

Mixed Convection MHD Stagnation Point Flow over a Stretching Surface with the Effects of Heat Source or Sink and Viscous Dissipation

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Abstract

The present study deals with MHD mixed convection stagnation point flow over a stretching sheet with the effects of heat source/sink and viscous dissipation including convective boundary conditions. The governing partial differential equations are transformed into ordinary differential equations by applying similarity transformations. These equations are then solved numerically by using finite difference scheme known as the Keller Box method. The effects of various parameters on velocity and temperature profiles are presented graphically interpreted and the results are discussed.

Keywords

Magnetohydrodynamics (MHD), Mixed Convection, Stagnation Point, Heat Source, Viscous Dissipation

1. Introduction

The study of MHD, boundary layer flow with heat transfer from a stretching sheet has several applications in many industrial fields. Magnetic fields can be used to manage thermal energy in flowing electrically conducting polymers (Garnier [1]). Crane [2] first investigated the flow of an incompressible fluid over a linearly stretching sheet. Boundary layer flow behaviour on continuous solid surface moving at a constant speed is investigated by Sakiadas [3]. Chakrabarthi and Gupta [4] discussed heat transfer of hydromagnetic flow over a stretching sheet. Heat transfer over a continuous, stretching surface with suction/blowing is investigated by Chen and Char [5]. T.

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C. Chiam [6] explained heat transfer in a two-dimensional fluid over a linearly stretching sheet in the presence of suction/blowing and with variable thermal conductivity.

In fluid dynamics, the stagnation point flow and flow over a stretching surface are important in theoretical and applications point of view. In fluid dynamics, stagnation is a point in a flow field where the local velocity of the fluid is zero. Stagnation points exist at the surface of objects in the flow field, where the fluid is brought to rest by the object. Stagnation flow towards a stretching sheet is investigated by Wang [7]. Mixed convection MHD stagnation point flow on vertical, linearly stretching sheet is explained by Ishak [8]-[10]. The steady two-dimensional stagnation point flow on a stretching sheet was first discussed by Chaim [11]. Stagnation point flow over a stretching surface is explained by T. R. Mahapatra and A. S. Gupta [12]. Recently Bhattacharya [13] investigated heat transfer in boundary layer stagnation point flow over a stretching sheet. In many electronic applications, temperature becomes an important role when designing a system. We have practical applications for various heat source/sink arrangements. An effect of heat source/sink on MHD flow over a shrinking sheet is explained by Krishnendu Bhattacharyya [14]. F. M. Hady [15] described the effects of heat source/sink on MHD viscoelastic fluid over a non linear stretching sheet. Mahapatra, T. R. and A. S. Gupta [16] discussed heat transfer in stagnation point flow over a stretching sheet. The effects of viscous dissipation and internal heat generation of a viscous fluid on a stretching sheet are investigated by Vajravelu K. and Hadjinicolaou A. [17]. Sharma P. R. and Singh G. [18] described the effects of viscous dissipation and heat source/sink on MHD stagnation point flow over a linearly stretching sheet.

This paper provides the solution to the problem of fluid flow, heat transfer of mixed convection MHD stagnation point flow over a stretching surface by considering the effects of heat source/sink and viscous dissipation including convective boundary conditions by adopting the Keller box method.

2. Mathematical Formulation

Consider two-dimensional steady, incompressible MHD stagnation point flow of a viscous fluid over a stretching sheet with convective boundary condition. It is assumed that the stretching velocity $u_w(x)$ and the external velocity U(x) are of the forms $u_w(x) = bx$, U(x) = ax respectively, where a, b are constants. A magnetic field of uniform strength B is applied perpendicular to the surface in the y direction, which generates magnetic field in the x direction. A heat source/sink is located within the flow to allow for certain heat generation or absorption effects.

