



Geometric Accuracy Design Method of Roller Cavity Surfaces for Net-Shape Rolling Compressor Blades

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Abstract

The accurate shape of roller cavity surfaces is vital part for net-shape rolling. This paper presents a new design method of roller cavity surfaces with high accuracy for rolling compressor blades based on the geometrical inheritance and evolution of the net-shape profiles. Firstly, a process model of the blade is modeled by adding process allowance and locating basis at the CAD (Computer Aided Design) model of the blade to represent the roll formed blade, the process model inherits the net-shape profiles of the blade at the pressure and suction surfaces. Secondly, an algorithm is proposed to discretize a curve to a set of ranked points with the restriction of the maximum chord height, and a new section curve which represents the geometrical feature of the pressure and suction surfaces are distributed on the process model based on the algorithm. Finally, a mapping algorithm is proposed to transform the section curves to the cavity section curves around the roller axis based on the conjugate movement between rollers and blade, and the cavity surfaces are reconstructed based on the transformed section curves. The design method is implemented for the roller cavities of a variable cross-section compressor blade, and the accuracy of the designed cavities is checked based on the precision of the roll formed blade by the finite element method. The results reveal that the designed cavities achieved the net-shape precision at pressure and suction surfaces of the blade. The paper provides an effective method for designing rolling cavity surfaces with excellent design quality.

Subject Areas

Aerospace Engineering, Mechanical Engineering

Keywords

Rollingblade, Cavity Design, Process Model, Section Curves, Discretizing Algorithm, Transformation Algorithm

1. Introduction

Rollforming is one kind of important machining method of high compressor blade, due to the characteristics of the rolling blade with large quantity, thin thickness, and high precision requirement. In a blade rolling process, a blank is rolled between a pair of rotated rollers with a shaped surface and produced plastic deformation. With the cross sectional shape being progressively decreasing, a blade is printed along the rolling direction at the outlet. In order to meet the high precision required by manufacture and good uniformity demanded by assembly, an accurate shape of rolling cavity is necessary for blade rolling.

In previous studies, many works have been done on rolling process, such as rolling parameter optimization [1] [2], rolling contact condition analysis [3] [4] and microstructure estimation [5] [6] by theoretical analysis, experimental study and the finite element method. Most of those works were based on the inerratic shape of product and ignored the profile shape which was the most important factor in rolling forming. For rolling complex components such as twisted blades, a reasonable design method of roller cavity affects manufacture precision and service life of roller. Sedighi and Mahmoodi [7] [8] proposed an approach for simulation of cold rolling blade. The rolling contact pressure distribution on blade distributed as a saddle shape. Meanwhile, the rolling force was studied to adjust the gap between two dies in order to improve the accuracy of the blade. Lu *et al.* [9] used a B-spline surface approximation to improve die surface quality for die shape representation by minimizing the total forging tolerances in an FEM (Finite Element Method) simulation. Sung *et al.* [10] designed the parameters of the two roll grooves by given equations for rolling oval rebar, and developed the equations by performing finite element simulations and examining variations in the design parameters dependent on rebar size. Because of elastic deformation and thermal distortion, Ou *et al.* [11] developed a forging simulation and optimization system to reduce forging deviation. In order to design a profile of tooth-shaped rolls for rolling I-shaped profile steel with corrugated web, Ma and Zhang [12] used the curve equations of corrugated web to set up the rollers. Kiuchi *et al.* [13] designed a roller profile for reshaping round pipes into non-circular pipes based on investigating deformation features and the designed profiles were suitable for making the required products. Li *et al.* [14] used two integral flexible rolls as the forming tool for sheet metal parts. A non-uniform elongation in the rolling direction and a bending deformation in the thickness direction occur simultaneously, and finally three-dimensional surface parts are formed. Cai [15] analyzed the kinematic relation between the surface of rolling die and that of forging piece during the roll-forging process, and an approach for

the precision design of rolling dies was presented based on the conjugate principle. All of those works were based on given die or roller profile which could be described by a formula. Indeed, few work focus on designing a roller cavity for rolling a complex component with varying cross section.

