

# Silica and Iron Recovery from a Residue of Iron Ore Flotation

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## Abstract

A study of silica and iron recovery from the iron ore concentration tailing is presented. The residue is composed of 40.1% Fe, 33.4% SiO<sub>2</sub>, 8.31% Al<sub>2</sub>O<sub>3</sub>, 0.08% P, and 0.34% MnO. The developed process of silica and iron recovery consisted of size classification, magnetic separation, and removal of impurities by leaching. A concentration of SiO<sub>2</sub> from 33.4% to 67.0%, with 60.0% of mass reduction, was achieved by size classification. After magnetic separation, the SiO<sub>2</sub> grade increased from 67.0% to 95.0%, in non-magnegtic fraction and iron increased from 40.1% to 60.2% in magnetic fraction. The iron content in magnetic fraction achieved the commercial grade. In order to increase the content of silica, the impurities removal from the non-magnetic fraction was studied. The leaching agents investigated were HCl, H<sub>2</sub>SO<sub>4</sub>, HNO<sub>3</sub>, HF, C<sub>6</sub>H<sub>8</sub>O<sub>7</sub>, (COOH)<sub>2</sub>·2H<sub>2</sub>O and NaOH. A concentration of 98.0% SiO<sub>2</sub> was attained with the acid digestion.

# **Keywords**

Industrial Residue Processing, Iron Recovery, Silica Recovery

# **1. Introduction**

The largest iron reserves on Earth are composed of Banded Iron Formations (BIFs), which are altered sedimentary deposits with laminated rocks formed by alternating layers of silica and hematite-magnetite, as well as carbonates and iron silicates. One of the most important iron provinces in Brazil is the Quadrilátero Ferrífero (QF), located in the São Francisco Craton, southeastern Brazil [1].

Ferric oxides are separated from silicates by flotation or magnetic separation. The residue generated by magnetic separation consists of fine iron oxide and silicates. Two types of residues are generated by flotation. One of them is similar to sand and consists of quartz particles (greater than 85 wt%) and iron oxides (less than 15 wt%). The other one is similar to clay, consisting of quartz ultrafine particles, iron oxides and hydroxides (mainly goethite) and aluminum silicates. These residues have been used to fill mining pits or stored in dams that require permanent and costly monitoring.

A trend of reducing the iron grade and of course increasing levels of contaminants is observed in itabirites tailings in the Quadrilátero Ferrífero (Minas Gerais state, Brazil). Currently, it is known that industrially, for each ton of iron ore concentrate produced, one tailings ton is generated (about 411.8 million tonnes year) [2]. Therefore, more and more tailings will be generated, presenting challenges to its disposal in dams or reuse. Therefore, it is imperative to seek the recovery of useful minerals iron and also the contaminants contained in these tailings, aiming at the minimization of generated volumes and reduced environmental impact.

The iron ore concentration tailing in the form that it is generated may have some applications, such as a substitute for sand in cementitious products. Depending on its purity, the silica may have other applications, such as in the glass industry, ceramics, optics, electronics, etc. [3].

There are several studies related to removal of iron from silicates, aiming at purification of silica by chemical processes. Various inorganic and organic acids have been used, such as sulfuric acid (H<sub>2</sub>SO<sub>4</sub>), hydrochloric acid (HCl), oxalic acid ((COOH)·2H<sub>2</sub>O) and citric acid ( $C_6H_8O_7$ ) [4] [5]. According to Abdelkrim [6], purification of silica from flotation residue may be performed by acid leaching with percolation using a mixture of hydrofluoric acid (HF) and hydrochloric acid (HCl) followed by an alkaline washing with sodium hydroxide (NaOH). Santos et al. [7] evaluated the performance of leaching for purification of metallurgical grade silicon using sulfuric acid (H<sub>2</sub>SO<sub>4</sub>), hydrochloric acid (HCl), and hydrofluoric (HF) acid and nitric acid (HNO<sub>3</sub>). Iron can also be removed by bio-hydrometallurgical processes. Iron can be leached by acid producing microorganisms, such as bacteria and fungi. Groudev [8] developed a process for iron removal at high temperatures using filtrates of cultured fungi, especially Aspergillus niger.

The sample used in this work was a reject from the Peak of Mine, provide by Vale S.A.

