Evaluating the Influence of Ageing Temperature on the Mechanical Properties of Al-Mg-Si Alloy

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Abstract

The effect of ageing temperature on the mechanical properties of Al-Mg-Si alloy has been studied. The material was machined into different shapes of the tests to be carried out: tensile, impact and hardness. The test specimens were divided into two and, some sets were solution treated at 500° C for one hour and peak aged at 160° C for eight hours while the other sets were solution treated at 500° C for one hour and peak aged at 180° C for eight hours. The above-mentioned tests were carried out on the specimens. The results show that at low ageing temperature of 160° C, the ductility and impact were high while at 180° C, the ultimate tensile strength and hardness are higher compared to the value obtained at 160° C.

Keyword: Ageing temperature, mechanical properties, solution treated, specimen.

1. INTRODUCTION

Aluminium does not have good casting or mechanical properties. These properties can be achieved by adding magnesium and silicon to aluminium. The addition of these alloying elements increases the aluminium response to heat treatment due to formation of Mg_2Si intermetallic compound, which improves the casting, corrosion resistance property as well as the strength of the alloy. This alloy is named as the 6063 aluminium alloy. Al+Mg+Si alloy is also known as architectural and decorative alloy; because of its easy extrudability property, distinctly superior fnishing quality and strength. Almost half of all the aluminium extrusions produced in UK are used in building [1].

Structural medium strength aluminum alloys based on the Al-Mg-Si system have been popular for a wide range of applications for a long time. These alloys are widely used for decorative, architectural and structural applications. The development of Al-Mg–Si alloys for light structures has led to an increasing market for extrusions of intricate shape, medium strength and good toughness. These alloys are required to meet specific tensile properties and good fatigue strength, welding characteristics and formability [2]. Alloys based on the Al-Mg-Si-Cu system are widely

used as medium strength alloys with major applications in extruded products and automotive body sheet.

AA6061 is one of the most widely used alloys from this group and optima mechanical properties are achieved by aging in the temperature range from 175° C to 180° C for 10 to 20 hours after solution treatment and quenching [3].

Heat treatment encompasses all operations of controlled heating and cooling of metals and their alloys in the solid state for the purpose of changing their structure and consequently their properties [4]. The common heat treatment operation for aluminum alloys is called ageing. This is the method of precipitating from solid solution a metastable phase that leads to change in properties of the alloy [5-6].

Nowadays, age hardened Al–Mg–Si alloys are widely used in construction and automotive industries. These alloys have been studied extensively for their exceptional increase in strength obtained by precipitation hardening. In order to control the precipitate distributions for these alloys, it is important to select proper silicon and magnesium contents, and also proper aging conditions [7]. This work was carried out to investigate the effect of ageing temperature on the mechanical properties of Al-Mg-Si alloy at the chosen temperatures.

2. EXPERIMENTAL PROCEDURE

Al-Mg-Si alloy with the following chemical composition as shown in Table 1 was used in this work.

Elements	Al	Mg	Si	Fe	Mn	Cu	Cr	Ti	Ca	Sr
Compositi	98.663	0.432	0.362	0.046	0.151	0.003	0.002	0.006	0.01	0.015
on	1	1	5	9	6	6	6	2	1	6

Table 1.	Chemical Composition	n of the Aluminum	Alloy Sample (in wt %).

The material was machine into the shapes of the tests to be carried out on the lathe machine from where tensile and impact specimens were produced. Ten specimens were prepared for tensile test while six specimens were prepared for impact and hardness tests each. These specimens were subjected to two different heat treatment conditions. The first sets were subjected to solution treatment at 500° C for one hour, quenched in water and peak aged at 160° C for eight hours before finally quenched in water. The other sets were subjected to solution treatment at 500° C for one hour, quenched at 180° C for eight hours before finally quenched in water and peak aged at 180° C for eight hours before finally quenched in water and peak aged at 180° C for eight hours before finally quenched in water and peak aged at 180° C for eight hours before finally quenched in water and peak aged at 180° C for eight hours before finally quenched in water and peak aged at 180° C for eight hours before finally quenched in water and peak aged at 180° C for eight hours before finally quenched in water and peak aged at 180° C for eight hours before finally quenched in water and peak aged at 180° C for eight hours before finally quenched in water. The following tests were carried out on the specimens.

2.1. Tensile Test

The specimen was clamped to the teeth of the tensiometer and load was gradually applied manually. The value of the applied load was indicated by the pointer in the mercury bulb. The effect of this load was also displayed on the graph sheet that was fixed at one end of the machine. The applied load stopped immediately the specimen breaks and the graph show the relation

between the load and the extension produced. The percentage elongation was determined from the specimen with the use of vernier caliper.

