Scientific
Research

Electric Field and Hot Spots Formation on Divertor Plates

Yuri Igitkhanov, Boris Bazylev
Karlsruhe Institute of Technology, *Association EURATOM-KIT*, *Karlsruhe*, *Germany*
E-mail: *juri.igitkhanov@ihm.fzk.de*

Abstract

In this paper, we consider the intensive erosion of tungsten brush-type armour structures that face the plasma in divertor fusion reactors. Surface erosion caused by multiple transient events (ELMs, disruption, etc.) could lead to the formation of a corrugated wedge-type shape. Our analysis shows that the augmentation of surface roughness increases the electric field at the vicinity of the wedge-type tips, thus enabling the formation of electric arcs. Specifically, under reactor conditions, the breakdown of the sheath potential may trigger unipolar arcs that will strongly contaminate the plasma with the resulting tungsten ions. We show that the erosion caused by arcs is almost two orders of magnitude larger than that caused by DT ion sputtering and comparable with that caused by self-sputtering.

Keywords: Plasma Facing Components, Erosion, Unipolar Arcs, Dust Formation

1. Introduction

The tungsten macro-brush (W-brush) structure has been envisaged as a plausible design for the divertor plates of ITER in order to mitigate surface cracking caused by energy loads of transient events [1]. Experimental and numerical investigations have already indicated that disruptions and giant ELMs power loadings may result in melting, evaporation, and vapor-shield formation of W-brush structures under ITER conditions [2,3]. In addition, it is known that the pressure gradient along the target surface moves the molten layer and contributes to the surface roughness. Actually, for the proposed ITER ELMs size, it has been estimated that, after more than one thousand ELMs, the molten layer thickness is within the millimeter scale. During ITER operation, several hundred disruptions may occur and create a molten surface layer of depth of up to hundred microns per disruption. This melting process has been investigated numerically using the MEMOS code [4]. The calculation showed that ELMs are the main responsible for the target's erosion and thus determine the lifetime of the divertor plates.

The cross-section of the model for the W-brush plate used in the present numerical simulations is shown in **Figure 1**.

The typical sizes of the elements of the macro-brush amour vary within the following ranges: diameter of brushes, $D \sim 0.5$ - 1.0 cm; depth of the gaps between the brushes, $h \sim 1$ cm; width of the gap, a~0.5-1mm (see **Figure 1**). In order to avoid sharp corners, each brush element is supposed to be rounded with a radius R that varies from 0.5 to 1 mm. The surface roughness is normally much less than 1 mm but it may reach 1 mm in the case of giant ELMs. Yet, as shown by earlier calculations, splashing of molten droplets does not occur because the capillary pressure exceeds the centrifugal pressure at the rounded surface corners, which constitutes the Taylor criterion limiting the outflowing of the molten layer [4]. However, we will show below that surface roughness can trigger unipolar arcs that would eject a substantial amount of tungsten atoms into the plasma. This mechanism may contaminate the plasma much more than plasma sputtering and evaporation.

In **Figure 2**, we show the evolution of the corrugated surface under recurrent impact of ELM-pulses with a heat load of $Q = 1.6$ MJ/m^2 and an exposition time t = 0.5 ms, as reported in [4].

The corrugated shape of the surface starts to form with the melting of the originally flat W-brush elements shown in **Figure 1**. The molten layer is then pushed to the left under the pressure of the incoming plasma. Since the molten material re-solidifies in between two ELMs, a peak starts to appear on the left edge of each brush element. As this mechanism repeats itself, the right edge of the brush element is shadowed by the corresponding peak of the neighboring brush element, thus protecting it from plasma exposure. This process eventually leads to
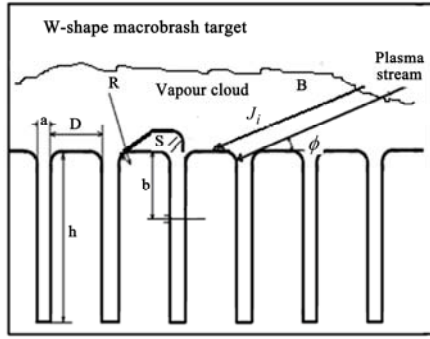
Figure 1. Schematic representation (cross-section) of the W macro-brush target. The geometrical parameters are given in [4].
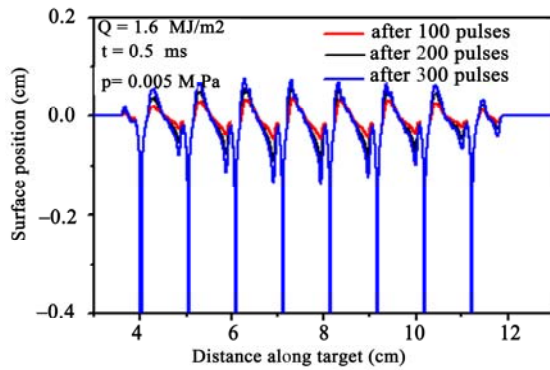