First the sample was chemical and physically characterized. Based on the granulochemical analysis, the fraction between the sieves of 298 µm and 37 µm was separated, which was subjected to wet and dry magnetic concentration to remove the magnetic fraction, iron-rich part. Leaching experiments and acid digestion were performed to reduce the levels of impurities of the non-magnetic fraction, especially aluminum and iron, in which the type and concentration of the leaching agent, the reaction time and the temperature were varied.

## 2. Materials and Methods

## 2.1. Sample and Reagents

The iron ore concentration tailing was provided by the Vale S.A.



The experiments were performed using sulphuric acid ( $H_2SO_4$ ), hydrochloric acid (HCl), nitric acid (HNO<sub>3</sub>), citric acid ( $C_6H_8O_7$ ), oxalic acid ((COOH)<sub>2</sub>·2H<sub>2</sub>O), hydrofluoric acid (HF) and sodium hydroxide (NaOH); all of them of analytical grade.

#### 2.2. Analytical Procedure

The chemical characterization of the samples and the analytical monitoring of the experiments was done by wavelength dispersive X-ray fluorescence spectrometer—WDX (Rigaku—model ZSX Primus II), energy dispersive X-ray fluorescence spectrometer (SHIMADZU, model EDX-720), flame absorption atomic spectrometry Varian/Agilent (model AA240FS) and the determination of the minerals phases was performed by X-ray diffraction with a Rigaku spectrometer (model D/Max Ultima).

#### 2.3. Methodology

Once dry, the sample was de-agglonerated, homogenized, quarted and packaged. After this preparation, the physical and chemical characterization, particle size analysis, and density measurement were performed.

Based on the granulochemical analysis, the fraction between the sieves of 298  $\mu$ m and 37  $\mu$ m was separated, which was subjected to wet and dry magnetic concentrations to remove the magnetic fração, iron-rich part. The magnetic separations experiments were performed in a high intensity, magnetic roller separator (RER4), a medium intensity, drum magnetic separator (WDRE), and a high intensity electromagnetic separator with magnetic field of about 16,000 gauss. Part of these experiments were carried out by Inbras-Eriez.

The leaching experiments, made in batch, were carried out in a beaker with mechanical stirring in water bath and temperature control. In this step the following process variables were investigated: type and dosage of the leaching agent, agitation time, relation between leaching agent and ore, percent of solids, and temperature. The acid digestion experiments were performed in a 150 mL beaker on a hot plate at 200°C for 4 h and 6 h. The digestion product was leached with water under mechanical stirring at room temperature (25°C) for 1 h.

## 3. Results and Discussion

#### 3.1. Sample Characterization

The chemical analysis of the sample showed Fe (40.1%), SiO<sub>2</sub> (33.4%), Al<sub>2</sub>O<sub>3</sub> (8.31%), P (0.18%), MnO (0.34%) and major mineral quartz (SiO<sub>2</sub>), hematite (Fe<sub>2</sub>O<sub>3</sub>), dickite (Al<sub>2</sub>Si<sub>2</sub>O<sub>5</sub>(OH)<sub>4</sub>), and goethite (FeO·OH). The density was 3.696 g/cm<sup>3</sup>.

#### 3.2. Mass and Metallurgical Distribution

The mass and metallurgical distributions of the main constituents are presented in Table 1. As noted, the fraction +  $37 \mu m$  recovered 38.6% of the mass and

Sing (um)	Distribution (%)						
Size (µm)	Mass	SiO <sub>2</sub>	Fe	$Al_2O_3$			
210	1.10	2.60	1.00	2.20			
149	6.90	16.2	2.00	3.60			
105	13.4	31.3	4.10	5.10			
74	20.7	44.8	8.60	6.90			
53	28.9	59.9	13.7	9.20			
44	34.6	69.5	17.4	11.6			
37	38.6	75.2	20.7	14.0			
-37	100.0	100.0	100.0	100.0			

Table 1. Mass and metallurgical distribution.

Table 2. Main constituents of the samples obtained in the granulometric classification and magnetic separation.

