

Optimal Control for Time-Delay Bilinear Systems with Sinusoidal Disturbances^{*}

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ABSTRACT

This paper considers the optimal control problem for time-delay bilinear systems affected by sinusoidal disturbances with known frequency and measurable amplitude and phase. Firstly, using the differential homeomorphism, a time-delay bilinear system affected by sinusoidal disturbances is changed to a time-delay pseudo linear system through the coordinate transformation. Then the system with time-delay in control variable is transformed to a linear controllable system without delay using model transformation. At last based on the theory of linear quadratic optimal control, an optimal control law which is used to eliminate the influence of the disturbances is derived from a Riccati equation and Matrix equations. The simulation results show the effectiveness of the method.

Keywords: Time-Delay Bilinear System; Feedback Linearization; Sinusoidal Disturbances; Optimal Control

1. Introduction

Bilinear system is a class of systems that is derived by introducing the interactive product term of the state variable and the control variable in the linear state equations. It is a rather special nonlinear system, which exists widely in the engineering community of electric, mechanical, biological, chemical and other fields. The study of the bilinear system starts in the 50's, then becomes an important branch of nonlinear system and made a series of research results. Fang proposed a method of research the stability of MIMO bilinear system [1]; the output-feedback control for bilinear system was studied by Sasaki [2]; a global feedback stability analysis method of bilinear system was presented by Jerbi [3]. In the real Industrial process control, time-delay is ubiquity and the mathematical models put forward from engineering technology, physical, chemical and biomedical had obvious delay amount, which can not be neglected in some accurate control systems. Tang had studied optimal disturbance rejection problem for time-delay system in recent years [4]. Meanwhile, various forms of external disturbances exist on the control system, such as sinusoidal disturbance, periodic perturbation, step disturbance, etc. So it has important actual meanings to study time-delay bilinear system affected by external disturbance [5].

This paper proposed an optimal control design method for time-delay bilinear systems affected by sinusoidal disturbances based on state-feedback linearization [6,7]. Based on the differential homeomorphism, the model of the system that is researched is changed to a time-delay pseudo linear system through the coordinate transition, then through delay-free transform, the time-delay pseudo linear system is converted to an easy pseudo linear system. At last, an optimal control law which is used to eliminate the influence of the disturbances is derived from a Riccati equation and Matrix equations [8,9]. It is shown that the method is easy to realize and has a good convergence.

2. Problem Statement

Consider time-delay bilinear system affected by sinusoidal disturbances

$$\dot{x}(t) = Ax(t) + \{Nx(t)\}u(t-\tau) + Bu(t-\tau) + Dv(t)$$

$$x(0) = x_0, \quad \{Nx(t)\} = \sum_{j=1}^n N_j x_j(t)$$
(1)

$$y = h(x)$$

where, $x \in \mathbb{R}^n$ is the state vector; u(t) is the control vector; $v \in \mathbb{R}^p$ is the external disturbances vector; y(t) is the output vector; A, B, D, N_j are scalar matrixes of appropriate dimensions; x_j is the *j*-th component of state vector; $\{Nx\}u$ is the bilinear term; h(x) is the scalar function of *x*.

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Assumption 1 The external disturbances can be expressed as

$$v(t) = \begin{bmatrix} v_1(t) \\ v_2(t) \\ \vdots \\ v_p(t) \end{bmatrix} = \begin{bmatrix} \alpha_1 \sin(\omega_1 t + \varphi_1) \\ \alpha_2 \sin(\omega_2 t + \varphi_2) \\ \vdots \\ \alpha_p \sin(\omega_p t + \varphi_p) \end{bmatrix}$$
(2)

which is an *m*-dimensional sinusoidal vector with known frequencies $-\pi < \omega_1 \le \omega_2 \le \cdots \le \omega_p \le \pi$, amplitudes $\alpha_1, \alpha_2, \cdots, \alpha_m$ and phases $\varphi_1, \varphi_2, \cdots, \varphi_m$ are measurable. By transformation, time-delay bilinear system could be changed as

$$\dot{x} = Ax + \left(\{Nx\} + B\right)u(t - \tau) + Dv \tag{3}$$

Change the bilinear system to the general expression of nonlinear system

$$\dot{x} = f(x) + g(x)u(t-\tau) + Dv(t) \quad y = h(x)$$
(4)

where, f(x) = Ax, $g(x) = \{Nx\} + B$ and j, g are continuously differentiable functions.

