

Identification of Preferable Distributed Generators Locations for Congestion Relief in Multi-Bus Power Network

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Abstract

Installation of Distributed Generator (*DG*) is a well accepted method to improve power system operation from the point of reducing congestion and improving voltage profiles. For best results, Distributed Generators should be placed at strategic locations to exploit maximum benefits out of them. The (N-1) contingency criterion has been taken into account in this work. Most congested lines of the grids are ranked by congestion Index and considered to study the impact of *DG* penetration on congestion. The present paper proposes contribution factors of Distributed Generators for the placement of *DG* to keep the line flow within the capacity of each transmission line of the network. The results obtained from IEEE 30-bus test system indicate that the proposed methods are capable of identifying desirable *DG* location and its maximum allowable size. The influence of *DG* on bus voltage profile has also been demonstrated in this paper.

Keywords

Distributed Generators, Congestion Index, Contribution Factor of DG, Voltage Sensitivity, Zone Classification

1. Introduction

In the last decade, the electricity supply industry has undergone global restructuring, which has significantly changed the electric energy system scenario. Transmission congestion exists in all emerging power networks as

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a natural consequence of demand and capacity mismatch. Active power generation changes according to load demands and system losses. This involves the most important information with which operators grasp present active and reactive power flow in power system, representing the basis of security assessment and contingency analysis. Ng [1] presented a novel approach to solve the real-time line flow calculation Generalized Generation Distribution Factor (GGDF) sensitivity factor. The GGDF loses its accuracy in line flow solutions [2] for non-conforming load change cases. Referring to recent research, sensitivity-based approaches have been widely proposed and applied in related studies into the control and operation of power systems. In [3], a direct method has been proposed for line overload alleviation using sensitivities of the bus injections to the overloaded lines. Transmission congestion may prevent the existence of new contracts, lead to additional outages, increase the electricity prices in some regions of the electricity markets and can threaten the system security and reliability [4]. In the literature, direct methods of line overload alleviation using generator rescheduling and load shedding are described in [5] [6]. In [7], ANN-based preventive approaches are used for congestion management to improve the power system security and reliability in the deregulated power market scenario. In recent days, placement of new generating stations goes under the hand of private entities and under the policy of Transmission Open Access (TOA), Independent Power Producers (IPP) may also be interested to install Distributed Resources (DR's) close to loads as competitive alternatives since DR's can ease the risks of market price hike. Currently there are several kinds of DG's [8] [9], such as diesel turbines with the capacity under 1MW, gas turbines with the capacity in the range of 1 - 20 MW, micro turbines range from 30 - 200 MW, hydro generation capacity in the range of 100 kW - 1 MW. Extensive research has been conducted for Electric Power System (EPS) security control by DG's which can also be introduced into the ancillary markets [10] [11]. From the perspective of the Independent System Operators (ISO) and Distribution Companies (DISCO), it is needed to analyze the role of DG's in congestion management. Parida *et al.* [12] proposed a value-based sensitivity approach for reactive power cost allocation; in addition Jupe and Taylor [13] presented power flow sensitivity factors for the online control of power output of Distributed Generators and Zhou and Bialek [14] developed voltage and loss sensitivity factors for generation curtailment. Ayres *et al.* [15] proposed voltage sensitivity as a means to determine the maximum allowable penetration of Distributed Generators without violations in steady-state voltage. Regarding the placement of *DG* sources, in the literature there are many solutions proposed, namely using fuzzy techniques [16] [17] analytical technique [18], heuristic optimization algorithm [19] [20] mixed integer nonlinear programming [21], evolutionary programming (EP) optimization technique [22], and others. In [23], a fuzzy clustering method has been used to identify the desirable location of Distributed Generators for congestion management. In [24], author has presented an introduction of neural network based clustering. It can be concluded that few studies have used fast line flow calculation using a sensitivity based approaches. Nevertheless, the studies mentioned above have demonstrated theoretical feasibility and practical value in the application of power systems. The use of clustering techniques for representing data, measuring the similarity between elements representative for the group, can be very suggestive and attractive. In the present work, identification of *DGs* desirable locations and its size for congestion management have been proposed. Power Contribution Factor and Voltage Sensitivity Index have been determined and an ANN clustering technique has been implemented to select the load buses for *DG* allocation with respect to overloaded lines in the system. In this paper, a new network Contribution Factors (CF), for real-time line flow calculation is proposed. Optimal value of the *DG* capacity can be obtained to enhance the system performance by improving voltage profiles of the various buses and reducing the system losses. The method proposed in this paper has a benefit over most of the earlier works cited in this literature, in the sense that union of three factors are considered as an the input for ANN clustering; the approach could be used in the field of new expansion of the networks meeting huge customer demand and estimates desirable zones for the placement of *DG* by dividing whole power system into different congestion zones reducing real and reactive power losses and improving voltage profiles.

