

Influence of Alloy Elements on the Osteoconductivity of Anodized Ti-29Nb-13Ta-4.6Zr Alloy

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ABSTRACT

Anodizing is expected to be an effective method to improve the osteoconductivity of the Ti-29Nb-13Ta-4.6Zr (TNTZ) alloy because the bioactivity of anodized Ti is good. However, it is not known how the alloy elements influence the surface roughness, composition, hydrophilicity, and osteoconductivity of the anodized film on the Ti alloy. In this study, we investigated the effects of anodizing on the surface properties and the osteoconductivity of the anodized TNTZ alloy, focusing on the functions of the individual alloy elements. The anodized oxides of the Nb, Ta, and Zr metals were hydrophobic at all the voltages applied, in contrast to the anodized oxide of Ti. As well as pure Ti, a TiO₂-based oxide film formed on TNTZ after anodizing. However, the oxide film also contained large amounts of Nb species and the molar Nb/Ti ratio in the TNTZ alloy was high, which makes the surface more hydrophobic than the anodized oxide on Ti. *In vivo* tests showed that the osteoconductivity of the TNTZ alloy was sensitive to both its surface roughness and hydrophilicity. When the TNTZ alloy was anodized, the process increased either the surface hydrophobicity or the surface roughness at the voltage used in this study. These changes in the surface properties did not improve its osteoconductivity.

Keywords: Ti-29Nb-13Ta-4.6Zr; Anodizing; Titanium Dioxide; Alloy Element; Hydrophilicity; Osteoconductivity

1. Introduction

A new single β type Ti alloy, Ti-29Nb-13Ta-4.6Zr (TNTZ), has been developed for biomedical applications [1,2]. Because this alloy has a lower Young's modulus than pure Ti or conventional Ti alloys, such as the Ti-6Al-4V alloy, the use of this alloy as a bone substitute is expected to suppress the bone resorption caused by the stress shielding effect, which arises when the Young's modulus of the implant material is higher than that of natural bone. However, despite its improved mechanical biocompatibility, the problem remains that the osteoconductivity of TNTZ is as low as that of pure Ti and the Ti-6Al-4V alloy [3]. Therefore, surface modification is required to change the surface chemical properties of the TNTZ alloy to improve its osteoconductivity.

Hydroxyapatite (HAp) coatings are widely used as a conventional surface modification for pure Ti to improve its osteoconductivity [4-12]. The anodizing process has also been investigated as a chemical surface treatment for

pure Ti, and improves the osteoconductivity of Ti as much as HAp coatings do, by forming a TiO₂ film [13, 14]. Previous studies have shown that the chemical properties of TiO₂ films, such as the surface roughness [13,15] crystal structure and crystallinity of TiO₂ [13,16,17] film thickness [13,18] and hydrophilicity [14,19,20] can differ depending on the anodizing conditions, resulting in different osteoconductivities. In particular, a fine and hydrophilic surface was found to be better for the early fixation of bone onto anodized TiO₂ coatings.

However, when we anodized the TNTZ alloy, Nb, Ta, and Zr are also contained in the oxide coating in addition to Ti [3] which may disturb the formation of a TiO₂ film on the TNTZ alloy. It is unclear how the alloy elements influence the surface roughness, composition, hydrophilicity, and osteoconductivity of the anodized film on the Ti alloy. Therefore, we investigated the influence of the Nb, Ta, and Zr species on the surface properties of the anodized TNTZ alloy in an aqueous solution of H₂SO₄, by

comparing the component metals of the TNTZ alloy. The osteoconductivity of the anodized films on the TNTZ alloy was then evaluated in *in vivo* tests.