Assumption 2 The relation degree of the nonlinear system is *r*, that is

$$L_{g}L_{f}^{i-1}h(x) = 0 \quad i = 1, 2, \cdots, r-1 \quad L_{g}L_{f}^{r-1}h(x) = m \quad (5)$$

Through exact delay-free transformation, the nonlinear system (4) can be converted to an easy pseudo linear system (6)

$$\dot{\eta} = A\eta(t) + Bu(t) + D_1v(t) \tag{6}$$

 $\eta = [\eta_1 \quad \eta_2 \quad \cdots \quad \eta_r]^{\mathrm{T}}$ is the new state vector.

$$A_{1} = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 & 0 \\ 0 & 0 & 1 & \cdots & 0 & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & 0 & \cdots & 0 & 1 \\ 0 & 0 & 0 & \cdots & 0 & 0 \end{bmatrix} \quad B_{1} = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix} \quad D_{1} = \begin{bmatrix} d_{1} \\ d_{2} \\ \vdots \\ d_{r-1} \\ d_{r} \end{bmatrix}$$

Then based on the theory of linear quadratic optimal control, an optimal control law which is used to eliminate the influence of the disturbances is derived.

3. Exact Delay-Free Linearization

3.1. State Feedback Linearization

State Feedback Linearization is a method of nonlinear controlling design, the design idea of which is to select a coordinate transformation $z = \phi(x)$ and made a mapping from x coordinate space to z coordinate space, thus the nonlinear system is changed to a linear time-invariant system as $\dot{z} = Az + Bv$. Let

$$z = \phi(x) = \begin{bmatrix} h(x) \\ L_f h(x) \\ \vdots \\ L_f^{-1} h(x) \end{bmatrix}$$
(7)

 $\phi(x)$ is the partial differential homeomorphism, according to assumption 2, then get

$$z_{i} = L_{f}^{i-1}h(x) \quad i = 1, 2, \cdots, r$$

$$L_{f}^{r}h(x) = \sum_{i=1}^{r} c_{i}L_{f}^{i-1}h(x) \qquad (8)$$

$$L_{D}L_{f}^{i-1}h(x) = d_{i} \quad i = 1, 2, \cdots, r$$

by operation, the system is changed to a new standard form

(

$$\begin{cases} \dot{z}_{1} = z_{2} + d_{1}v(t) \\ \dot{z}_{2} = z_{3} + d_{2}v(t) \\ \vdots \\ \dot{z}_{r-1} = z_{r} + d_{r-1}v(t) \\ \dot{z}_{r} = \sum_{i=1}^{r} c_{i}z_{i} + mu(t-\tau) + d_{r}v(t) \end{cases}$$

$$(9)$$

r-step time-delay linear system with disturbances can be obtained as follow

$$\dot{z} = Az + B_1 u \left(t - \tau \right) + D_1 v \left(t \right) \tag{10}$$

where

$$A = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 & 0 \\ 0 & 0 & 1 & \cdots & 0 & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & 0 & \cdots & 0 & 1 \\ c_1 & c_2 & c_3 & \cdots & c_{r-1} & c_r \end{bmatrix}$$
$$z = \begin{bmatrix} z_1 \\ z_2 \\ \vdots \\ z_{r-1} \\ z_r \end{bmatrix} \quad B_1 = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ m \end{bmatrix} \quad D_1 = \begin{bmatrix} d_1 \\ d_2 \\ \vdots \\ d_{r-1} \\ d_r \end{bmatrix}$$

3.2. Exact Delay-Free Transformation

Definite transformation for the time-delay linear system, let

$$\eta(t) = z(t) + \int_{t-\tau}^{t} e^{A(t-\sigma)} Bu(\sigma) d\sigma$$
(11)

The expression (10) is converted to delay-free system

$$\dot{\eta} = A\eta(t) + Bu(t) + D_1v(t) \qquad \eta(0) = \eta_0 \qquad (12)$$

where $B = e^{-A\tau} B_1$.