The conjugate movement between rollers and component is fundamental for designing roller cavity. Cai [15] stated that cavity design for rolling process is a sophisticated task due to the complex relative motion between dies and the plastic deformation of the roll-forging pieces. Zhang *et al.* [16] investigated the motion characteristic between the die and the workblank under varied center distance in rolling spline. According to the kinematic relation of the rolling process, the roller cavity design is different from the cavity design for casting, which is almost a copy of the component's profile. The rolling cavity is a varied and semi-closed gap between a pair of rotated roller, and cavity surfaces are enwound from component's profiles. Zhao *et al.* [17] designed the arc length of groove of roller based on predicted forward slip value for rolling a revolving component with changeable thickness. Most of the roller for rolling complex components is achieved by trial and error. It prolongs the setting time, and cannot meet the requirement of high manufacturing accuracy either. In a rolling process, the blank deforms continuously within an open gap, which is shaped by a pair of rotating rollers. The blank is squeezed and experienced plastic deformation, and the excrescent material, *i.e.* overflow, is generated at two sides of the roller gap. The blank is rolling formed to an expanded shape of the blade after the blade rolling process. In order to characterize the expanded shape, the original blade CAD model is inlaid into the expanded model, which is named as the process model of blade. Hence, design the process model based on the CAD model of the blade is the first step for designing roller cavity. Then, the pressure and suction surfaces of the process model are mapped to cavity surfaces based on a transforming algorithm. Chan *et al.* [18] proposed a new fitness function for family mould layout design optimization, and considered the accurate requirement.

In order to design the roller with acceptable accurate requirement for a complex part, it is vital for transforming the profile of the rolled part to the cavity surfaces of the rollers. In this paper, a numerical design method for blade rolling cavity surfaces is studied with geometric inheritance of the blade's profiles. The rolling cavity design process is demonstrated for a high compressor blade with varying cross-section, and the simulative method are implemented to estimate the designed cavities. The results show that the rolling formed blade achieved net-shape at pressure and suction surface when using the designed roller. The proposed design method of roller cavity surfaces surmounts traditional method which based on trial and error, and shortens the setting period of roller with a high design precision.

2. Outline of the Cavity Surface Design Method

This paper proposes a new method to design roller cavity surfaces for complex

part based on geometrical inheritance and evolution, and the geometrical inheritance and evolution accuracy of the part is emphasized. A stator blade model of compressor is used to illustrate the design method of the rolling cavity surface. The original cross section curves of the blade and CAD model of the blade are showed in **Figure 1(a)** and **Figure 1(b)** respectively. The flowchart of the design method is presented in **Figure 2**. Firstly, a process model is designed by inheriting the profiles from the CAD model of blade. Secondly, a new section curve distribution is created on the process model based on a discretizing algorithm which is also used in following parts, and the new section curves should represent the geometrical characteristics of the process model. Finally, the section curves are transformed to the section curves of the cavity surface based on a transformation algorithm, the transforming accuracy of the corresponding section curves are assured by the discretizing algorithm. The rolling cavity surfaces are created

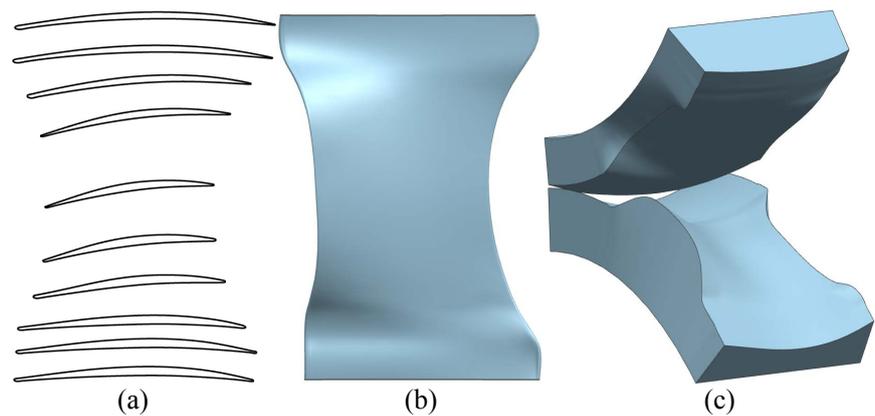


Figure 1. CAD models of a representative compressor blade and its corresponding roller: (a) Original cross section curves of the blade; (b) Overview of the compressor blade; (c) Overview of the roller for the rolling blade.