2. Materials and Methods

2.1. Preparation of Substrates

Disks (surface area of 1.13 cm²) and rods (2 × 5 mm) of TNTZ alloy were used as substrates to prepare anodized films for their surface analysis and for *in vivo* tests, respectively. Disks (area = 0.79 cm²) of single metals (cp-Ti, Nb, Ta, and Zr) and those (area = 1.00 cm²) of binary alloys (Ti-35.2Nb [TN], Ti-19.6Ta [TT], and Ti-7.9Zr [TZ], prepared by arc melting), and Ti-6Al-7Nb (Ti67) were used to evaluate the films on the TNTZ alloy in detail. The composition of each binary alloy was controlled to ensure the same Nb/Ti, Ta/Ti, and Zr/Ti molar ratios as occur in the TNTZ alloy, as shown in **Table 1**. All of the substrates were polished with emery paper and then with buffing using Al₂O₃ particles (particle size = 0.05 μm), to produce mirror-finished surfaces (Ra/μm < 0.1). After polishing, the substrates were cleaned and degreased with distilled water and ethanol, and then anodized.

2.2. Anodizing of the Substrates

A substrate and a Pt coil were set as the anode and cathode, respectively, and no reference electrode was used. Anodizing was performed in a 0.1 M H₂SO₄ aqueous solution (pH = 1.0) with an applied voltage that increased from 0 V up to 200 V at a rate of 0.1 V·s⁻¹. After anodizing, the sample was sterilized at 394 K for a period of 20 min in an autoclave unit.

2.3. Analysis of the Coatings

The surface morphology was examined with scanning electron microscope (SEM). The crystal structures of the anodized films were determined using X-ray diffraction (XRD). The chemical compositions of the anodized films on the surfaces were analyzed using X-ray photoelectron spectroscopy (XPS). The anodized films were etched

Table 1. Molar ratios of Nb, Ta, and Zr to Ti in the TNTZ, TN, TT, and TZ alloys.

	Molar ratio of alloy elements to Ti in the alloy		
	Nb	Ta	Zr
TNTZ	0.280	0.064	0.045
TN	0.280	—	—
TT	—	0.064	—
TZ	—	—	0.045

with Ar ion bombardment (at 2 kV) and depth profiles were obtained using Auger electron spectroscopy. Surface roughness was measured using confocal laser scanning microscope with a measurement area of 150 × 112 μm², and expressed with the arithmetical mean of the surface roughness (Ra). The water contact angle (WCA) was measured at three different points for each sample using a 2 μL droplet of distilled water after 24 h in air, and the average value was used as the WCA value.

2.4. In Vivo Test

Because the experimental procedure for our *in vivo* study was almost the same as that described in previous reports [9], it is described only briefly here. Before surgery, all the implants were cleaned in distilled water and immersed in a chlorhexidine gluconate solution. Ten-week-old male Sprague Dawley rats (Charles River Japan, Inc., Tokyo, Japan) were used in our experimental procedures. The specimens were implanted in the tibial metaphysis of the rats. A slightly oversized hole, which did not pass through to the rear side of the bone, was created using a low-speed rotary drill. Subsequently, the implants were inserted into these holes, and then the subcutaneous tissue and skin were closed and sterilized.

The rats were sacrificed after a period of 14 d, and the implants with their surrounding tissue were retrieved. The specimens were fixed in a 10% neutral buffered formalin solution, dehydrated in a graded series of ethanol, and embedded in methylmethacrylate. Following polymerization, each implant block was sectioned into 20 μm thick slices. These sections were then stained with toluidine blue.

The sum of the linear bone contact with the implant surface was measured and was expressed as a percentage over the entire implant length (the bone-implant contact ratio, R_{B-I}) in the cortical bone part. Significant differences in the bone-implant contact ratio were analyzed statistically using the Tukey-Kramer method [21]. Differences were considered statistically significant at the $p < 0.05$ level. This animal study was conducted in the laboratory of the Association for Assessment and Accreditation of Laboratory Animal Care (AAALAC) International.

3. Results and Discussion

3.1. Film Properties

3.1.1 Anodizing of Single Metals

Figures 1-3 show the surface morphology, XRD pattern, and WCA, respectively, of each of the metals at different applied voltages.