Figure 2. Side view of the corrugated W-brush target under recurrent ELM-like plasma heat loads Q = 1.6 MJ/m² and exposition time t = 0.5 ms [4].

the appearance of the second peak. The details of the resulting wedge-like shape of a brush element after exposure are shown in **Figure 3** for various numbers of pulses. In the following section, we will show that such an augmentation of surface roughness increases the electric field at the vicinity of the wedge' tips.

2. Simulation of the Sheath Electric Field

In this work, we will consider the voltage drop across the Langmuir sheath as the primary driving force for unipolar arc ignition. The electric field in the vicinity of corrugated W-wedges, as those shown in **Figures 2** and **3**, will be estimated. The electric field profile can be found by solving the 2D Poisson's equation:

$$\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} = \kappa^2 \psi \quad (1)$$

$$\kappa^2 = 4\pi e^2 \left(\sum_i Z_i^2 n_i / T_i + n_e / T_e \right) \quad (2)$$

where $\psi \equiv \varphi / \varphi_f$ is the electrostatic potential normalized to the floating potential φ_f, n_i is the ion density, including tungsten impurities in Z_i charge state, n_e is
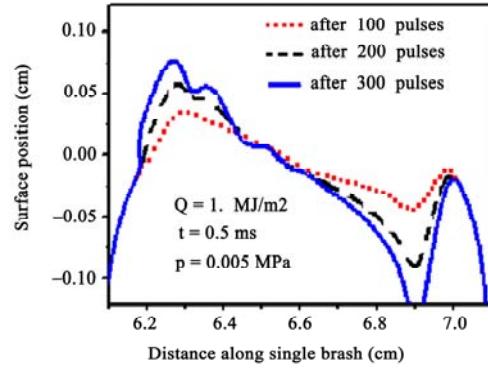

Figure 3. View of a single W-brush after melting and displacement of the molten layer for various numbers of pulses [4].

the electron density, T_e and T_i are the electron and ion temperatures, respectively. The coordinate along and normal to the surface are denoted by x and y, respectively. The electric potential is considered to be averaged in time so that the right side of Equation (1) is linearized and κ is inversely proportional to the Debye length. We solve Equation (1) within the SOL region, which is bounded from the bottom by the corrugated metallic surface at which, necessarily, $\psi = 0$; and from the top by an imaginary flat boundary (at y→∞) at which we set arbitrarily $\psi = 1$. We also assume that ψ increases as a linear function of y along the lateral sides of the SOL. The standard variation procedure of a finite element method is applied here for solving the 2D Poisson's equation in the case of systems with sudden changes in the boundary shape, such as rectangular corners.

The numerical grid used for solving Equation (1) for the surface after 300 ELMs exposition was generated with triangles. Such a grid in the area adjacent to the corrugated surface is shown in **Figure 4.** A set of supplementary functions is used to model the rectangular corners along with the mesh refinement (see [5] for details).