Considering u, v as velocity components in the directions of x and y respectively in the flow field. The governing equations of continuity, momentum, energy and concentration are given by

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \tag{1}$$

$$u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = U\frac{\mathrm{d}U}{\mathrm{d}x} + v\frac{\partial^2 u}{\partial y^2} + g\beta_T \left(T - T_{\infty}\right) - \frac{\sigma B^2}{\rho} \left(u - U\right)$$
(2)

$$u\frac{\partial T}{\partial x} + v\frac{\partial T}{\partial y} = \alpha \frac{\partial^2 T}{\partial y^2} + Q\left(T - T_{\infty}\right) + \frac{\mu}{\rho C_p} \left(\frac{\partial u}{\partial y}\right)^2$$
(3)

where ρ is the density of the fluid, σ is the electrical conductivity, v is the kinematic viscosity, *B* is the magnetic induction, $\alpha \left(=\frac{K}{\rho C_p}\right)$ is the thermal diffusivity, *K* is the thermal conductivity, μ is the dynamic

co-efficient of viscosity, C_p is the specific heat capacity at constant pressure, T_{∞} is the free stream temperature, Q is the volumetric rate of heat source or sink diffusion ratio. The boundary conditions considered are defined as

$$u = u_w(x) = bx, \quad v = 0, \quad -K \frac{\partial T}{\partial y}(x,0) = h_f(T_f - T(x,0)) \text{ at } y = 0.$$
$$u = U(x), \quad T \to T_{\infty} \text{ as } y \to \infty$$

where T_f is the temperature of fluid, h_f is the heat transfer coefficient.

Introducing the similarity transformations

$$\eta = \sqrt{\frac{U}{\upsilon x}} y, \quad \psi(x) = \sqrt{\upsilon x U} f'(\eta), \quad \theta(\eta) = \frac{T - T_{\infty}}{T_{W} - T_{\infty}}$$

 $u = axf'(\eta), \quad v = -\sqrt{av} \left[f(\eta) - \eta f'(\eta) \right] \text{ into the Equations (2) & (3) we get}$ $f''' + ff'' - (f')^2 - M(f'-1) + \lambda\theta + 1 = 0,$

$$f''' + ff'' - (f')^2 - M(f'-1) + \lambda\theta + 1 = 0,$$
(4)

$$\frac{1}{Pr}\theta'' + f\theta' + S\theta + Ec(f'')^2 = 0$$
⁽⁵⁾

where $M = \frac{\sigma B_0^2}{\rho a}$ is the magnetic parameter, $Pr = \frac{v}{\alpha}$ is the Prandtl number, $\lambda = \frac{Gr}{Re^2}$ is the mixed convec-

tion parameter, $Re = \frac{Ux}{V}$ is the Reynolds number, $Gr = \frac{g\beta_T (T - T_{\infty})x^3}{V^2}$ is the Grashoff number,

 $Ec = \frac{a^2}{C_n(T_c - T_c)}$ is the Eckert number, $S = \frac{Q}{a}$ is the heat generation parameter.

The boundary conditions are reduced to

$$\eta = 0: f(0) = 0, f'(0) = \epsilon, \theta'(0) = -\gamma (1 - \theta(0))$$
$$\eta \to \infty: f'(\infty) = 1, \theta(\infty) = 0$$

where $\epsilon = \left(\frac{b}{a}\right) \ge 0$ is the stretching parameter and $\gamma = \left\{\frac{h_f}{K}\left(\sqrt{\frac{\nu}{a}}\right)\right\}$ is the conjugate parameter for the con-

vective boundary condition. The skin friction coefficient at the surface of the sheet is given by $C_f = \frac{2\tau_w}{\sigma L^2}$

$$\begin{bmatrix} C_f R e^{1/2} = -f''(0) \end{bmatrix}, \text{ where } \tau_w = -\mu \left(\frac{\partial u}{\partial y}\right)_{y=0} \text{ is the shear stress, } Nu_x = \frac{xq_w}{k(T_w - T_\infty)} \quad \left[Nu_x = -Re^{1/2}\theta'(0) \right] \text{ is the Nusselt number, where } q_w = -K \left(\frac{\partial T}{\partial y}\right)_{y=0} \text{ is the rate of heat transfer.}$$

3. Method of Solution

The governing equations with boundary equations are solved numerically by using finite difference scheme known as Keller box method which is described by Cebeci and Bradshaw [19]. This method involves the following steps.

Step 1: Reducing higher order ODEs (systems of ODES) in to systems of first order ODEs.

Step 2: Writing the systems of first order ODEs into difference equations using central difference scheme.

Step 3: Linearizing the difference equations using Newton's method and writing it in Vector form.