The surface of all the metals became rougher as the applied voltage increased (**Figure 1**). At Ra/μm > 0.1, many pores were formed on their surfaces, although the

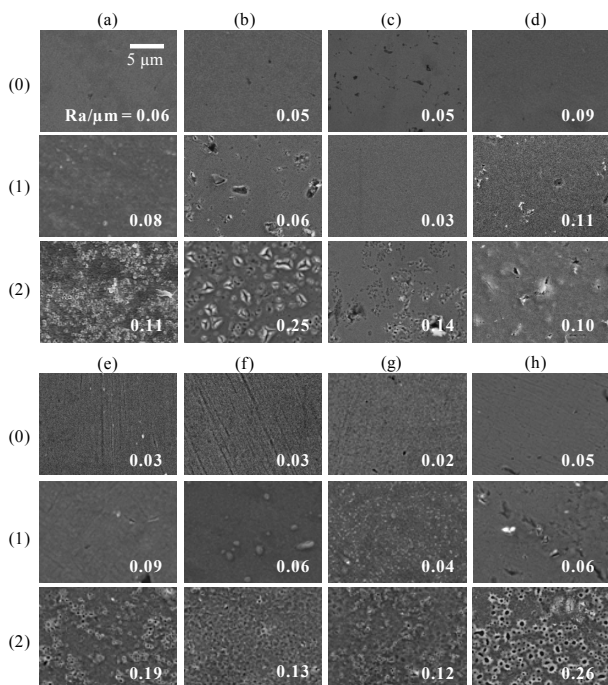


Figure 1. Surface SEM images and surface roughness (Ra) of (a) Ti, (b) Nb, (c) Ta, (d) Zr, (e) TN, (f) TT, (g) TZ, and (h) TNTZ, each of which was (0) as-polished or anodized at a voltage of (1) 100 V or (2) 200 V in a 0.1 M H₂SO₄ aqueous solution.

degree of roughness differed depending on the type of metal. An oxide film was formed on Ti as the applied voltage increased. At voltages above 100 V, anatase-type TiO₂ was detected in the XRD pattern (Figure 2(a)). The other single metals (Nb, Ta, and Zr) also formed oxide films as the applied voltage increased: ZrO₂ was detected on anodized Zr at voltages above 100 V (Figure 2(d)), and Nb₂O₅ on anodized Nb at a voltage of 200 V (Figure 2(b)), but no oxide peak was detected on anodized Ta at any voltage (Figure 2(c)). Because the oxide is in an

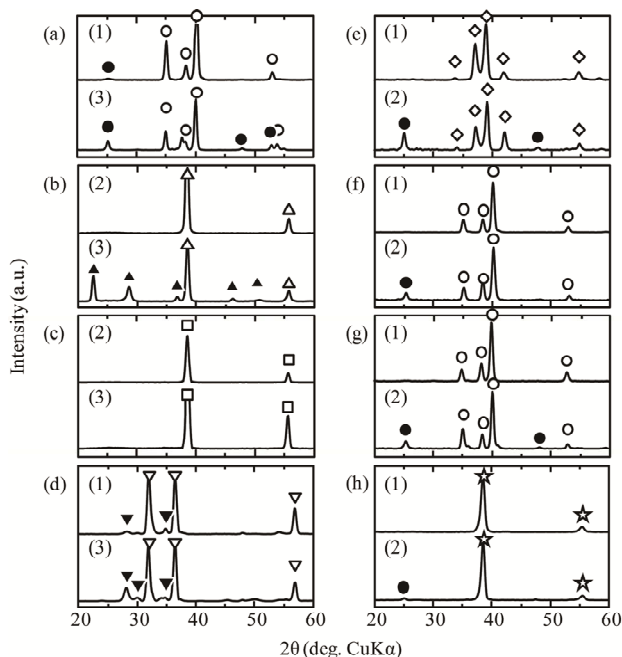


Figure 2. XRD patterns of (a) Ti, (b) Nb, (c) Ta, (d) Zr, (e) TN, (f) TT, (g) TZ, and (h) TNTZ, each of which was anodized at a voltage of (1) 100 V, (2) 150 V, or (3) 200 V in a 0.1 M H₂SO₄ aqueous solution. Symbols: ○ = α-Ti, ☆ = β-Ti, △ = Nb, □ = Ta, ▽ = Zr, ◇ = Ti₄Nb, ● = TiO₂ (anatase), ▲ = Nb₂O₅, and ▼ = ZrO₂.