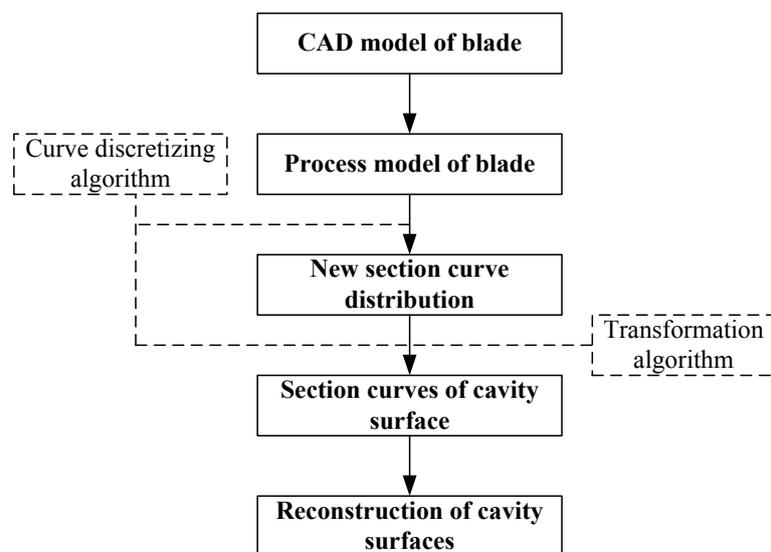


Figure 2. Flowchart of the design method for the rolling cavities.

based on the transformed section curves and the rolling dies are created based on designed cavity surfaces. The designed roller for the blade is showed in **Figure 1(c)**.

3. Details of the Roller Cavity Surface Design Method

According to the flowchart of the method to design the rolling cavities for producing compressor blades, the development of the process model, the creation of the section curves of the process model, and the creation of section curves of the cavity are discussed below in details.

3.1. Development of Process Model

The process model is an imaginary model based on the CAD model of the blade to describe the shape of the blade blank after rolling process. It inherits and develops the geometrical characteristic of the pressure and suction surface of the blade, and intermediates the original blade model to the rolling cavity model. The process model is represented by its cross section curves, which are evolved from the section curves of the original CAD model of blade. The overflow boundaries at the leading and trailing edges are added to the suture pressure and suction surface. The machining allowances are added by extrapolating the root and top section curves of the blade to ensure integrity of the blade profiles. A location block is also appended at the root section of process model for holding and positioning in manufacturing process. The process model evolves from the original blade CAD model, and it seems like that the compressor blade inlaid in the process model. The procedure of developing process model is presented as followed.

3.1.1. Addition of Rolling Overflows on Original Section Curves of Blade

In order to minimize machining allowance at the leading and trailing edges to suture the pressure and suction surfaces by an arc smoothly after rolling, meanwhile, to avoid misrun defect on the pressure and suction surface, the convergent overflow boundaries are added at the leading and trailing edges of every cross section curve. First, an unbroken section curve is discretized to many points confined by a chord height tolerance Δ which is the same as the blade tolerance (it is 0.02 mm in this paper). The leading and trailing edges are matched by circles respectively. The discretized points are divided into four groups which describe the leading edge curve, the pressure surface curve, the trailing edge curve and the suction surface curve respectively, see **Figure 3(a)**. Every unbroken section curve of CAD blade model is divided into four curves by fitting the relevant points. The four curves are showed in **Figure 3(a)**. Then, the mean camber curve is sketched through the center points of the inscribed circles between the compressed surface and the suction surface. The two endpoints on the mean camber curve of blade are extended by twice of the radius of leading and trailing edges along the tangential direction, see **Figure 3(b)**. The mean camber curve of the cross section of the process model is created by smoothing the two extended