Our results for the electric potential are presented as a contour plot in **Figure 5**, which clearly shows that the equipotential lines follow the shape of the corrugated surface in its vicinity and smoothen away from it (top region in **Figure 5**). On the overall, as expected, the electric potential increases from the surface to upstream region. Most importantly, our calculation shows that the electric field (see **Figure 6**) has components along y and x directions and that, at the wedge' tips, it reaches values as large as $|E_{max}| \sim 3.5 \times 10^7$ V/cm. Such large values of the electric field can trigger intensive field electron emission (see **Figure 8**). Since electron field emission is extremely sensitive to the actual value of the electric field and is crucial for arcs ignition, the calculation of the
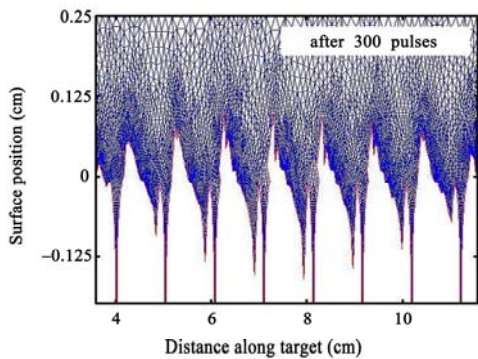
Figure 4. Grid for solving Equation (1) in the case of a corrugated W-brush-type divertor plate after 300 ELMs pulses.
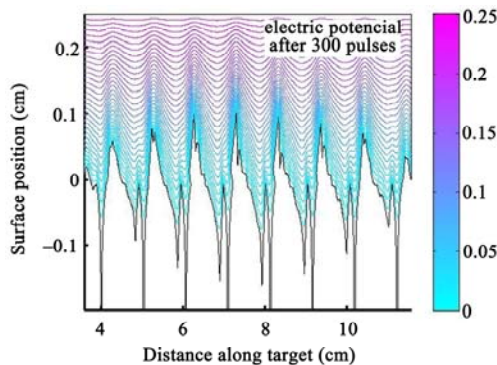

Figure 5. Equipotential lines (ψ = const) graduated according to the column shown on the right side. The lines are smoothened by using the cubic spline interpolation.
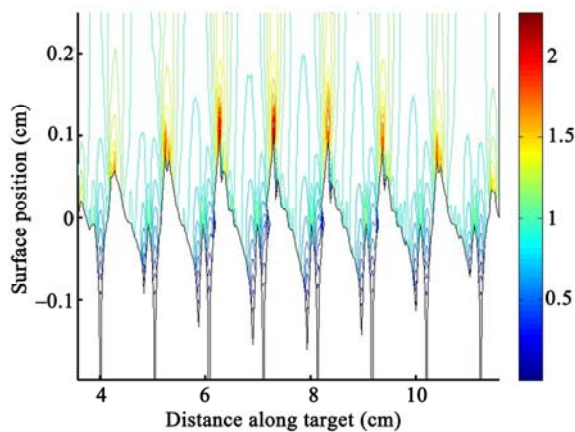

Figure 6 Electric field contour lines based on a normalization unit of 1×10^4 keV/cm. The electric field is graduated according to the column shown on the right side.

singular electric field at the wedge' tips requires a much higher precision than that achieved by only refining the numerical mesh. For that reason, the behaviour of the electric field near the metallic wedge' tip is estimated

analytically by assuming that the metallic 3D tip has a wedge-like shape with an aperture θ (see picture embedded in **Figure 7**) [6] and by solving the corresponding Laplace's equation in spherical coordinates.

The electric field components on the metallic wedge behave like $|E| \sim const./r^{\alpha(\theta)}$, where $\alpha(\theta)$ is a function of θ (see **Figure 7**), and $const.= |E_{max}|\delta^{\alpha(\theta)}$. The latter constant can be determined from the numerical calculations (discussed above) for some mesh size in the vicinity of the tip. The electric field diverges for $\alpha > 0$ and very sharp wedge's tips ($\theta \to 0$). For small θ, α characterizes the degree of singularity and behaves as $\alpha \sim 1-\pi/(2\pi-\theta°)$. This allows one to estimate the electric field at the wedge tip for arbitrary values of the cone angle: $E(r, \theta)$=const. $(1-\alpha(\theta))\cdot\sin(\varphi//2)/2r^{\alpha(\theta)}$[**7**].