amorphous form in the first stage of the anodizing of these metals, anodized films that do not have oxide peaks in the XRD pattern are considered to consist of amorphous oxides [22,23].

All the as-polished metals showed similarly high WCA in the range of 50 - 70 (deg.) (○ □ △ ▽ at 0 V in (a)). When Ti was anodized, the WCA decreased to less than 30 (deg.) at 100 V, and decreased further at above 150 V (○ in Figure 3(a)). This is consistent with the previous report that stated that roughness reduces the WCA

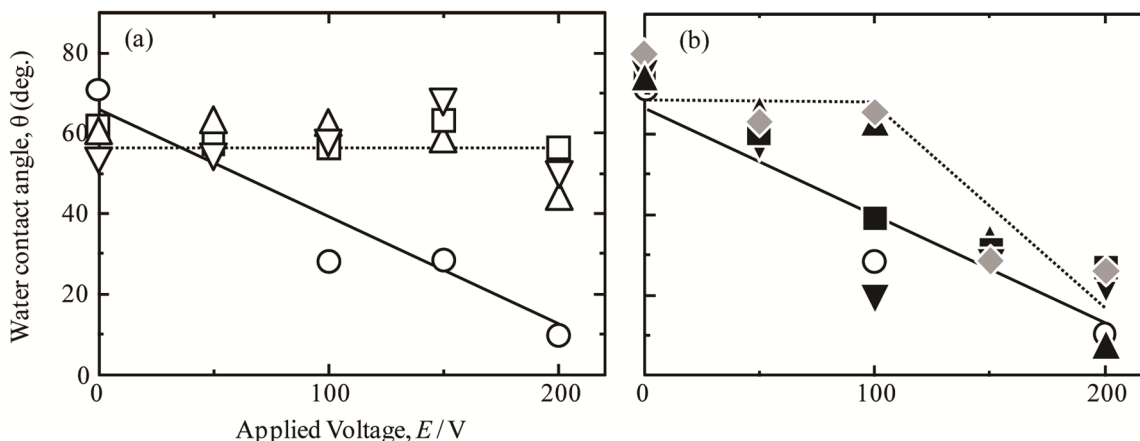


Figure 3. Relationships between WCA and anodizing voltage applied to (a) single metals and (b) Ti-based alloys in a 0.1 M H₂SO₄ aqueous solution. Symbols: ○ = Ti, △ = Nb, □ = Ta, ▽ = Zr, ▲ = TN, ■ = TT, ▼ = TZ, and ◆ = TNTZ.

if its value on the unroughened surface of the same material is < 90 (deg.) [24]. However, the WCA of the other single metals did not change with increasing surface roughness, but maintained high values of ≥ 50 (deg.) (Δ , \square , ∇ in (a)). This indicates that the anodized oxides of Nb, Ta, and Zr show low compatibility with water, which cancels the effect of surface roughness.