Step 4: Solving the system of equations using block elimination method.

4. Numerical Discussions

In this process the step size $\Delta \eta = 0.01$ is used to obtain numerical solution. Table 1 shows that the comparison between the present results with the previously described results by Wang, Yacob and Ishak for various values of the stretching parameter ϵ . It has been found that they are in good agreement.

5. Results and Discussion

In this study, the following values are used for the numerical computations M = 0.05, S = 0.5, $\lambda = 0.1$,

Pr = 0.72, $\gamma = 0.1$, $\epsilon = 2.0$, Ec = 0.1. These values are mentioned throughout the computations unless otherwise stated.

Figure 1 illustrates the velocity profile for different values of the magnetic parameter *M*. As The value of *M* increases, velocity decreases due to Lorentz force. **Figure 2** shows that the velocity profile for different values of mixed convection parameter λ . It illustrates that the dimensionless velocity increases, as the value of λ increases. As λ increases, the buoyancy effects increase and hence the fluid flow accelerates (**Table 2**).

Figure 3 depicts the effects of ϵ on dimensionless velocity profiles, which produce $f'(0) = \epsilon$ and $f'(\infty) = 1$. When $\epsilon > 1$, the flow has an inverted boundary layer structure and the thickness of the boundary layer decreases with ϵ . On the other hand, when $\epsilon < 1$, the flow has a boundary layer structure, which results from the fact that when $\frac{b}{a} < 1$, the external velocity ax of the surface exceeds the velocity bx of the stretching

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e	Yacob and Ishak [20]	Wang [8]	Present
0.0	1.23258	1.23258	1.2326
0.5	0.71329	0.71329	0.7133
2.0	-1.88730	-1.88730	-1.8873

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Γ	e	Λ	Ec	S	-f''(0)	- heta'(0)
1.0	2.0	0.1	0.1	0.5	1.8814	0.2285
1.0	3.0	0.1	0.1	0.5	4.2831	0.0764
1.5	2.0	0.1	0.1	0.5	1.8775	0.2875
2.5	2.0	0.1	0.1	0.5	1.8730	0.3550
1.0	2.0	1.0	0.1	0.5	1.7030	0.2429
1.0	2.0	3.0	0.1	0.5	1.3216	0.2695
1.0	2.0	0.1	1.5	0.5	1.8747	0.6733
1.0	2.0	0.1	2.0	0.5	1.8723	0.9924
1.0	2.0	0.1	0.1	0.0	1.8830	0.3475
1.0	2.0	0.1	0.1	1.0	1.8789	0.0674



Figure 1. Velocity profile for various values of *M*.



sheet. For this case, the boundary layer thickness increases with the increase of ϵ . Figure 4 shows that the temperature profile for the values of ϵ . The temperature is found to decrease with the increasing values of ϵ .

Figure 5 shows that effect of heat source parameter *S* on temperature profile. It generates heat in the fluid. Therefore temperature profile increases. **Figure 6** indicates the temperature profile for different values of conjugate parameter γ . The effects of Prandtl number on temperature profiles are shown in **Figure 7**. Prandtl number can be used to increase the rate of cooling conducting fluids. Prandtl number signifies the ratio of momentum diffusivity to thermal diffusivity.

Increasing the values of the Ec generates heat in the fluid due to frictional heating. Figure 8 demonstrates that influence of the Ec on the profile of temperature. It is observed that the temperature profile increases as the value of the Ec increases.



Figure 4. Temperature profile for various values of ε .



Figure 5. Temperature profile for various values of *S*.



Figure 6. Temperature profile for various values of γ .



Figure 7. Temperature profile for various values of *Pr*.



6. Conclusions

The numerical solutions for mixed convection MHD stagnation point flow over a stretching surface with the effects of various parameters were analyzed. The effects of various parameters on heat flow characteristics were also discussed. From the graphical representations, we have the following observations.

- The velocity increases with increasing values of the magnetic parameter M.
- An increase in the mixed convection parameter λ increases the velocity profiles.
- An increase in the value of ϵ reduces the temperature, and increases the velocity profiles.
- With increasing values of conjugate parameter γ the temperature profile increases.
- An increase in the Eckert number *Ec* increases the temperature profile.

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