2. Proposed Methodology

DG allocation for congestion management considering their power contribution factors (*CF*'s) and voltage sensitivity Index will have the more impact on system from reliability point of view. The task is to quantify the *CF*'s of the *DGs* according to the most restrictive constraints of the grid that may cause congestion. This paper introduces a simple and direct approach to these challenges. In this section, the closed form contribution factors of *DG*'s to the line flows and system voltages are derived.

2.1. Contingency Selection

The contingencies are selected by calculating a kind of severity indices known as Performance Indices. Based on the values obtained the contingencies are ranked in a manner where the highest value of PI is ranked first. During contingency both active and reactive power flow limit affects and the bus voltages get altered, hence it is essential to predict the power flow and the bus voltages following contingency. Given this information, an Independent System Operator (ISO) can judge the relative severity on the system security and decide if the preventive actions should be initiate to mitigate congestion problem. The general performance index for a system is defined as [25],

$$(PI)^i = \sum_{\text{allbranches}} \frac{\omega_l}{2n} \left(\frac{S_l^i}{S_l^{\max}} \right)^{2m} + \sum_{j=1}^{NL} \frac{\omega_j}{2n} \left(\frac{\Delta V_j^i}{\Delta V_j^{\lim}} \right)^{2m} \quad (1)$$

$$\Delta V_j^i = V_j^i - V_j^{\text{norm}}$$

$$V_j^{\text{norm}} = V_j^{\min}, \forall V_j^i \leq 0.95$$

$$V_j^{\text{norm}} = V_j^{\max}, \forall V_j^i \geq 1.05$$

where, S_l^i = Active power flow in post contingency cases in line l with i^{th} outage, S_l^{\max} = Maximum active power flow in line l , NL = Number of load buses and m is the integer exponent. V_j^i is the voltage at bus j with i^{th} outage, ΔV_j^{\lim} average of V_j^{\min} and V_j^{\max} where ω_j and ω_l the weighing factor of bus- j and line- l respectively that is decided by the system operator depending upon the operating condition of the system. Following a contingency, any line which is overloaded will make a contribution greater than unity. The m value is fixed at 3. These Performance Index (PI) values have been simulated for various cases by considering $(N-1)$ contingency criteria.

2.2. Congestion Index

It is the measure of congestion of a particular line or overall system. It gives an idea about how much percentage of the line is getting overloaded to power flow. If the value of Index more, it means that more power has been transferred and the line will be more congested and vice-versa. P_{ij}^{\max} is the rating of the power flow of a line connecting bus i and bus j whereas P_{ij} is the actual power flow of the line. For secure operation, the transmission line congestion Index L_{ij} is restricted by upper limit as follows:

$$L_{ij} = \left(P_{ij} / P_{ij}^{\max} \right) \leq 1 \quad (2)$$

$$V_n^{\min} \leq V_n \leq V_n^{\max}, \forall n \in NL$$

where P_{ij} and P_{ij}^{\max} are real power flow in line $i-j$, V_n represents voltage magnitude of n th bus and NL represents number of load buses.

2.3. Contribution Factor based DG Allocation in Electric Grid

The contribution factors denote how much active and reactive power flow over a transmission line would change due to change in real and reactive power injections from Distributed Generators. The power flow of a line k can be modeled as the sum of base case active power flow (P_k^{base}) and incremental power flow (ΔP_k), that is,

$$P_k = P_k^{\text{base}} + \Delta P_k \quad (3)$$

The power flow contribution of Distributed Generators (DG) to each line is computed by the following equations: As proved in the Appendix (Section A.1), the Real power contribution factor of the DG 's to real flow of line k is

$$CFP_{DG}(k, n) = \sum_{j=1}^{nb} \frac{\partial |V_j|}{\partial P_n} \frac{\partial P_k}{\partial |V_j|} + \sum_{j=1}^{nb} \frac{\partial |\delta_j|}{\partial P_n} \frac{\partial P_k}{\partial |\delta_j|} \quad k = 1, 2, \dots, nl \quad (4)$$

The Reactive power contribution factor of the DG s to real flow of line k is given by

$$CFQ_{DG}(k, n) = \sum_{j=1}^{nb} \frac{\partial |V_j|}{\partial Q_n} \frac{\partial P_k}{\partial |V_j|} + \sum_{j=1}^{nb} \frac{\partial |\delta_j|}{\partial Q_n} \frac{\partial P_k}{\partial |\delta_j|} \quad k = 1, 2, \dots, nl \quad (5)$$

$$P_k = P_k^{base} + \sum_{n=1}^{nb} CFP_{DG}(k, n) \Delta P_n + \sum_{n=1}^{nb} CFQ_{DG}(k, n) \Delta Q_n \quad (6)$$