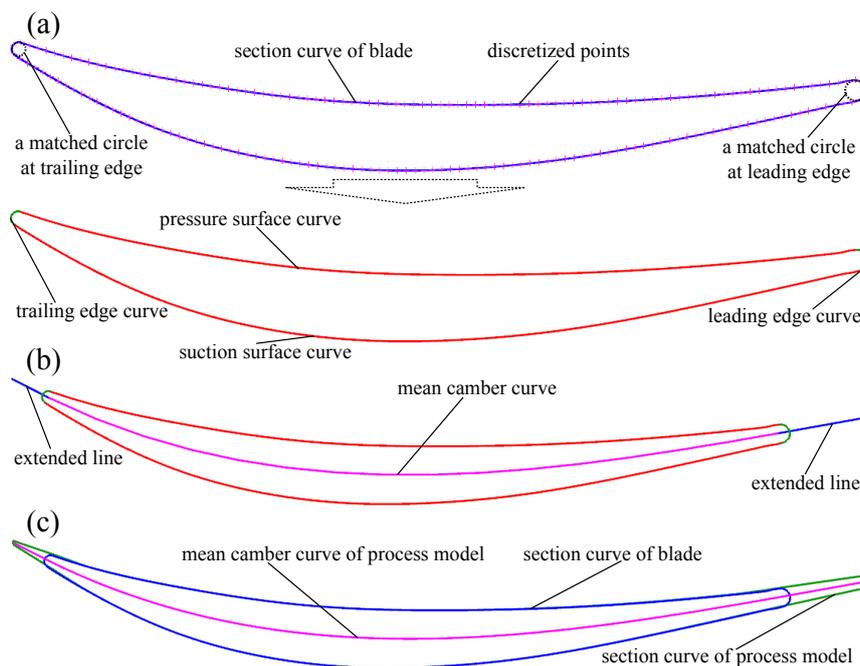


Figure 3. Constructing a typical cross section of a process model from the cross section of the original CAD model of the blade. (a) Section curve of the blade with discretized points. (b) Mean camber curve of the blade section curve. (c) Section curve and mean camber curve of the process model.

lines and the mean camber curve of the blade, see **Figure 3(c)**. The two end-points on the mean camber curve of processor model are offset to two sides as relevant radius of leading and trailing edges. The offset points are connected and smoothed to the pressure surface curve and suction surface curve, and the smoothed curves are the section curves of the process model. The original section curve, mean camber curve and section curve of a representative cross section of the process model are showed in **Figure 3(c)**. After adding the overflow boundaries on every theoretical cross section of the blade, a CAD model which represents the shape of the blade after rolling is structured through the closed section curves of the process model sequentially.

3.1.2. Addition of Auxiliary Units

A wire electrode cutting process will be used to separate the blade from the rolling formed blade at root and tip sections after machining arcs, which suture the pressure and suction surfaces at the leading and trailing edges. Hence, the machining allowances are added at the root and the tip of blade, see **Figure 4**. The addition of the machining allowances can also reduce the impact load on the cavity at the beginning and the end of the rolling process. The tip section curve of blade is stretched outwards by a length of l_t to set up the tip machining allowance, and root section curve of blade is stretched outwards by a length of l_r to set up the root machining allowance, see **Figure 4**. An integrated process model for rolling blade also needs a location block for holding the blade in the entire

of original section curves at different stacking height sequentially. The center point of the biggest inscribed circle is a unique point for every section curve, and it locates section curve on cross section. A discretizing algorithm is proposed by limiting the maximum chord height to segment a curve to a set of ranked point. The cross sections are created at the discretized points along the orientational curve. The section curves of the process model are generated as the intersection curves of the blade profile and the cross sections.

3.2.1. Determining the Location of the Section Curves

A curve can be discretized into points using different methods, such as the length restriction of segmented units, the restriction of chord height, and the restriction of angle, etc. In order to use less number of points to represent a smooth curve with required accuracy, a discretizing method is proposed by limiting the chord height of the discretized units. The threshold value is related to the requirement of the blade tolerance. The chord height is the largest distance from the bow to the line between start and end point in each unit. If the chord height is smaller than the threshold value, the curve can be simplified to the line. Otherwise, a new point is inserted on the curve at the farthest point from the line. Then, the new units are checked by limiting the chord height again until every discretized unit meets the limitation of the threshold value. In the case illustrated in the inset of **Figure 5**, if $d_k \leq \delta$, then the straight green line is used to replace the original red curve; if $d_k > \delta$, the straight blue line can't replace the original red curve, then a new point is added and the two straight green lines are used to replace the original red curve. The curve is discretized into the ranked points based on the required threshold value. The diagram of discretizing process is showed in **Figure 5**. k is the serial number of discretized curves and returned points, P_k is the serial number of discretized points, L_k is the serial number of broken lines, and d_k is the height of the chord. In this way, the red curve is discretized into the green polyline based on the discretizing algorithm, and the discretized points are used to represent the orientational curve. These discretized points of the orientational curve are the locations to create the section curves of the process model.

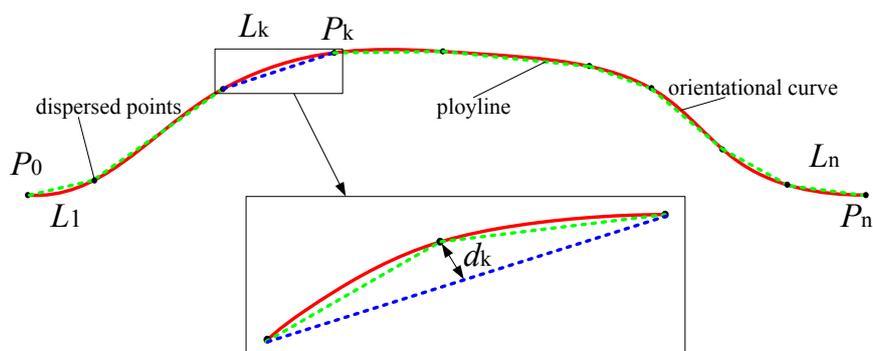


Figure 5. Discretizing the blade orientational curve under the constraint of the chord height.