2.2. Impact Test

The test was carried out by placing the specimen on the anvil of the pendulum of a charpy impact testing machine and the load was apply suddenly by the failing pendulum. As the pendulum swings past, it carries a pointer to its highest point of swing thus, indicating the amount of energy used in fracturing the test piece.

2.3. Hardness Test

The Rockwell hardness scale B testing machine with hardened steel ball as the indenter was used. A force was applied to press the indenter in contact with the surface followed by another force that causes an increase in depth of the indenter penetration into the material. The calibrated dial scale read the hardness value of the material obtained by counseling the minor load before applying the major load.

2.4. Metallographic Analysis

The prepared specimen surfaces were smoothened by grinding with the modern hand grinding deck using emery paper of progressive finer grades 220, 230, 400 and 600. They were polished with polishing machine using fine alumina as the polishing powder to obtain a mirror like surface. The polishing disk was covered by solvyt cloth and there was constant supply of water as lubricant. The sample were etched using freshly prepared dilute hydrofluoric acid [50cm³ NH₃ (OH)₄ and 50cm³ H₂0] as enchants. The surfaces were observed under the microscope and their photograph's taken with magnification x 100.

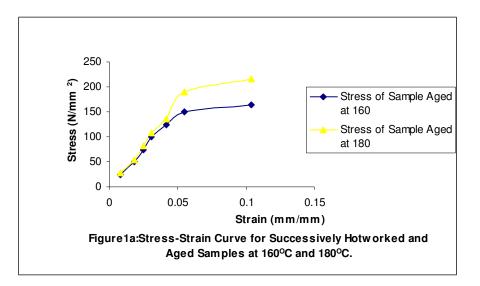
3. RESULTS AND DISCUSSION

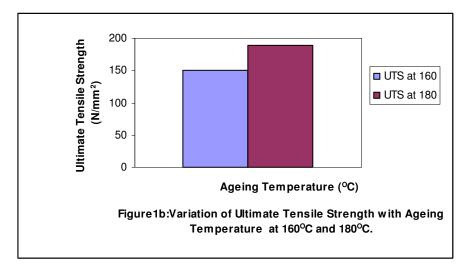
3.1. Influence of Ageing Temperature on the Ultimate Tensile Strength of Al- Mg-Si alloy.

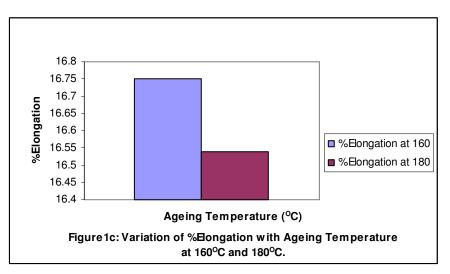
Ultimate tensile strength is the stress attained at the highest applied force before necking in ductile metals [8-9] like aluminium. Figures 1 (a) and (b) show that specimen aged at 160° C has 149.85N/mm² UTS while specimen aged at 180° C has 189.70N/mm².

Ductility and yield strength are some of the variables that are used to measure the UTS of a metal.

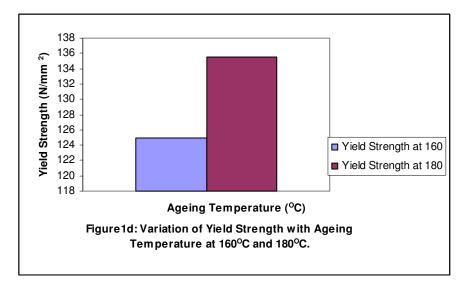
Ductility is the measure of the amount of deformation a material can withstand without breaking. This is determined by the percentage elongation values as shown in Figure 1(c). Specimen aged at 160° C has 16.75% elongation while specimen aged at 180° C has 16.54% elongation.





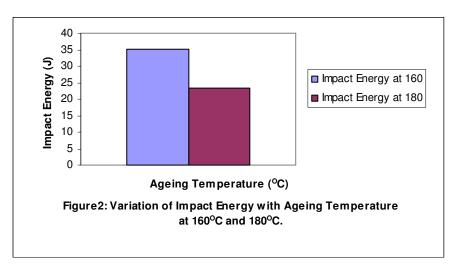


Yield strength is the stress at which plastic deformation become noticeable. It is the stress required for dislocation to slip and it is the stress that divides the elastic and plastic behaviour of metal. In aluminium and its alloys, this stress is not easily detected and 0.2% proof stress is used to determine the offset of yield strength. It was determined from Figure 1 (d) that, the yield strength of specimen aged at 160° C is 124.87N/mm² while specimen aged at 180° C has 189.70N/mm². From the results; it was observed that specimen aged at 180° C has improved strength than specimen aged at 160° C.