Surface hydrophilicity is often related to surface OH groups and adsorbed hydrocarbons. **Figure 4** shows the quantitative relationship between these chemical species and WCA. Analysis of the spectrum was performed as in our previous report [14]. In this figure, the amounts of OH groups and adsorbed hydrocarbons are normalized as ratios to $[O^{2-}]$, because the peak intensity can be affected by the vacuum conditions during the analysis. The samples shown in this figure were limited to those with $Ra/\mu\text{m} < 0.1$ to exclude any morphological influence on WCA. Whichever metal was used, the amounts of OH groups and adsorbed hydrocarbons varied as the applied voltage changed. In particular, the use of different types of metals produced very different values for $[-OH]/[O^{2-}]$ or $[C-H]/[O^{2-}]$. This means that each of the anodized metals, or more precisely the anodized oxides, had different potential to bind OH groups or adsorb hydrocarbons on its surface. In contrast, the WCA of anodized Zr was much higher than that of anodized Ti, even with

lower $[C-H]/[O^{2-}]$ and similar $[-OH]/[O^{2-}]$. This indicates that the effects of the OH groups or adsorbed hydrocarbons on hydrophilicity differed, depending on the type of underlying oxide. Therefore, the hydrophilicity of different types of oxides cannot be explained simply by the values for $[-OH]/[O^{2-}]$ or $[C-H]/[O^{2-}]$, and the influence of the underlying oxides must also be considered. However, it was not clear in this study.

3.1.2. Anodizing Ti Alloys

Oxide films were formed on all of the binary alloys and the TNTZ alloy after anodizing. At voltages lower than 100 V, no oxide peaks were detected for those alloys with XRD (**Figures 2(e) (1), (f) (1), (g) (1) and (h) (1)**). The surfaces of these samples were fine ($Ra/\mu\text{m} < 0.1$) (**Figures 1(e) (1), (f) (1), (g) (1) and (h) (1)**). At voltages above 150 V, anatase was detected on all of the alloys (**Figures 2(e) (2), (f) (2), (g) (2) and (h) (2)**) and their surfaces were roughened by surface pores (**Figures 1(e) (2), (f) (2), (g) (2) and (h) (2)**). No oxides of Nb, Ta, or Zr species were detected with XRD, even after the highest voltage of 200 V was applied (**Figures 2(e) (2), (f) (2), (g) (2) and (h) (2)**). However, the depth profiles revealed that an Nb species was present in the anodized film on the TN and TNTZ alloys (**Figure 5(c) (2)**). The chemical composition of the anodized film seemed to re-