3.2.2. Creating Section Curves of the Process Model

The orientational curve of blade describes rotation and translation of the pressure and suction surface along the stacking direction. The orientational curve is discretized into a ranked point set by limiting chord height as discussed in Section 3.2.1, see **Figure 6(a)**. The distribution of cross sections is created by inserting planes vertical to Z-axis at the locations of the ranked points, see **Figure 6(b)**. New section curves are the intersection curves of the auxiliary planes and the profiles of the process model, see **Figure 6(c)**.

3.3. Creating Section Curves of Roller Cavity through Coordinate Mapping

The final step to design the roller cavity is to revolve the updated section curves of the process model to the section curves of the cavity surfaces. According to the coordinate systems presented in Section 3.1.2, the corresponding coordinates of the points of the cavity section curve are mapped from the new section curves. The springback compensation was implemented to achieve net-shape of the cross sections and forward slip compensation was implemented to calculate the mapping angle of the sections [20]. In order to achieve the coordinate transformation, the updated section curves of process model are discretized into point sets. The number and distribution of the discretized points on the section curve also have an important effect on the precision of the section curve of cavity surface.

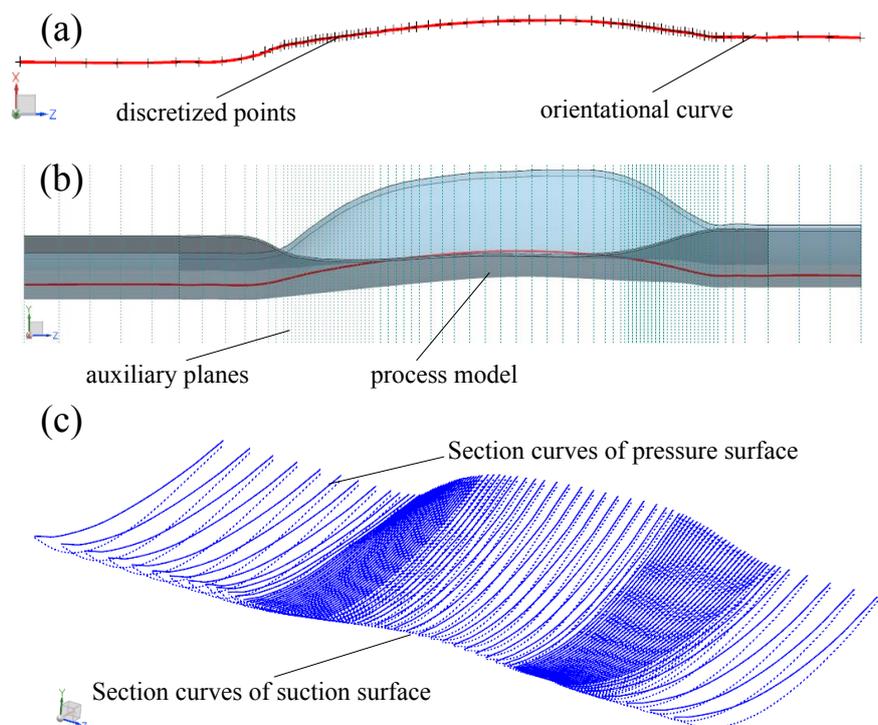


Figure 6. Creation of cross section curves of the process model based on the discretized points on the orientational curve. (a) The orientational curve and discretized points. (b) The auxiliary planes and the process model. (c) A new set of section curves of the process model.

The updated section curves are discretized into ranked points used the discretizing algorithm presented in Section 3.2.1. The coordinates of the ranked point set are rotated around the roller axis and generated the corresponding ranked point set which represents the section curve of cavity. The distance between the top roller's axis and the bottom roller's axis is D . The coordinate mapping algorithm for the top and the bottom roller cavity surfaces are presented in Equation (1) and Equation (2), respectively,

$$\begin{cases} x' = x \\ y' = \frac{D}{2} - \left(\frac{D}{2} - y\right) \cos(\theta_k) \\ z' = \left(\frac{D}{2} - y\right) \sin(\theta_k) \end{cases} \quad (1)$$

$$\begin{cases} x' = x \\ y' = -\frac{D}{2} - \left(y - \frac{D}{2}\right) \cos(-\theta_k) \\ z' = \left(y - \frac{D}{2}\right) \sin(-\theta_k) \end{cases} \quad (2)$$

where $(x \ y \ z)$ is the discretized point's coordinates of the updated section curve, $(x' \ y' \ z')$ is the point coordinates of the section curve of the cavity surfaces, θ_k is the rotational angle.