2.4. Voltage Sensitivity

The voltage sensitivity related to active power injections has a vital role of improving the system voltage profile in the presence of Distributed Generators. The proposed method for estimating the maximum allowable power injection into each system bus based on the voltage sensitivity is validated in Appendix A. Supposing that $\Delta Q = 0$, and J_{21}^{-1} non-singular, from Appendix (Section A.2) we have

$$\Delta V_{P_{DG}} = J_R^{-1} \Delta P \quad (7)$$

where J_R is a reduced Jacobian matrix, which gives the voltage magnitude variations due to active power injection variations. The matrix J_R can be used directly in order to indicate which buses of the system will be more or less affected by the installation of a *DG* unit. Therefore the estimated voltage profile after the installation of one or a group of new generators can be analytically expressed by

$$V = V^0 + \Delta V_{(P_{DG})} \quad (8)$$

where V^0 is the voltage profile for the base case. Equation (8) allows one to estimate the voltage profile when the generator is installed at every possible bus of the system, with unity power factor and with any specified generation level. In the following section, these sensitivities are used in the proposed method for estimating the maximum allowable power injection of Distributed Generators.

2.5. Determination of *DG* Size

The determination of the maximum power that a Distributed Generator (*DG*) can inject into a system without causing steady-state voltage violations is difficult. The maximum active power that the installed *DG* unit at bus i with unity power factor can export to the system without violating the voltage limits of bus n is expressed as follows:

$$P_{DG_i}^n = \frac{\Delta V_n}{J_{R(n,i)}} \quad (9)$$

One *DG* unit can affect all the nodal voltages of the system; thus, the maximum amount of active power that can be injected at bus n will be different if the violation is considered for the different buses of the system. Consequently, the maximum capacity that can be injected at bus i is the minimum amount of power necessary to violate at least one nodal voltage of the system.

3. Clustering Approach for Transmission Congestion Management

To classify the most desirable and undesirable location of *DGs* in large systems, a proper and simple clustering on the basis of Contribution Factors is necessary. It is observed that the values of the *CF*'s are diverse according to the location and the expected *DG* output. Due to the uncertainty of the *DG* operations, it may be very desirable to determine the trend of such influences in a loading area rather than an accurate value. In the present work, the whole system has been clustered in different zones by estimating power flow contribution factors and voltage sensitivity indexes of *DGs* to manage the congestion in the operating area.

SOFM Architecture and Algorithm

SOFM is a simplified model of the feature called "localized region mapping" of the brain from which it derives its name. **Figure 1** shows the typical architecture of SOFM. This network learns without supervision, implying that the topological relationship of the input data is not necessarily known a priori. This network architecture

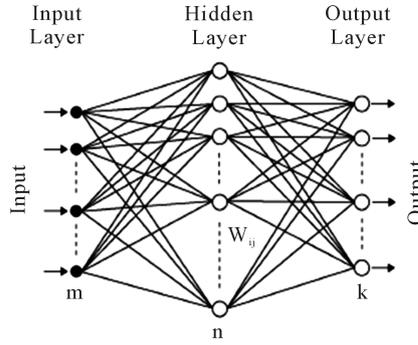


Figure 1. Self-organizing neural network architecture with the output layer neurons arranged in one-dimensional.

was originally conceived by Kohonen [26] and in his approach, Kohonen proposed a fully laterally connected network with distance related feedback synapses showing inhibition and excitation features. The remarkable feature of SOFM is that it reduces dimensionality of mapping without losing important topological relationship between them. In the SOFM algorithm, first the weights between input and output are initially set to small random values and an initial neighborhood is also chosen. After that the input vectors for the network are selected, the distance of an input vector from each neuron j in the Kohonen's layer can be calculated as:

$$d_j = \|X - W_j\| = \sqrt{\sum_{k=1}^n (i_k - w_{jk})^2} \quad (10)$$

where, $X = (i_1, i_2, \dots, i_n)$ denotes an input vector; $W_j = (w_{j1}, w_{j2}, \dots, w_{jn})$ denotes the weight vector of the j th neuron.

The Kohonen neuron with the minimum distance d_w is chosen as the winner and is presented input vector, which is given by:

$$d_w = \min \{d_j\} \quad j \in \{\text{Kohonen - layer}\} \quad (11)$$

During training, the winner adjusts its weights to be closer to the values of input data while the neighbors of the winner also simultaneously adjust their weights to compete with the winner and to be closer to the same input vector according to the following weight adjustment schedule:

$$W_j = W_j + \alpha (X - W_j) \quad j \in \{\text{Kohonen - layer}\} \quad (12)$$

The term α is a gain term that decreases in time. It may be convenient to start with the value of $\alpha = 0.5$ and decrease it over time to 0.1 or lower. After training, the weight vectors are self-organized and represent prototypes of the classes that pre-exist within the input vectors.

4. Result and Discussions

All the programming modules have been developed in MATLAB working environment. A Pentium IV with 2 GHZ processor speed and 512 MB RAM has been used for simulation of the problem. The performance Index (PI) values are computed considering the outage of only one line sequentially. The PI values of ten most emergency lines with 70% - 80% loading are given in descending order in **Table 1**. It can be inferred that outage of line 2 - 4 in the test system is the most vulnerable one and will result great impact on the whole system.

