Doubly Salient Machine," *Proceedings of the Eight International Conference on Electrical Machines and Systems*, Nanjing, 27-29 September 2005, pp. 718-721.
- [8] K. T. Chau, J. Z. Jiang and W. Yong, "A Novel Stator Doubly Fed Doubly Salient Permanent Magnet Brushless Machine," *IEEE Transactions on Magnetics*, Vol. 39, No. 5, 2003, pp. 3001-3003. doi:10.1109/TMAG.2003.816722
- [9] Y. Amara, L. Vido, M. Gabsi, E. Hoang, A. H. Ben Ahmed and M. Lecrivain, "Hybrid Excitation Synchronous Machines: Energy-Efficient Solution for Vehicles Propulsion," *IEEE Transactions on Vehicular Technology*, Vol. 58, No. 5, 2009, pp. 2137-2149. doi:10.1109/TVT.2008.2009306
- [10] D. Fodorean, A. Djerdir, I. A. Viorel and A. Miraoui, "A Double Excited Synchronous Machine for Direct Drive

- Application-Design and Prototype Tests,” *IEEE Transactions on Energy Conversion*, Vol. 22, No. 3, 2007, pp. 656-665. [doi:10.1109/TEC.2007.896279](https://doi.org/10.1109/TEC.2007.896279)
- [11] E. Sulaiman, T. Kosaka and N. Matsui, “Design Improvement and Performance Analysis of 12S-10P Permanent Magnet Flux Switching Machine with Field Excitation Coil,” *Journal of Electrical System*, Vol. 8, No. 4, 2012, pp. 425-432. [doi:10.1109/TIA.2003.818993](https://doi.org/10.1109/TIA.2003.818993)
- [12] H. Wei, M. Cheng and G. Zhang, “A Novel Hybrid Excitation Flux-Switching Motor for Hybrid Vehicles,” *IEEE Transactions on Magnetics*, Vol. 45, No. 10, 2009, pp. 4728-4731. [doi:10.1109/TMAG.2009.2022497](https://doi.org/10.1109/TMAG.2009.2022497)
- [13] E. Hoang, M. Lecrivain and M. Gabsi, “A New Structure of a Switching Flux Synchronous Polyphased Machine with Hybrid Excitation,” *Proceedings of European Conference on Power Electronics and Applications*, Aalborg, 2-5 September 2007, pp. 1-8. [doi:10.1109/EPE.2007.4417204](https://doi.org/10.1109/EPE.2007.4417204)
- [14] E. Sulaiman, T. Kosaka and N. Matsui, “Design Optimization and Performance of A Novel 6-Slot 5-Pole PMFSM with Hybrid Excitation for Hybrid Electric Vehicle,” *IEEJ Transactions on Industry Applications*, Vol. 132, No. 2, 2011, pp. 211-218.
- [15] A. Zulu, B. C. Mecrow and M. Armstrong, “A Wound-Field Three-Phase Flux-Switching Synchronous Motor with All Excitation Sources on The Stator,” *IEEE Transactions on Industry Applications*, Vol. 46, No. 6, 2010, pp. 2363-2371. [doi:10.1109/TIA.2010.2072972](https://doi.org/10.1109/TIA.2010.2072972)
- [16] E. Sulaiman, T. Kosaka and N. Matsui, “High Power Density Design of 6Slot-8Pole Hybrid Excitation Flux Switching Machine for Hybrid Electric Vehicle,” *IEEE Transactions on Magnetics*, Vol. 47, No. 10, 2011 pp. 4453-4456. [doi:10.1109/TMAG.2011.2140315](https://doi.org/10.1109/TMAG.2011.2140315)
- [17] M. Kamiya, “Development of Traction Drive Motors for the Toyota Hybrid Systems,” *IEEJ Transactions on Industry Applications*, Vol. 126, No. 4, 2006, pp. 473-479.