A new point set which represents the section curve of cavity surface is created based on the mapping algorithm. The cavity section curves are reconstructed through the new point sets. The mapping process of the section curves of the top and bottom cavity surface is shown in **Figure 7**. The blue curves S_k are section

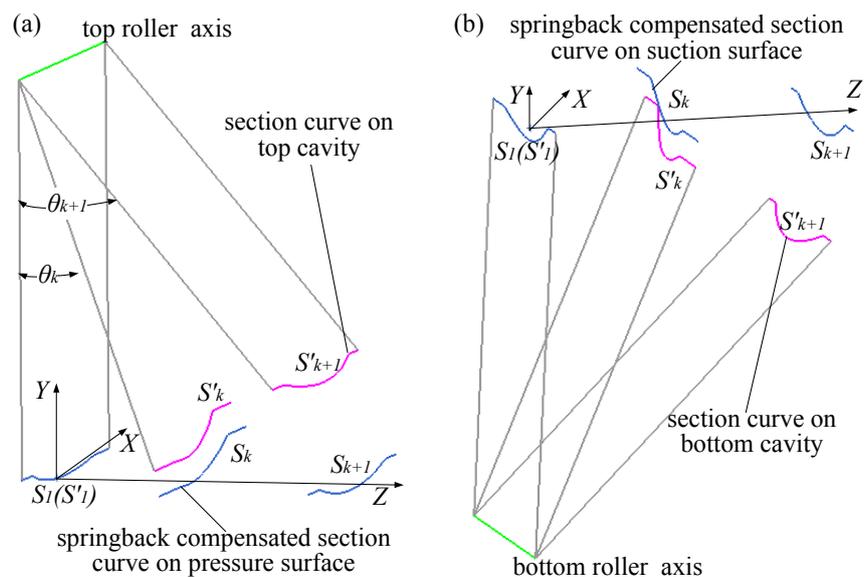


Figure 7. Illustration of mapping transformation for section curves: (a) Mapping section curves from the pressure surface to top mold cavity; (b) Mapping section curves from the suction surface to bottom mold cavity.

curves of process model which are created in Section 3.3.2. The red curves S'_k are ranked section curves of cavity surfaces. The section curves of the processes model and cavity surface are the same at the exit section ($\theta_0 = 0$), see **Figure 7**.

The designed cavity surfaces are reconstructed based on the mapped section curves, as showed in **Figure 8**. The rollers for rolling compressor blade a re-created based on the design cavity surfaces.

4. A Case Study to Validate the New Design Method

In order to validate the new design method, the FEM simulation were carried out to form a rolled blade, and four groups of corresponding section curves at the different stacking height are investigated.

4.1. A Case Study to Design Cavity Surfaces for a High Pressure Compressor Blade

A high-pressure compressor statorblade (**Figure 1(b)**) of an aero-engine is formed by rolling. The total stacking height of the blade is 38 mm, and the machining tolerance is ± 0.02 mm. The new design method was used to create the roller cavity surface for the blade. Firstly, a process model of the blade was developed based on the CAD model of the blade. The overflow were added on the original section curves of the blade, see Section 3.1.1. The auxiliary units were added to achieve the process model, see Section 3.1.2. In order to add the machining allowances at the root and the tip of blade, the tip machining allowance l_t was 6 mm and the root machining allowance l_r was 10 mm, see **Figure 4**. Secondly, a new section curves distribution was created on the process model, see Section 3.2. An orientational curve was sketched along the maximum inscribed circle's center point of original section curves at different stacking height sequentially. The orientational curve was discretized into a ranked points which determining the location of the section curves. The new cross section is created by inserting planes vertical to Z -axis at the locations of the ranked points and the new section curves are the intersection curves of the auxiliary planes and the profiles of the process model, see **Figure 6**. Thirdly, the section curves of cavity