4.1. Identification of Most Congested Zones in the Network Using Congestion Index

The Performance Indices (PI) with highest value reflect a severe case and the system parameters go beyond their limits which results power flow congestion in the lines. The IEEE-30 bus system has 6 PV buses, 24 PQ buses and 41 lines; hence for the PI calculation a total number of 41 line contingency cases are performed. From Table 1 it can be inferred that the post contingency analysis gives the reflection of overloaded lines connected between

buses (28 - 27, 25 - 27, 4 - 6, 1 - 2, 1 - 3, 15 - 23, 6 - 28, 8 - 28, 29 - 30 and 16 - 17) in which desirable operation must be claimed to relieve 1congestion by placing *DG* at the load buses.

4.2. Utilization of Distributed Generators for Relieving Congestion

4.2.1. Determination of *DG* Contribution Factors

For each loading scenario, the real and reactive power flow contribution factors associated with real and reactive power injections from *DGs* are computed in each line and voltage sensitivity at each bus by considering real power flow limit of transmission line as the system security constraints. It is clear from **Figure 2** and **Figure 3** that two most critical lines Line no. 36 (28 - 27) and Line no. 7 (4 - 6) are the suitable lines to relieve power flow congestion by connecting *DG* which create the diversity of such effects in heavily loaded areas. The darkened area indicates the desirable locations which will reduce the transferred real power along the critical lines having most negative Real power contribution factor of *DGs* (CFP_{DG}). Line no. 36 (28 - 27) and Line no. 7 (4 - 6) have the most negative CFP_{DG} with respect to real power injection from *DGs*. The lightened area represent the *DGs* with positive CFP_{DG} values has least participation in mitigating congestion which means the line flows may be increased beyond the limit of rated power flow capacity with insertion of *DGs* which is undesirable from the system reliability point of view. The other post contingency critical lines along with some power injected buses having small real power and reactive power contribution of Distributed Generators are not so much distinct and

Table 1. Different critical lines with critical contingency.

Sl. no	Critical Lines	<i>PI</i>	Sl. no	Critical Lines	<i>PI</i>
1	1 - 2	28.7520	6	6 - 28	28.7520
2	28 - 27	30.4486	7	8 - 28	30.4486
3	25 - 27	29.6393	8	1 - 3	29.6393
4	4 - 6	30.4666	9	29 - 30	30.4666
5	16 - 17	29.2732	10	15 - 23	29.2732

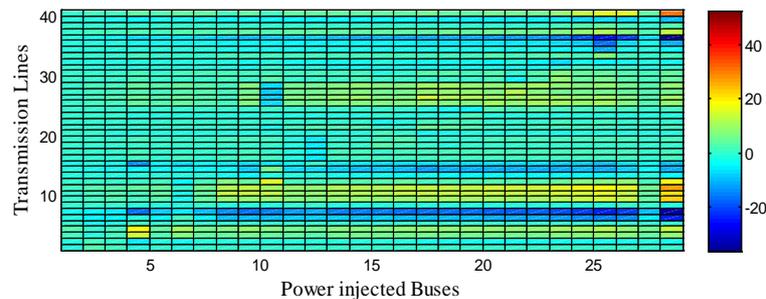


Figure 2. Active power contribution factor of *DG*.

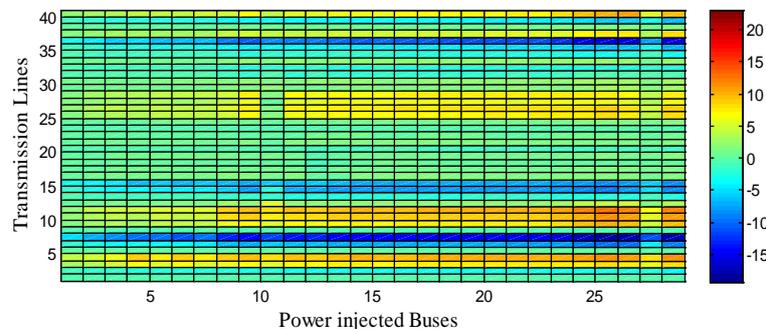


Figure 3. Reactive power contribution factor of *DG*.

need to be analyzed by neural network based intelligence.

Similarly the darkened area in **Figure 3** indicates that Line no. 7 (4 - 6) has the most negative reactive power CFQ_{DG} with respect to real power injection from DGs . For the above lines, most of DGs will even reduce the transferred power through the critical lines, which express importance of DGs to relieve congestion.