	Grade (%)						
Sample	Fe	SiO <sub>2</sub>	$Al_2O_3$	Р	MnO		
Original sample	40.1	33.4	8.31	<0.08	0.34		
(–298 + 37) μm fraction	20.6	67.0	2.70	< 0.08	0.08		
Wet test, non-magnetic fraction	0.90	94.5	3.00	<0.08	0.01		
Dry test, non-magnetic fraction	0.74	95.4	2.56	< 0.08	0.01		
Wet test, magnetic fraction	60.2	10.9	1.84	<0.08	0.17		
Dry test, magnetic fraction	54.3	17.2	4.15	< 0.08	0.16		

75.2% of SiO<sub>2</sub>. In the granulometric classification between  $-298 + 37 \mu m$ , the silica content increased from 33.4% to 67.0%.

## 3.3. Magnetic Separation

In the dry test, the silica content increased from 67.0% to 95.4% in 3 steps and in the wet test, the silica content increased from 67.0% to 94.5% in 2 steps. In the dry test, 44.8% of mass and 69.7% of silica were recovered, while in the wet test, 55.4% of mass and 84.1% of silica were recovered. The concentration of the original constituents of the sample and the fraction -298 + 37  $\mu m$  of magnetic and non-magnetic fractions are shown in Table 2.

## 3.4. Leaching

Initially, tests were performed to choose the best leaching agent for the dissolution of Fe and Al. As mentioned above, the leaching agents selected were the acids HCl, H<sub>2</sub>SO<sub>4</sub>, HNO<sub>3</sub>, HF, C<sub>6</sub>H<sub>8</sub>O<sub>7</sub>, and (COOH)<sub>2</sub>·2H<sub>2</sub>O. The experiments were performed at 70°C, 3 hours of reaction and 10% of solids. The results are shown in Table 3.

As shown in Table 3, under the test conditions, there was no significant difference between the leaching agents investigated in the purification of silica.

Leaching agent		Dissolu	tion (%)	(0)
Acid	Concentration (mol/L)	Fe	$Al_2O_3$	- SIO <sub>2</sub> grade (%)
HCl	2.00	39.8	39.0	96.5
HCl	5.00	54.7	25.2	96.2
$H_2SO_4$	5.00	27.8	15.8	95.2
$H_2SO_4$	2.00	26.4	8.7	94.7
$C_6H_8O_7$	1.00	40.7	23.8	96.0
(COOH) <sub>2</sub> ·2H <sub>2</sub> O	0.70	33.9	18.3	95.6

**Table 3.** Effect of the leaching agent in the purification of silica from the original iron ore concentration tailing.

Original sample: 0.90% Fe; 3.00% Al<sub>2</sub>O<sub>3</sub> and 94.5% SiO<sub>2</sub>.

Solid content (%)	NaOH (mol/L)	Temp. (°C)	Time (h) -	Dissolution (%)		SiO <sub>2</sub> grade
				Fe	$Al_2O_3$	(%)
10	5.00	70	3	17.2	22.4	95.6
50	12.50	70	3	41.0	41.7	95.7
70	12.50	70	3	27.6	40.5	95.3
50	12.50	70	8	38.9	46.4	96.9
50	12.50	25	24	34.0	27.5	95.5

Table 4. Results and experimental conditions of alkaline leaching tests.

Original sample: 0.90% Fe; 3.00% Al<sub>2</sub>O<sub>3</sub> and 94.5% SiO<sub>2</sub>.

However, H<sub>2</sub>SO<sub>4</sub> was the least efficient, showing the lowest dissolution of Fe.

To remove the Al in the sample, alkaline leaching tests with NaOH were performed. Tests were performed with NaOH 5 mol/L and 12.5 mol/L (~50% w/w), where the percentage of solids, reaction time, and temperature were varied. The experimental conditions and results of these tests are presented in **Table 4**.

According to the data in **Table 4**, the best results were obtained when using NaOH solution of 12.5% at 70°C, with Al dissolution of 46%. The results also showed that in this case a high percentage of solids (50% w/w) can be used.

In a following stage, alkaline leaching residues were subjected to acid leaching to increase the purity of the silica. The leaching agent used was HCl at the concentration of 5 mol/L. **Table 5** shows the results and the conditions of these experiments.

The results in **Table 5** are inconclusive. However, they show the difficulty of removal of iron and aluminum from the sample after magnetic separation.