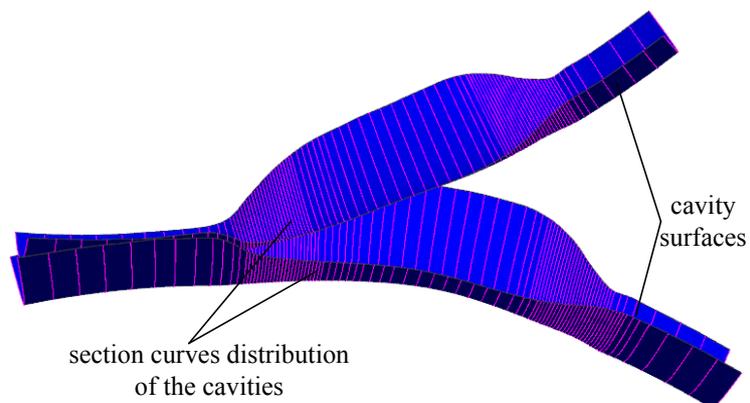


Figure 8. Reconstruction of the cavity surfaces based on the section curves of the cavity.

surface were transformed from the section curves based on the mapping algorithm, see Section 3.3. The distance between the top roller's axis and the bottom roller's axis is 136 mm which discussed in Equation (1) and Equation (2). The cavity surfaces were reconstructed based on the mapped section curves of the cavity, see **Figure 8**. Finally, the contour surfaces of the roller were created based on the designed cavity surface, see **Figure 9(a)**. In order to create a pair of solid roller, a pair of fan-shaped bodies was separated by the contour surfaces, see **Figure 9(b)**. The solid roller is showed in **Figure 1(c)**.

4.2. FEM Code for Blade Rolling Process

A simulation model was created for the blade rolling process. The rolling process was replicated in the numerical simulation using a non-linear Explicit FE code (ABAQUS/Explicit 6.14-1). The reduced integration, hourglass control (C3D8I) is used to mesh the blank, and the mesh size is 0.1 mm. The blank is a flat plate and the thickness reduction is 30%. The properties of the blank are showed in **Table 1**. The bilinear, rigid, quadrilateral element control (R3D4) is used to mesh the dies, and the size of mesh is 0.1 mm. The top and bottom rollers are rotated with the angle velocity of 0.5 rad/s. The interactions between the blank and roller surface are defined using the default "master-slave" algorithm. To simulate the oil lubrication, the interface friction coefficient is set as 0.25. The model of rolling simulation is showed in **Figure 10(a)**, and the rolling formed blade is showed in **Figure 10(b)**.

4.3. Results and Discussion

The precision of profile of the produced blade is evaluated by its section curves [21]. The root and tip section curves (0 mm and 38 mm) are boundaries of the blade for assembly. The section curves of the blade are severely rotated and translated at the stacking height of 8 mm and 32 mm. Hence, the cross section curves of the rolling formed blade and the simulation result at the stacking height of 0 mm, 8 mm, 32 mm, 38 mm are measured and sketched. Those section curves are compared with the original section curves of CAD model. The section outlines are showed in **Figure 11**.

Table 1. Material parameters of GH4169 at room temperature.

		GH4169	
Density (Kg/m ³)		8250	
Young's modulus (MPa)		220,000	
Poisson's Ratio		0.3	
	Yield Stress (MPa)	Plastic Strain	
	989	0	
Plastic parameters	1119	0.0042	
	1190	0.0092	
	1236.4	0.0192	
	1282.7	0.0272	

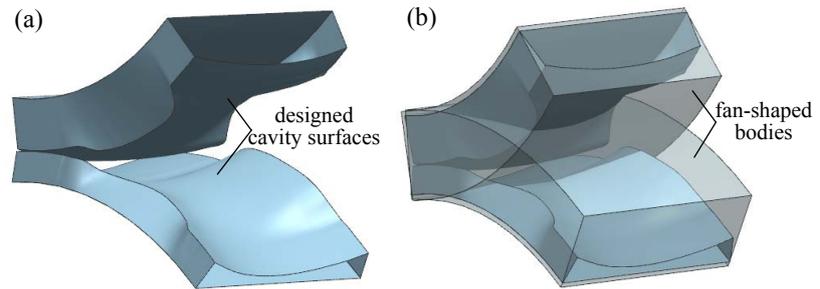


Figure 9. Illustration of a fully designed rollers based on the designed cavity surfaces: (a) The contour surfaces of the rollers; (b) Separation of the solid rollers from fan-shaped bodies by the contour surfaces.