4.2.2. Identification of Desirable and Undesirable DG Location Using ANN Clustering

ANN based intelligent technique has been applied to mitigate power flow congestion by clustering approach to identify preferable DG location in the system which mainly depends upon the line flow and voltage scenario of the power system. Active and Reactive power contribution factors of Distributed Generators have been utilized for identifying the desirable location of DG to extenuate overloads in the electric grid. When the generation cannot meet the demand, voltage instability occurs and therefore there will be a large increase in the need for active power generation. When a system is heavily congested voltage sensitivity information of Distributed Generators has taken as a part of the input information in congestion management, otherwise the voltages at different buses becomes lower than a fixed or nominal value and go beyond the security margins. Determination of the number of neurons of Kohonen network should depend on the application and make the Kohonen network capable of forming sufficient clusters of input vectors. It has been found that 16×16 neurons in the Kohonen's layer give the best clustering for this particular system after rigorous testing with 11×11 , 12×12 , 13×13 , 14×14 , 15×15 , 16×16 , 17×17 , 18×18 of output layer neurons. The properties of the clusters can be identified by analyzing the weight vectors associated with the neurons in the clusters, as all neurons belonging to a cluster have "similar" features. In the present work, the properties of the clusters can be identified by analyzing the weight vectors associated with the neurons in the clusters and comparing them with the CFP_{DG} and CFQ_{DG} values which are indicated in **Table 2**, **Table 3** and **Table 4** based on systems which are clustered as undesirable zone (Zone I), intermediate zone (Zone II) and most desirable zone (Zone III). However, the degree of desirability of DGs for relieving system congestion can be simply identified by SOFM based clustering method.

Figure 4 indicates most desirable zone for the placement of DGs to mitigate congestion and as well as improve the system voltage profiles. It can be observed that in Zone III, bus-30, bus-29, bus-27, bus-26, and bus-25 have the most negative value of real power flow and reactive power flow contribution factors and accordingly the system operator (SO) selects the most desirable zone for placing DG to manage congestion in the network. However, the degree of desirability of DGs for relieving system congestion can be simply identified by SOFM based clustering method.

4.3. Analysis of Congestion Levels before and after Connecting DGs

Our proposed method is capable of handling changes in demand across all buses as well as providing a precise reflection of the active and reactive power injection into the active power flow. At new loading point, the amount of change in the active and reactive power demands of the bus can be expressed as increments from the base load. These incremental terms must be balanced by active and reactive power generation of Distributed Generators without affecting the reference bus. It has been observed that the ISO selects the load bus no. 30 for DG

Table 2. Zone classification by ANN based clustering for line no. 36 (bus28 - bus27).

Zone I				Zone II				Zone III	
CFP_{DG}		CFQ_{DG}		CFP_{DG}		CFQ_{DG}		CFP_{DG}	CFQ_{DG}
28, -6.559	5, -5.937	28, -7.528	5, -5.294	24, -14.568	17, -10.237	24, -12.105	17, -10.458	30, -36.547	30, -16.4345
13, -8.282	4, -3.910	13, -8.941	4, -5.713	23, -11.753	16, -9.531	23, -11.043	16, -10.012	29, -36.279	29, -14.592
11, -7.699	3, -2.658	11, -8.030	3, -4.653	22, -11.817	15, -10.293	22, -11.256	15, -10.203	27, -20.185	27, -15.053
9, -7.699	2, -1.504	9, -8.856	2, -2.884	21, -11.608	14, -9.866	21, -11.022	14, -9.916	26, -24.239	26, -17.130
8, -5.940		8, -6.677		20, -10.882	12, -8.282	20, -10.675	12, -8.941	25, -19.486	25, -14.211
7, -5.228		7, -6.216		19, -11.117	10, -9.897	19, -10.733	10, -9.348		
6, -5.246		6, -6.561		18, -11.057		18, -10.580			

Table 3. Zone classification by ANN based clustering for line no. 7 (bus4 - bus6).

Zone I				Zone II				Zone III	
CFP_{DG}		CFQ_{DG}		CFP_{DG}		CFQ_{DG}		CFP_{DG}	CFQ_{DG}
28, -9.005	5, -15.681	28, -10.694	5, -9.804	24, -14.568	17, -15.832	24, -15.749	17, -14.434	30, -34.128	30, -19.282
13, -11.287	4, -4.867	13, -14.480	4, -8.413	23, -11.753	16, -14.236	23, -15.059	16, -14.199	29, -32.420	29, -17.810
11, -14.467	3, -3.246	11, -11.668	3, -6.815	22, -11.817	15, -15.041	22, -14.913	15, -14.480	27, -20.301	27, -17.439
9, -14.118	2, -2.798	9, -12.953	2, -4.728	21, -11.609	14, -14.321	21, -15.028	14, -14.305	26, -23.829	26, -18.467
8, -8.638		8, -9.831		20, -10.882	12, -11.856	20, -14.751	12, -13.642	25, -20.80	25, -17.178
7, -5.637		7, -10.794		19, -11.117	10, -14.467	19, -14.902	10, -14.184		
6, -7.255		6, -9.753		18, -11.058		18, -14.814			

Table 4. Zone classification by ANN based clustering for line no. 35 (bus25 - bus27).