3. Unipolar Arc Ignition and Stationary Burn

The large electric field found at the wedge tips (**Figure 6**) strongly enhance the electron field-emission. Emitted electrons accelerate within the sheath potential and can easily acquire a kinetic energy of ~100 eV. At that energy the ionization cross section for tungsten atoms has its maximum. Ionized tungsten atoms accelerate towards the tips of the wedge. Such a tungsten bombardment leads to heating of some spots, augmenting the electron thermal emission and vaporization. The initial electron field-emission breaks the sheath potential and eventually drops itself. However, because of the high temperature at the spot, an arc current can be sustained by increased thermal electron emission and ejection of tungsten atoms from the hot spot. The requirement for arc ignition is that the initial current density from the tip to the plasma (dominated by field emission) must exceed some threshold value~1 A/cm^2 for tungsten [8]. For stationary burning, the arc voltage and current must exceed U_a~15 V and ~10 A, respectively [9]. Calculations show that
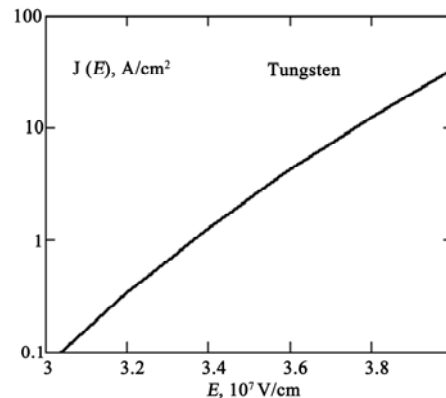

Figure 7. The electron field emission J (E) as a function of the electric field E.

the electric field of $\sim 3.5 \times 10^7$ V/cm at the tips vicinity is sufficient for triggering the field-emission current on the level of ~ 1 A/cm^2 (see **Figure 8**). The arc current density J_a needed to maintain a stationary hot spot can be estimated as [10-12]:

$$J_a \le I_i \cdot \left(e^{\phi_D - \phi_a} - 1 \right) \qquad (3)$$

Here $\varphi_D = e\,\varphi_f / T_e$ is the floating potential $_f$, normalized on the electron temperature T_e, $\varphi_a = U_a / T_e$ and I_i is the ion current from the plasma. The electron temperature is lower than the ion temperature due to cold electron emission from the arc spot and can be estimated from $(T_i - T_e)/T_i \le J_a/I_i$ [13]. From Equation (3) one can determine the ratio J_a/I_i as a function of the ion temperature T_i, as shown in **Figure 9**. It is seen that the arc current is a few times larger than the ion current for pure DT plasma and can be one order of magnitude larger in presence of tungsten impurities. Assuming that the plasma leakage from the vapour cloud to the plate is $j_i \sim 6 \times 10^{20}$ cm$^{-2} \cdot$s^{-1} and that the spot area is $S \sim \pi r^2 \le 0.01$ cm^2, one can estimate the ion current I_i ~ 1 A and for expected ion energies ≤ 100 eV (see **Figure 8**) the arc current from one spot $J_a \le 20$ A. Such a current density exceeds the minimum arc current needed for sustaining a unipolar arc [8, 9] and the associated surface heating by ions can result in the explosive formation of hot spots and a strong tungsten impurity ejection.

4. Discussion

In order to initiate an arc on even tungsten surfaces, in the quiescent operation stage, the floating voltage should exceed a critical value of ~ 24 V and the arc current must be at least $I_a \sim 10$ A [9]. In the presence of thermal electron emission and tungsten impurities in the vapour cloud surrounded the plate, the sheath floating potential was calculated in [12] and is within the range $\varphi_f \approx$
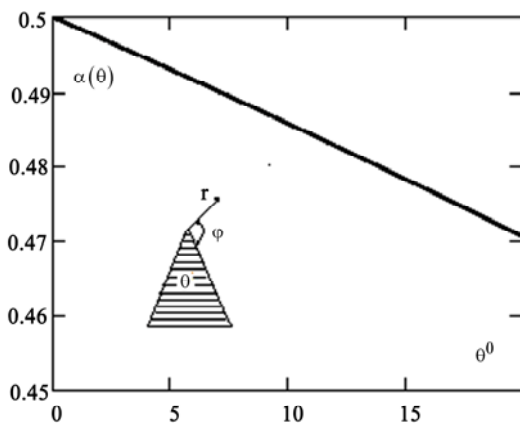