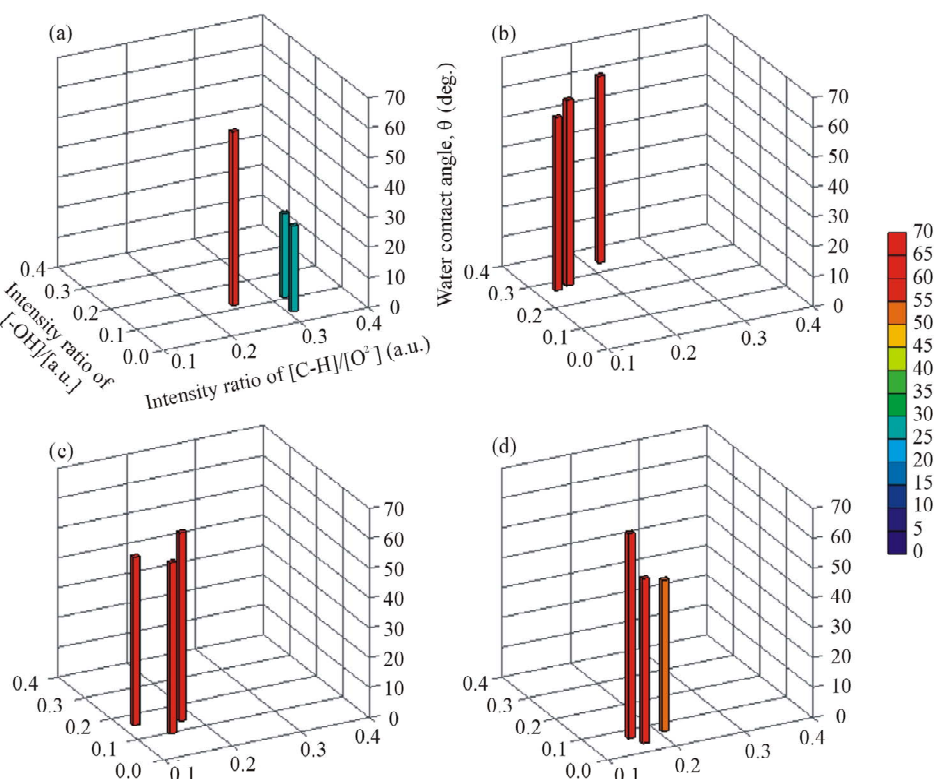


Figure 4. Quantitative relationships among surface OH groups, adsorbed hydrocarbons, and WCAs for single metals, (a) Ti, (b) Nb, (c) Ta, and (d) Zr, that were anodized at a voltage of 50, 100, or 150 V in a 0.1 M H_2SO_4 aqueous solution. The amounts of $[-OH]$ and $[O^{2-}]$ were calculated from the O1s spectra of the XPS analysis, and of $[C-H]$ from the C1s spectra.

main constant at any applied voltage below 150 V, because the Nb/Ti ratio in the film was constant with depth. The Nb/Ti ratio in the anodized films did not change when 0.1 M H_3PO_4 was used instead of 0.1 M H_2SO_4 for anodizing, as in our previous study [3]. However, little Ta or Zr species were present near the surface of the anodized TT or TZ, respectively (**Figures 5(d) (2) and (e) (2)**). This means that the surface compositions of the anodized TT and TZ alloys were similar to that of anodized pure Ti, unlike those of the anodized TN and TNTZ alloys.

There was no difference in WCA among the Ti alloys before anodizing, but in the samples with $Ra/\mu m < 0.1$, a difference was clearly seen after anodizing, depending on the type of alloy examined. The WCA of the TT and TZ alloys decreased to 20 - 40 (deg.) after a voltage of 100 V

was applied, in the same way that the WCA of pure Ti decreased. This also indicates that whether the oxide was amorphous or anatase did not influence the WCA. However, the WCA of the TN and TNTZ alloys, which contained Nb species in the oxides, remained at about 60 (deg.) after the same voltage was applied.

To understand the effect of Nb on surface hydrophilicity, Ti67, which also contains Nb as an alloy component, was anodized in 0.1 M H_2SO_4 with 100 V and formed an oxide film with a fine surface ($Ra/\mu m < 0.1$). The oxide contained Nb species, but was hydrophilic, with a WCA of 20 (deg.), unlike the TN and TNTZ alloys. The content of the Nb species in the oxide film was evaluated, as shown in **Table 2**. The Nb/Ti ratio in the anodized film was much lower for the Ti67 alloy than