Zone I				Zone II				Zone III	
CFP_{DG}		CFQ_{DG}		CFP_{DG}		CFQ_{DG}		CFP_{DG}	CFQ_{DG}
28, -2.068	5, -2.749	28, -3.054	5, -2.290	26, -5.072	17, -4.403	26, -5.278	17, -4.538	30, -11.878	30, -7.113
13, -3.496	4, -1.547	13, -3.874	4, -2.398	23, -5.123	16, -4.067	23, -4.798	16, -4.341	29, -10.244	29, -6.743
11, -3.378	3, -1.043	11, -3.503	3, -1.943	22, -5.010	15, -4.393	22, -4.899	15, -4.425	27, -16.405	27, -6.327
9, -3.378	2, -0.624	9, -3.861	2, -1.218	21, -4.689	14, -4.196	21, -4.788	14, -4.302	24, -8.593	24, -6.378
8, -2.238		8, -2.770		20, -4.777	12, -3.496	20, -4.632	12, -4.050	25, -6.345	25, -6.234
7, -2.5566		7, -2.648		19, -4.740	10, -4.270	19, -4.657	10, -4.515		
6, -2.041		6, -2.740		18, -4.740		18, -4.539			

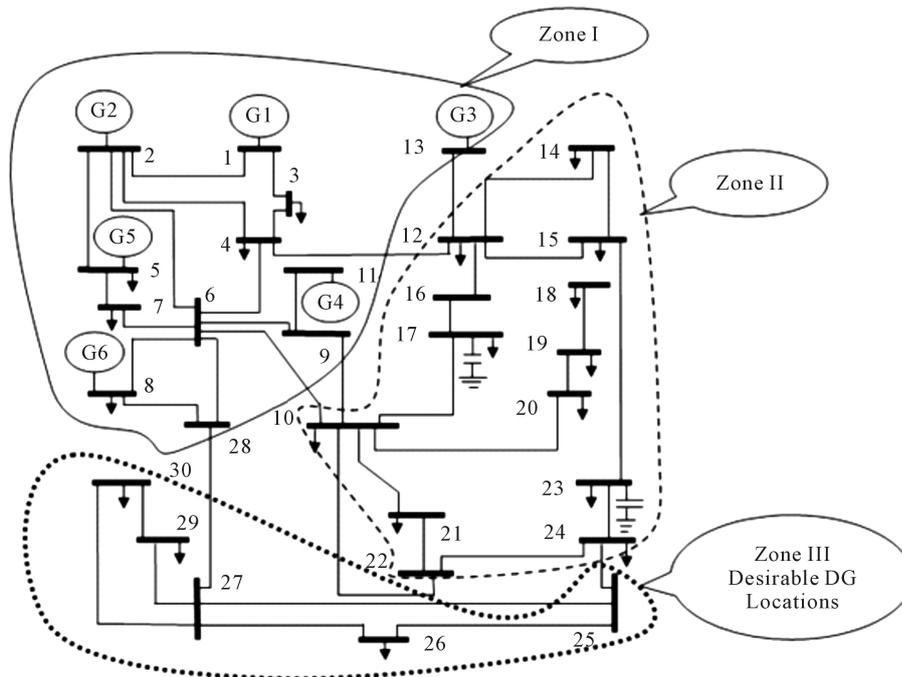


Figure 4. Classification of different zone for placement of DG.

connection taking from desirable zone which is clustered by ANN based technique for the whole system. One *DG* unit can inject into the respective bus without causing superior voltage limit violation in any bus. The maximum active power of installed *DG* at bus 30 can inject into the system without causing voltage violations is 20 kW, since the installation of generators in these buses extremely affects the system voltage profile. The results provided by the repetitive power flow method, where a step of 1.0 kW of power injection was used to determine the maximum allowable power injection, are compared with those obtained by the analytical method. The congested lines 1 - 3, 6 - 28, 4 - 6, 3 - 4, and 2 - 6 are getting relieved with significant amount of 67.8%, 65.62%, 61.54%, and 53.22% respectively and other lines are also listed in **Table 5**.

It can be observed that only ten most congested lines, in descending order of their values are shown in **Table 6**. The Congestion Index value for heavily congested lines before and after connection of *DG*s in desirable locations is listed in this table. **Figure 5** shows the variation of bus voltage profiles of the system with *DG* placement at bus no. 30. It is noticed that, for a particular loading scenario, the installation of *DG* improve the bus voltages due to injection of power locally.

It should be noted that the voltages at every bus after employing *DG* within acceptable limits. Therefore an improvement in voltage in buses related to the congested lines indicates a reasonably good and impact of distributed generation (*DG*) on the voltage profiles. Improvement in voltage profile also suggests an enhancement in voltage stability margin in the system.