Figure 8. The degree of singularity α as a function of the wedge aperture θ.
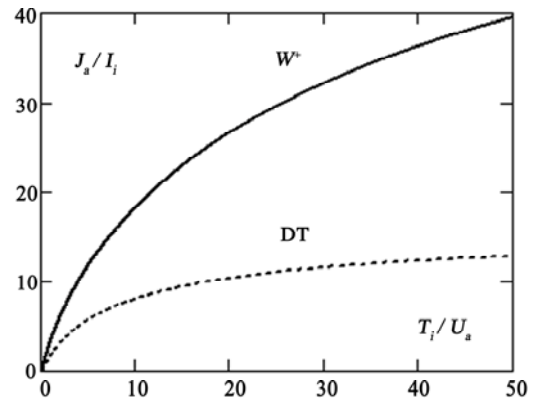

Figure 9. Arc current J_a as a function of plasma ion temperature T_i compared to that in the DT plasma.

$(2.5 - 0.5)\ T_e$. To reach the critical voltage drop for arc stationary burning, the minimum electron temperature needed is in the range of 10 - 50 eV. Such high electron temperatures, however, are unlikely at the first-wall surface of existing machines, therefore arcs are not expected. Even so, at the divertor plate, the arcs could ignite. However, the magnetic field intersecting the surface of the divertor plates prohibits arcs formation because it limits the plasma volume which can supply the electrons needed to close the arc current circuit.

In contrast, a corrugated surface surrounded by a vapour cloud facilitates the triggering of arcs and the closing of the arc current. Namely, the large value of the electric field ($> 3.5 \times 10^7$ eV/cm) yields a strong electron field emission that allows to achieve the minimum required arc current. The effect of the magnetic field does not appear explicitly in this case because the plasma itself has a large capacity to supply sufficient electrons to the plates, and a current loop can be formed through the plasma due to surface electric conductance, associated with electron scattering on the potential in homogeneity [11].

The creation of an arc is also facilitated by the existence of a dense vapour cloud and high ion density in front of the cathode spot. Only then will the electrons from field-emission be able to ionize the neutral atoms in the vapour cloud. The local heating derived from the consequent tungsten-ion bombardment can lead to metal evaporation. Considering that tungsten atoms are emitted at the melting temperature (3695 K), they will leave the surface with a thermal velocity of 4×10^5 cm/s. For a sheath potential of 20 eV and an electron density of 10^{13}cm^{-3}, the sheath width is about 1×10^{-3}cm and the time of flight for W atoms to enter the plasma would be 3×10^{-8} s - well within the duration of the ELM pulse. If, for instance, 10% of a monolayer of typically 3.6×10^{18} cm^{-2} is suddenly released from a surface spot, the neutral density in the sheath would locally increase up to 10^{20}

cm^{-3}. Assuming an ionization cross section of 2×10^{-16} cm^2, a small fraction of the neutral atoms (10^{-3}) would be ionized within the sheath, *i.e.*, $n_{iw} \sim 10^{17}cm^{-3}$. This would effectively increase the existing plasma density near the target. For this example, a W^+ ion produced in the sheath would need about several nanoseconds to fall back onto the surface.

Arcs erosion of tungsten according to vacuum data [9] is 0.62×10^{-4} g/coulomb and is proportional to the current flowing through the plate. Since the electron current forms a considerable part of the whole arc current, about $0.62 \times 10^{-4} \times 20$ A = 1.2 mg per second of tungsten material will be released into plasma from one spot. Arcs are triggered at each tip and one arc occurs from $1cm^2$ wedge surface (**Figure 1**), therefore, the contamination rate from the all divertor plates (~100 m² in ITER) may reach the level of 12 grams of tungsten per second or ~ 4 $\times 10^{22}$ tungsten impurity ions per second.