4. Design of Optimal Control

The time-delay bilinear system (1) is changed to the equivalent delay-free linear system affected by disturbances

$$\dot{\eta} = A\eta(t) + Bu(t) + D_1v(t) \tag{13}$$

where, $\eta \in \mathbb{R}^n$ is the new state vector; $u \in \mathbb{R}^m$ is the new control vector; A is state coefficient matrix; B is control coefficient matrix; the system (6) is completely controllable.

When $t \rightarrow \infty$ select the quadratic performance index of system (6) as

$$J = \frac{1}{2} \int_{0}^{\infty} \left(\eta^{\mathrm{T}} Q \eta + u^{\mathrm{T}} R u \right) \mathrm{d}t$$
 (14)

where Q is a $n \times n$ positive semi-definite matrix, R is a $m \times m$ positive definite symmetric matrix.

Theorem: Consider the optimal control problem of system (6) with the quadratic performance index (14). Suppose the system is completely controllable and observable, the optimal disturbance rejection control law is unique existence and can be expressed as

$$u^{*}(t) = -R^{-1}B^{T} \left[P\eta(t) + P_{1}v(t) + P_{2}v_{m}(t) \right]$$
(15)

P is the unique positive definite solution of the matrix Equation (16)

$$A^{\mathrm{T}}P + PA - PSP + Q = 0 \tag{16}$$

 P_1 is the unique solution of the matrix Equation (17)

$$A^{\rm T} P_1 + PD - P_2 \Omega^2 - PSP_1 = 0$$
 (17)

 P_2 is the unique solution of the matrix Equation (18)

$$A^{\rm T}P_2 + P_1 - PSP_2 = 0 \tag{18}$$

where

$$S = BR^{-1}B^{T}$$
$$v_{m}(t) = \dot{v}(t)$$
$$\Omega = \text{Diag}(w_{1}, w_{2}, \dots, w_{p})$$

Proof: According to the necessary conditions of the optimal control problem based on maximum principle, the optimal control law of system (6) with the quadratic performance index (14) can be expressed as

$$u^*(t) = -R^{-1}B^{\mathrm{T}}\lambda(t) \tag{19}$$

where $\lambda(t)$ is the solution of the following two-point boundary value problem

$$-\dot{\lambda}(t) = Q\eta(t) + A^{\mathrm{T}}\lambda(t)$$

$$\dot{\eta}(t) = A\eta(t) + Bu(t) + D_{1}v(t), t > 0 \qquad (20)$$

$$\eta(0) = \eta_{0}, \quad \lambda(\infty) = 0$$

In order to obtain the solution to the problem in (14),

let

$$\lambda(t) = P\eta(t) + P_1 v(t) + P_2 v_m(t)$$
(21)

where $P \in \mathbb{R}^{n \times n}$, $P_1, P_2 \in \mathbb{R}^{n \times p}$ are both undetermined matrix.

From expression (2), the vector function v(t) satisfies the following vector differential equation

$$\dot{v}(t) = v_m(t) = \begin{bmatrix} v_1(t) \\ v_2(t) \\ \vdots \\ v_p(t) \end{bmatrix} = \begin{bmatrix} w_1 \alpha_1 \cos(\omega_1 t + \varphi_1) \\ w_2 \alpha_2 \cos(\omega_2 t + \varphi_2) \\ \vdots \\ w_p \alpha_p \cos(\omega_p t + \varphi_p) \end{bmatrix}$$
(22)
$$\ddot{v}(t) = \dot{v}_m(t) = \begin{bmatrix} -\omega_1^2 \alpha_1 \sin(\omega_1 t + \varphi_1) \\ -\omega_2^2 \alpha_2 \sin(\omega_2 t + \varphi_2) \\ \vdots \\ -\omega_p^2 \alpha_p \sin(\omega_p t + \varphi_p) \end{bmatrix} = -\Omega^2 v(t)$$