Table 5. Percentage of loading in different congested lines.

Lines	% of loading before <i>DG</i>	% of loading after <i>DG</i>	% relieved loading	Lines	% of loading before <i>DG</i>	% of loading after <i>DG</i>	% relieved loading
10 (6 - 8)	48.77	47.941	16.58	3 (2 - 4)	51.471	49.575	37.92
6 (2 - 6)	70.712	68.051	53.22	15 (4 - 12)	49.655	47.986	33.38
7 (4 - 6)	82.013	78.936	61.54	4 (3 - 4)	95.853	92.787	61.32
2 (1 - 3)	104.5	101.11	67.8	5 (2 - 5)	87.743	86.461	25.64
41 (6 - 28)	25.414	22.133	65.62	1 (1 - 2)	208.23	201.95	74.01

Table 6. Index values of different lines before and after *DG* connection.

Sl. No	Line No.	Before connecting <i>DG</i>	After connecting <i>DG</i>	Sl. No	Line No.	Before connecting <i>DG</i>	After connecting <i>DG</i>
1	1 (1 - 2)	1.60176	1.55343	6	41 (6 - 28)	0.79418	0.69166
2	10 (6 - 8)	1.52406	1.49815	7	3 (2 - 4)	0.79186	0.76269
3	6 (2 - 6)	1.08787	1.04693	8	15 (4 - 12)	0.76392	0.73824
4	7 (4 - 6)	0.91125	0.87706	9	4 (3 - 4)	0.73733	0.76269
5	2 (1 - 3)	0.80384	0.77776	10	5 (2 - 5)	0.67494	0.66508

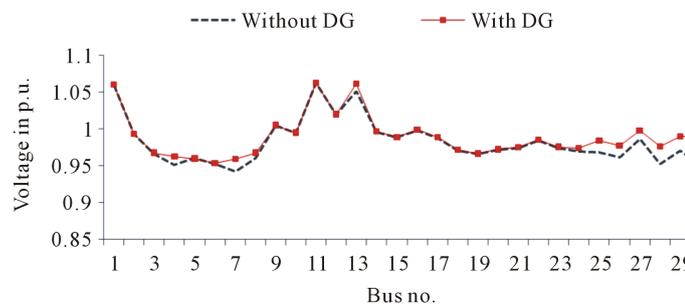


Figure 5. Improvement of voltage profile with insertion of *DG*.

5. Conclusions

Contribution Factors of Distributed Generator based on Jacobian based power flow methodologies are proposed. ANN based unsupervised technique has been presented to cluster the whole system into *DG* connection zone to manage congestion situation of the system. Voltage sensitivity approach is proposed to determine maximum *DG* size. The proposed methods are tested on IEEE 30-bus system and it reveals the following:

- This voltage sensitivity expresses the incremental changes in voltages in different buses with real power injection from *DG* with improvement in voltage profiles of the system.
- The suggested method is quite fast and can be applied for updating line flows and hence the cluster of zones for congestion management with help of proper placement of *DG*'s.

Thus the present research clearly demonstrates the role of *DG*s as an effective tool for relieving congestion in power networks. The proposed approach is computationally efficient and simple as it utilizes the sensitivity factors, which can be easily updated for future expansion of the system.

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Appendices

A.1. Calculation of Contribution Factors (CF) of Distributed Generators to Real Power Flow of Transmission Lines

The real power flow (P_k) and reactive power flow (Q_k) in a line k connected between bus- i and bus- j can be written as

$$P_k = G_k |V_i|^2 - G_k |V_i||V_j| \cos(\delta_i - \delta_j) - B_k |V_i||V_j| \sin(\delta_i - \delta_j) \quad (\text{A1.1})$$

$$Q_k = -B_m |V_i|^2 + B_k |V_i||V_j| \cos(\delta_i - \delta_j) - G_k |V_i||V_j| \sin(\delta_i - \delta_j) \quad (\text{A1.2})$$

Hence, the total variations of real power flow can be expressed by the following linear formula:

$$\Delta P_k = \sum_{n=1}^{nb} \frac{\partial P_k}{\partial P_n^{DG}} \Delta P_n^{DG} + \sum_{n=1}^{nb} \frac{\partial Q_k}{\partial Q_n^{DG}} \Delta Q_n^{DG} \quad (\text{A1.3})$$

Consequently Equation (A1.3) can be written as

$$\Delta P_k = \sum_{n=1}^{nb} CFP_{DG}(k, n) \Delta P_n + \sum_{n=1}^{nb} CFQ_{DG}(k, n) \Delta Q_n \quad (\text{A1.4})$$

$$CFP_{DG}(k, n) = \frac{\partial P_k}{\partial P_n^{DG}} \quad (\text{A1.4a})$$

$$CFQ_{DG}(k, n) = \frac{\partial Q_k}{\partial P_n^{DG}} \quad (\text{A1.4b})$$

$CFP_{DG}(k, n)$ and $CFQ_{DG}(k, n)$ respectively, termed active power contribution factor and reactive power contribution factor of DG .