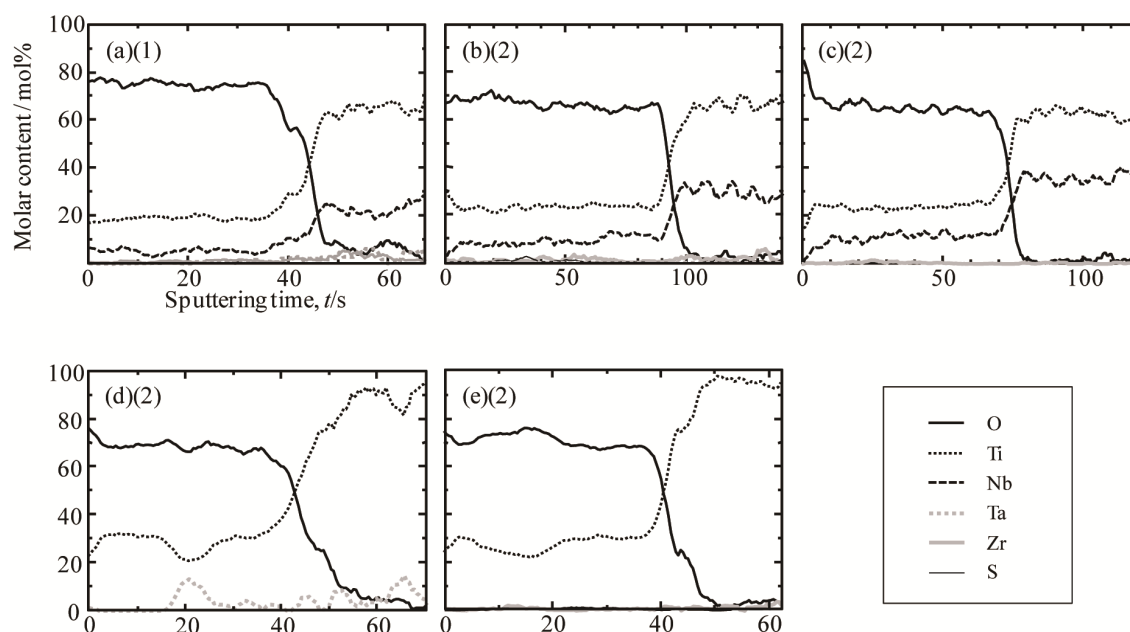


Figure 5. Depth profiles of (a) (b) TNTZ, (c) TN, (d) TT, and (e) TZ, each of which was anodized at a voltage of (1) 100 V or (2) 150 V in a 0.1 M H_2SO_4 aqueous solution.

Table 2. Average molar ratios of Nb, Ta, Zr, and Al to Ti in the anodized films and in the substrates TNTZ, TN, TT, TZ, and Ti67, estimated from depth profiles.

Specimen	Solution	Voltage/V	Average molar ratio of alloy elements to Ti							
			Nb		Ta		Zr		Al	
			Film	Substrate	Film	Substrate	Film	Substrate	Film	Substrate
TNTZ	0.1 M H_3PO_4	100	0.37	0.45	0.00	0.00	0.06	0.08	—	—
			0.28	0.35	0.02	0.06	0.04	0.04	—	—
			0.40	0.39	0.01	0.02	0.06	0.03	—	—
TN	0.1 M H_2SO_4	150	0.36	0.55	—	—	—	—	—	—
TT			—	—	0.20	0.08	—	—	—	—
TZ			—	—	—	—	0.03	0.02	—	—
Ti67		100	0.06	0.03	—	—	—	—	0.02	0.02

for the TN and TNTZ alloys. Because at least 20% of Nb ions are reported to be soluble in TiO_2 [25], it is thought that Nb_2O_5 dissolves into TiO_2 to some degree and forms a solid solution, but comes to exist as a second phase when the oxide contains high amount of Nb species. The second phase of Nb_2O_5 seems to have increased the WCA, when the high WCA of anodized Nb is increased (Δ in **Figure 3(a)**). Similar effects may possibly be caused by Ta and Zr if their concentrations are high in the anodized film, but this was not confirmed in this study.

At surface with $R_a/\mu\text{m} > 0.1$, the WCA of the anodized TN and TNTZ alloys decreased to ≤ 40 (deg.), as in the other binary alloys. From results described above we conclude that when anodizing is used as a surface treatment for the TNTZ alloy, a low WCA cannot be achieved on a fine surface ($R_a/\mu\text{m} < 0.1$) but can be achieved on a rough surface ($R_a/\mu\text{m} > 0.1$). Therefore, the samples for the *in vivo* tests were prepared under the following conditions: (1) anodizing in 0.1 M H_2SO_4 at 100 V, to produce a sample with a fine and nonhydrophilic surface, and (2) anodizing in 0.1 M H_2SO_4 at 150 V, to produce a sample with a rough and hydrophilic surface.