5. Conclusions

In this paper, we have demonstrated that repetitive ELM events in ITER discharges increase the probability of arcing on corrugated wedge-shape armour surfaces. Although tungsten is a refractory material and the probability of arcing is low in quiescent plasma, in the case of transients, unipolar arcs can ignite and strongly contribute to the erosion of the armour by ejecting tungsten impurities (neutral vapor, molten and solid droplets) into the plasma. Moreover, arcs at the wedge's tips may grow and eventually create hot spots. These have dominant thermal or burst-type emission that also releases a substantial amount of tungsten impurities into the plasma.

It is shown that the geometric enhancement of the electric field on the corrugated surface facilitates the arc triggering. We find that the electric filed at the wedges' tips reaches a value sufficient to originate intensive field electron emission. The tungsten arc erosion rate per each spot is estimated as 1.2 mg per second. We note that since sputtering of the tungsten armour by DT ions is ~ 10^{-2} tungsten atoms per incident DT ion (for energies $\leq$100eV), the arc erosion according to **Figure 9** is almost two orders of magnitude larger than that of sputtering yield, and comparable with self-sputtering yield.

6. Acknowledgments

7. References

[1] A. Loarte, G. Saibene, R. Sartori, *et al.*, "Transient Heat Loads in Current Fusion Experiments, Extrapolation to Iter and Consequences for its Operation," *Physica Scripta*, Vol. 128, 2007, pp. 222-228. doi:10.1088/0031-8949/2007/T128/043

[2] B. Bazylev, G. Janeschitz, I. Landman *et al.*, "ITER Transient Consequences for Material Damage: Modelling Versus Experiments," *Physica Scripta*, Vol. T128, 2007, pp. 229-233. doi:10.1088/0031-8949/2007/T128/044

[3] A. Zhitlukhin, N. Klimov, I. Landman *et al.*, "Effect of ELMS on ITER Armour Materials," *Journal of Nuclear Materials*, Vol. 363-365, 2007, pp. 301-307. doi:10.1016/j.jnucmat.2007.01.027

[4] B. Bazylev, G. Janeschitz, I. Landman and S. Pestchanyi, "Erosion of Tungsten Armor after Multiple Intense Transient Events in ITER," *Journal of Nuclear Materials*, Vol. 337-339, 2005, pp.766-770. doi:10.1016/j.jnucmat.2004.10.070

[5] L. Olson, G. Georgiou and W. Schultz, "An Efficient Finite Element Method for Treating Singularities in Laplace's Equation," *Journal of Computational Physics*, Vol. 96, No. 2, 1991, pp.391-410. doi:10.1016/0021-9991(91)90242-D

[6] S. Marchetti and T. Rozzi, "Electric Field Behavior near Metallic Wedges," *IEEE Transactions on Antennas and Propagation*, Vol. 38,No. 9, 1990, pp.1333-1339. doi:10.1109/8.56983

[7] L. Landau, E. Lifshitz and L. Pitaevskii, "Electrodynamics of Continuous Media," Vol. 8, 1984 (1rst Ed.), Butter-Worth-Heinemann, ISBN 978-0-750-62634-7.

[8] V. Granovski, "The Electric Current in a Gases," (in Russian), Nauka, Moscow, 1971.

[9] J. Wesson, "Tokamaks," 3rd edition, Oxford, 2004.

[10] G. Hobs and J. Wesson, "Heat Flow through a Langmuir Sheath in the Presence of Electron Emission," *Plasma Physics*, Vol. 9, 1967, pp. 85-87. doi:10.1088/0032-1028/9/1/410

[11] Yu. Igitkhanov, "On the Mechanism of Stationary Burn of Unipolar Micro-Arcs in the Scrape-Off Tokamak Plasma," *Contribution in Plasma Physics*, Vol. 28, No. 4-5, 1988, pp. 421-425. doi:10.1002/ctpp.2150280425

[12] Yu. Igitkhanov and D Naujoks, "Sheath Potential Drop in the Presence of Impurities," *Contribution in Plasma Physics*, Vol. 36 S, 1996, pp. 67-72.

[13] A. Nedospasov and V. Petrov, "Model of the Unipolar Arc on a Tokamak Wall," *Journal of Nuclear Material*, Vol. 76 & 77, 1978, pp. 490-491.