Substituting Equation (6) and Equation (7) for ΔP_k in Equation (5)

$$P_k = P_k^{base} + \sum_{n=1}^{nb} CFP_{DG}(k, n) \Delta P_n + \sum_{n=1}^{nb} CFQ_{DG}(k, n) \Delta Q_n \quad (\text{A1.5})$$

For practical system, it is necessary to include the changes in bus power injection which cause variations in all bus voltage magnitudes and phase angles.

$$CFP_{DG}(k, n) = \sum_{j=1}^{nb} \frac{\partial |V_j|}{\partial P_n} \frac{\partial P_k}{\partial |V_j|} + \sum_{j=1}^{nb} \frac{\partial \delta_j}{\partial P_n} \frac{\partial P_k}{\partial \delta_j} \quad (\text{A1.6})$$

$$k = 1, 2, \dots, nl$$

$$CFQ_{DG}(k, n) = \sum_{j=1}^{nb} \frac{\partial |V_j|}{\partial Q_n} \frac{\partial P_k}{\partial |V_j|} + \sum_{j=1}^{nb} \frac{\partial \delta_j}{\partial Q_n} \frac{\partial P_k}{\partial \delta_j} \quad (\text{A1.7})$$

$$k = 1, 2, \dots, nl$$

The inverse Jacobian can be written as

$$\begin{bmatrix} \Delta \delta \\ \Delta |V| \end{bmatrix} = \begin{bmatrix} J_{11}^{-1} & J_{12}^{-1} \\ J_{21}^{-1} & J_{22}^{-1} \end{bmatrix} \begin{bmatrix} \Delta P \\ \Delta Q \end{bmatrix} \quad (\text{A1.8})$$

$$CFP_{DG}(k, n) = \left(\frac{\partial |V_i|}{\partial P_n} \right) \frac{\partial P_k}{\partial |V_i|} + \left(\frac{\partial |V_j|}{\partial P_n} \right) \frac{\partial P_k}{\partial |V_j|} + \left(\frac{\partial \delta_i}{\partial P_n} \right) \frac{\partial P_k}{\partial \delta_i} + \left(\frac{\partial \delta_j}{\partial P_n} \right) \frac{\partial P_k}{\partial \delta_j} \quad (\text{A1.9})$$

$$CFQ_{DG}(k, n) = \left(\frac{\partial |V_i|}{\partial Q_n} \right) \frac{\partial P_k}{\partial |V_i|} + \left(\frac{\partial |V_j|}{\partial Q_n} \right) \frac{\partial P_k}{\partial |V_j|} + \left(\frac{\partial \delta_i}{\partial Q_n} \right) \frac{\partial P_k}{\partial \delta_i} + \left(\frac{\partial \delta_j}{\partial Q_n} \right) \frac{\partial P_k}{\partial \delta_j} \quad (\text{A1.10})$$

$$\frac{\partial P_k}{\partial |V_i|} = 2|V_i^{base}|G_k - |V_j^{base}|G_k \cos(\delta_i^{base} - \delta_j^{base}) - |V_j^{base}|B_k \sin(\delta_i^{base} - \delta_j^{base}) \quad (\text{A1.11})$$

$$\frac{\partial P_k}{\partial \delta_i} = |V_i^{base}||V_j^{base}|G_k \sin(\delta_i^{base} - \delta_j^{base}) - |V_j^{base}||V_j^{base}|B_k \sin(\delta_i^{base} - \delta_j^{base}) \quad (\text{A1.12})$$

$$\frac{\partial P_k}{\partial |V_j|} = -|V_i^{base}|G_k \cos(\delta_i^{base} - \delta_j^{base}) - |V_i^{base}|B_k \sin(\delta_i^{base} - \delta_j^{base}) \quad (\text{A1.13})$$

$$\frac{\partial P_k}{\partial \delta_j} = -|V_i^{base}||V_j^{base}|G_k \sin(\delta_i^{base} - \delta_j^{base}) + |V_j^{base}||V_j^{base}|B_k \sin(\delta_i^{base} - \delta_j^{base}) \quad (\text{A1.14})$$

A.2. Voltage Sensitivity

Supposing that $\Delta Q = 0$, and J_{21}^{-1} non-singular,

$$\begin{bmatrix} \Delta P \\ \Delta Q \end{bmatrix} = \begin{bmatrix} J_{11} & J_{12} \\ J_{21} & J_{22} \end{bmatrix} \begin{bmatrix} \Delta \delta \\ \Delta |V| \end{bmatrix} \quad (\text{A2.1})$$

$$\Delta P = (J_{12} - J_{11}J_{21}^{-1}J_{22})\Delta V = J_{RPV}\Delta V \quad (\text{A2.2})$$

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