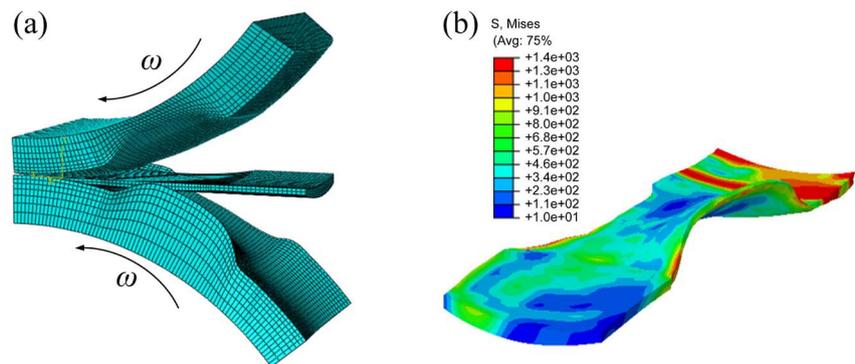


Figure 10. The validation of the designed cavity surface by the FEM simulation. (a) The FEM model for rolling simulation, (b) The rolling formed blade from the FEM simulation.

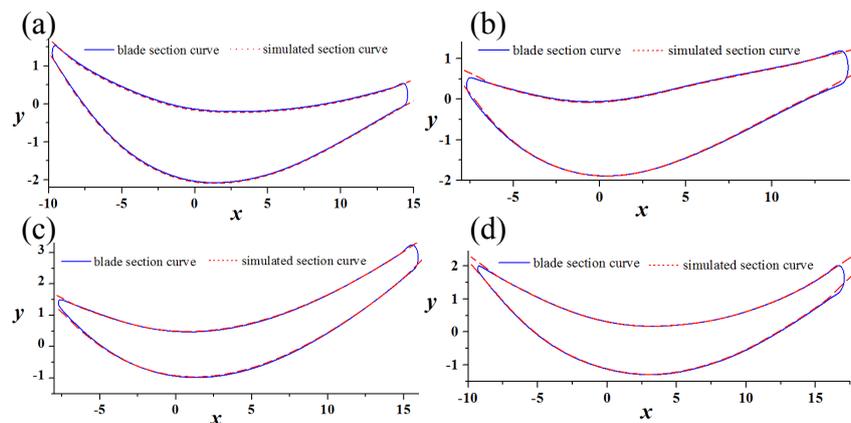


Figure 11. Comparison of section curves from the original CAD model of blade, FEM simulation at different stack height: (a) $Z = 0$ mm; (b) $Z = 8$ mm; (c) $Z = 32$ mm; (d) $Z = 38$ mm.

The section curves from FEM simulation are compared with the original section curves on CAD model at the same stacking height. The results demonstrate that the section curves from simulation have a good consistency with the CAD model. The largest error of every section curves is smaller than the required tolerance (0.02 mm) of the blade. The results reveal that the designed cavities meet

the precision of net shape at the pressure and suction surfaces of the blade. The design method is suitable for designing the roller cavity surface for the compressor blade.

5. Conclusions

A new design method of cavity surfaces for rolling compressor blades is proposed for complex part based on geometrical inheritance and evolution, and the geometrical inheritance and evolution accuracy of the part are emphasized. The design procedure and algorithm are discussed in detail. The major works are summarized below.

- The new cavity surface design method for net shape rolling blade is proposed based on the motion relation and geometrical inheritance. A process model between the blade and the cavity surface is introduced in design process to represent the pressure and suction surface of the blade before transformation.
- An algorithm is used to discretize a curve to a set of ranked points with the restriction of the maximum chord height. The discretizing algorithm connects the discretizing precision with the design tolerance of a blade. It is an effective method to improve design accuracy under a tolerance requirement.
- A mapping algorithm is presented for designing a compressor blade rolling cavity surfaces. The coordinate transformation formula from the updated section curves to the section curves of cavity surfaces is derived based on the conjugate movement between the rollers and blank.
- A case study is implemented based on the new design method to design a pair of rollers for rolling a compressor blade. The numerical simulation was used to evaluate the precision of the designed cavities. The results indicated that the formed blade satisfied with the tolerance requirement of blade. The proposed method is suitable for designing roller cavity surfaces.

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Author Contributions

Qichao Jin designed, conducted the research and wrote the paper. Wenhui Wang and Ruisong Jiang improved the design method and developed the program. Zongyan Cai and Datao Li discussed the research and editing the paper.

Conflicts of Interest

The authors declare no conflict of interest.

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