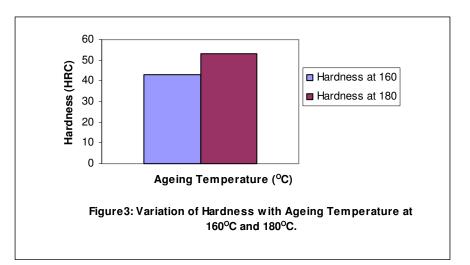
3.2. Influence of Ageing Temperature on the Impact Energy of Al-Mg-Si alloy.

Impact test is often used to evaluate the brittleness of a material under a sudden intense blow in which the strain rate is extremely rapid. Specimen aged at 160° C absorbed more energy (35.03J) before fracture than specimen aged at 180° C that absorbed (23.23J) as a result of high ductility experienced by specimen aged at 160° C. This was shown in Figure 2.



3.3. Influence of Ageing Temperature on the Hardness of Al-Mg-Si alloy.

Hardness test measure the resistance of the surface of a material to penetration or indentation. Figure 3 show the response of the specimens to hardness at 160° C and 180° C. Specimen aged at 180° C has high hardness of 53HRB than specimen aged at 160° C that has 43HRB as a result of improved strength of the specimen.



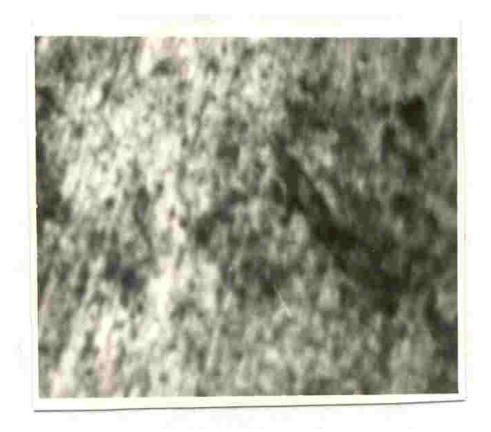


Figure 4. Microstructure of Sample Treated at 160 ^OC. Magnifications (x100)

The microstructure revealed the response of the aluminium alloy to heat treatment due to formation of Mg_2Si intermetallic compound (black). The revealed structure in Figure 4 shows a clumsy precipitate of the Mg_2Si intermetallic compound in Al-Matrix at the right side of the Figure.

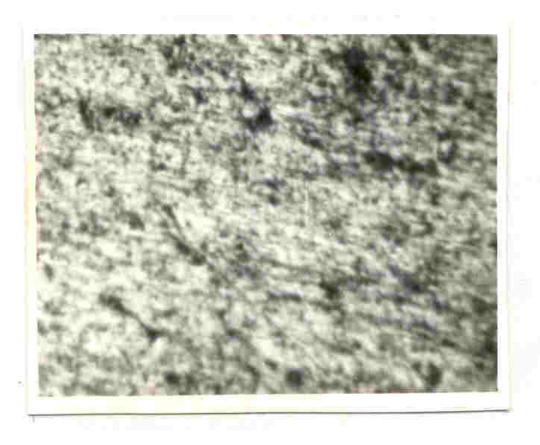


Figure 5. Microstructure of Sample Treated at 180 ^oC. Magnifications (x100)

Figure 5 show the response of the aluminium alloy to heat treatment at the microstructural point of view due to formation of Mg₂Si intermetallic compound. The revealed structure in Figure 5 shows a well dispersed precipitate of the Mg₂Si intermetallic compound (black) in Al- Matrix (white) compared to what was observed in Figure 4. This was responsible for the improved properties for the sample compared to the sample that was treated at 160 $^{\circ}$ C.

4. CONCLUSION

It has been observed that ageing temperature influence the precipitation of Mg₂Si intermetallic compound in Al-Mg-Si alloy and hence, its microstructures as shown in Figures 4 and 5. Since the structure of a material determines its properties, which invariably determine its application. Proper attention must be given to the ageing temperature when the strength of the material is to be improved. Ageing at 180° C for 8hrs enhance uniform dispersal of the Mg₂Si intermetallic compound precipitate in solid solution strengthening techniques and, hence, better mechanical properties than what obtains at 160° C.

The results have shown that percentage elongation and impact energy decreases with increase in ageing temperature while ultimate tensile strength, yield strength and hardness increases with increase in ageing temperature.

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