Taking the derivatives to the sides in (21) and substituting (22) into it get (23)

$$\dot{\lambda}(t) = P\dot{\eta}(t) + P_{1}\dot{v}(t) + P_{2}v_{m}(t) = PA\eta(t) + PBu(t) + (PD - \Omega^{2}P_{2})v(t) + P_{1}v_{m}(t)^{(23)}$$

Add (23) into the first expression of (20), obtain (24)

$$(A^{T}P + PA - PSP + Q)\eta(t) + (A^{T}P_{1} + PD) -P_{2}\Omega^{2} - PSP_{1})v(t) + (A^{T}P_{2} + P_{1} - PSP_{2})v_{m}(t) = 0$$
(24)

Considering for any $\eta(t), v(t)$ and $v_m(t)$, Equation (24) is all hold, so we can get matrix Equations (16)-(18). The optimal control law of the bilinear systems affected by sinusoidal disturbances is as follow

$$u^{*}(t) = -R^{-1}B^{\mathrm{T}}\left[P\eta(t) + P_{1}v(t) + P_{2}v_{m}(t)\right]$$
$$= -R^{-1}B^{\mathrm{T}}P\left[z(t) + \int_{t-\tau}^{t} e^{A(t-\sigma)}Bu(\sigma)d\sigma\right] \quad (25)$$
$$+ P_{1}v(t) + P_{2}v_{m}(t)$$

5. Simulation Example

Consider a time-delay bilinear system with sinusoidal disturbances, system parameters as follows

$$\dot{x} = Ax + \{Nx\}u(t-0.2) + Bu(t-0.2) + Dv(t)$$

$$y = x_{2}$$

$$\begin{bmatrix} 1 & 1 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 \end{bmatrix} \begin{bmatrix} 1 & 1 \end{bmatrix}$$
(26)

$$A = \begin{bmatrix} 0 & 0 & 1 \\ 0 & -1 & 0 \end{bmatrix} N = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} B = \begin{bmatrix} 0 \\ 1 \end{bmatrix} D = \begin{bmatrix} 2 & 0 \\ 1 & 0 \end{bmatrix}$$

According to calculation r = 2, through local linearization, we can get a two-step linear system affected by sinusoidal disturbances

$$\dot{z} = Az + B_1 u (t - 0.2) + D_1 v (t)$$
(27)

where

$$A = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} \quad B_1 = \begin{bmatrix} 0 \\ 1 \end{bmatrix} \quad D_1 = \begin{bmatrix} 2 & 0 \\ 1 & 1 \end{bmatrix}$$

The form of the disturbances described as follows

$$v(t) = \begin{bmatrix} \frac{1}{2}\sin\left(\frac{4}{5}t\right) \\ \frac{1}{3}\sin\left(t + \frac{1}{4}\pi\right) \end{bmatrix}$$
(28)

Using model transformation, change the system with time-delay to a linear controllable system without delay

$$\dot{\eta} = A\eta(t) + Bu(t) + D_1v(t)$$
⁽²⁹⁾

where
$$A = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}$$
, $B = e^{-A\tau} B_1$.
Select $R = 1.0$, $Q = \text{diag}(1,1)$, we get
 $P = \begin{bmatrix} 1.2872 & 0.4142 \\ 0.4142 & 0.9102 \end{bmatrix}$

The simulation results of $x_1(t)$, $x_2(t)$ and $u^*(t)$ are presented in **Figures 1** and **2**.

It is shown that the optimal control design method for the system affected by sinusoidal disturbances based on state-feedback linearization is easily realized, and has a good convergence through the simulation results.

6. Conclusion

This paper concentrates on the solution of the optimal control problem for time-delay bilinear system affected by sinusoidal disturbances with known frequency and measurable amplitude and phase based on state feedback, a method of optimal control law is given. Simulation re-



Figure 1. The diagram of state variables $x_1(t), x_2(t)$.



Figure 2. The diagram of the optimal control $u^*(t)$.

sults show that the designed control law is accurate and easy to implement.

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