3.2. In Vivo Test

The R_{B-I} values for the anodized TNTZ samples in the cortical bone part are shown as a function of WCA in **Figure 6**. Our previous results for surface-treated Ti, Ti67, and TNTZ ($R_a/\mu\text{m} < 0.1$) are also plotted on the figure [3,14]. For the sample anodized at 100 V (**Figures 6(a)** and **(d)**), R_{B-I} was as low as that for the as-polished sample. This value is consistent with the values for anodized Ti showing the same WCA, which are fitted to the curve in **Figure 6**. For the sample anodized at 150 V (**Figure 6(b)**), R_{B-I} was also as low as that for the as-polished sample, but the R_{B-I} value was lower than the values for anodized Ti with similar WCA. This is because the increase in surface roughness reduced the hard tissue formation on the sample in the range of $0.1 < R_a/\mu\text{m} < 0.3$ [15]. In contrast, WCA of the anodized Ti67 alloy also fitted the curve, as did that of the TNTZ sample anodized at 100 V. This means that the R_{B-I} values of these alloys tended to change with WCA, in the same way as for pure Ti, and did not depend on the type of base metal. It is also clear that the surface Nb species influenced hydrophilicity of the alloy but did not directly negatively affect the formation of hard tissue in the living body. This result supports the proposition that Nb species are not cytotoxic to osteoblast cells [26]. It is important that the R_{B-I} values of different types of alloys treated with different anodizing conditions were simply ordered according to their WCAs, even though their surface compositions were quite different. All these data seems

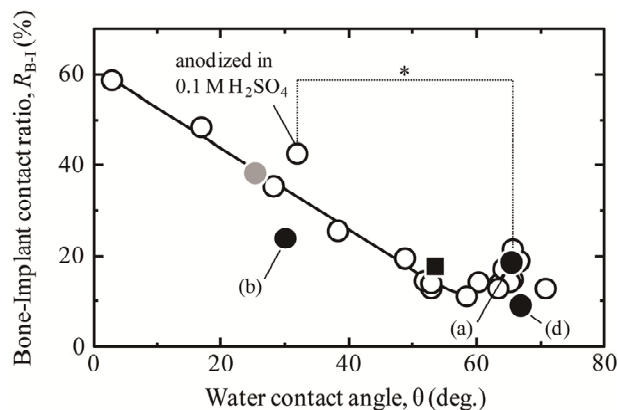


Figure 6. The relationship between WCA and RB-I in the cortical bone part of ●: TNTZ specimens anodized in (a) 0.1 M H_2SO_4 solution up to 100 V, (b) 0.1 M H_2SO_4 solution up to 150 V, or (d) 0.1 M H_3PO_4 solution up to 100 V, ● = Ti67 alloy anodized in 0.1 M H_3PO_4 solution up to 100 V, ■: as-polished TNTZ specimen, and ○: anatase-coated Ti specimen with the same surface roughness ($R_a/\mu\text{m} < 0.1$), prepared with different treatments [17]. * $p < 0.05$.

to recommend that a hydrophilic surface be fabricated on TNTZ to improve its osteoconductivity, and that is one of goals in our future work.

4. Conclusions

In this study, we investigated the influence of the Nb, Ta, and Zr species on the surface properties of the TNTZ alloy after its anodizing in an aqueous solution of H_2SO_4 . We then evaluated the osteoconductivity of the anodized films of the TNTZ alloy in *in vivo* tests. The following results were obtained:

- 1) The anodized oxides of the Nb, Ta, and Zr metals were hydrophobic at any applied voltage, unlike the single metal Ti.
- 2) As well as pure Ti, a TiO_2 -based oxide film formed on TNTZ after anodizing. However, the oxide film also contained high amounts of Nb species because the molar Nb/Ti ratio in the TNTZ alloy substrate is high, and this made the surface more hydrophobic than the anodized oxide on Ti.
- 3) The *in vivo* test showed that the osteoconductivity of the TNTZ alloy was sensitive to both surface roughness and hydrophilicity. When the TNTZ alloy was anodized, the process increased either the surface hydrophobicity or the surface roughness at the voltages used in this study. These changes in its surface properties did not improve the osteoconductivity of the TNTZ alloy.

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