Still in search of better conditions for reducing the level of impurities in the residue to obtain high-purity silica, another leaching test was performed with a mixture of HF 50% and HCl 25% in relation 1:1. The acid concentrations and the ratio of their mixture were chosen based on literature (Abdelkrim, 2009). The percentage of solids was 50% with a reaction time of 3 h at room temperature. The residue was washed with distilled water and dried at 110°C. After that,

Solid content (%)	T	T:	Dissolution	S:O (0/)	
	Temp. (C)	Time (n)	Fe	$Al_2O_3$	$-300_{2}(\%)$
10	70	3	48.9	67.3	98.0
20	70	5	24.1	66.9	97.1
50	70	5	21.4	14.9	96.0
20	70	5	39.7	20.6	97.2
50	70	5	27.7	10.2	96.1
50	70	7	19.3	29.7	97.4
50	25	24	30.2	71.9	96.4

Table 5. Results and experimental conditions of acid leaching.

Table 6. Results of leaching tests with the HF/HCl mixture and with NaOH.

Looching agont	eaching agent Concentration (%) -	Concentration	Dissolution (%)		S:O (0/)	
Leaching agent		Fe	$Al_2O_3$	Fe	$Al_2O_3$	$310_2(\%)$
HF/HCl	50/25	0.38	0.70	37.2	74.4	97.4
NaOH	10	0.28	0.66	18.7	6.91	97.8

Original sample: 0.74% Fe; 2.56% Al<sub>2</sub>O<sub>3</sub> and 95.4% SiO<sub>2</sub>.

**Tabel 7.** Fe,  $Al_2O_3$  e SiO<sub>2</sub> grade in residue from acid and alkaline digestion of the nonmagnetic fraction.

RAM (kg/t) —	Dissolu	Dissolution (%)		Impurity grade (%)			
	Fe	$Al_2O_3$	$310_2(70)$	Fe	$Al_2O_3$	Р	SO <sub>3</sub>
500	72.4	73.9	97.7	0.30	0.70	0.16	0.91
1000	73.6	75.9	98.0	0.29	0.66	0.09	0.93
1500	72.2	78.4	98.2	0.31	0.60	0.04	0.78

Original sample: 0.74% Fe; 2.56% Al<sub>2</sub>O<sub>3</sub> and 95.4% SiO<sub>2</sub>. RAM = acid/ore relation.

a very alkaline leaching with NaOH 12.50 mol/L was performed, aiming at the dissolution of the remaining Al. The results of these tests are presented in Table 6.

As shown in **Table 6**, for the conditions under which the tests were performed, there was no gain in purification of silica compared with previous experiments. Another expected drawback with the mixture HF/HCl is a high dissolution of silica (7.0% w/v). In leaching experiments, the silica content raises from 94.0% to 98.0%. Thus, the acid digestion with concentrated  $H_2SO_4$  at high temperature was investigated, as shown in the next section.

## 3.5. Digestion

Acid digestion tests were performed at 200°C, using concentrated  $H_2SO_4$  with three different sample/acid relations, 500, 1000 and 1500 kg/t, and 4 hours of reaction. The conditions and results of these experiments are presented in Table 7. After completion of the reaction time, distilled  $H_2O$  was added at a ratio of

10% of solids and stirred for one hour before proceeding to filtering the pulp.

According to the results in **Table 7**, in acid digestion tests, higher Fe and Al dissolution was obtained. The silica content was maintained at 98.0%.

#### 4. Conclusions

The steps that contributed the most to the purification of the silica from the flotation residue were granulometric classification and magnetic separation. The granulochemical analysis of the flotation residue showed that 79.0% of iron and 86.0% of aluminum are contained in the fraction below 37  $\mu$ m. In desliming of the sample in 37  $\mu$ m, recovery was 75.2% silica and 61.4% mass reduction. In this step, the SiO<sub>2</sub> content increased from 33.4% to 67.0%. In magnetic concentration, the wet experiment was more efficient than the dry one. The cleaning concentration was performed in 3 stages, and the wet one, in 2 stages. However, the final composition of the non-magnetic and magnetic fractions was similar for the two techniques (~95.0% SiO<sub>2</sub>), 55.0% of the mass and 84.1% of SiO<sub>2</sub> were recovered in the wet concentration, while in the dry concentration, the mass recovered was 44.8%, including 69.7% of SiO<sub>2</sub>.

The purification experiments of silica by chemical processes indicated the difficulty of removing the contaminants, Fe and Al, present in the sample after the magnetic classification. Quite drastic conditions were used even in acid and alkaline leaching as well as in acid digestion, the maximum silica obtained was 98.0%.

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