

# Enhancement of Dimensional Stability of Rigid PVC Foams Using E-Glass Fibers

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## Abstract

Short cut E-glass fibers of two different lengths were used to determine the effect of glass fiber length on the dimensional stability of rigid Polyvinyl Chloride (PVC) foam in this study. Glass fibers measuring, 1/16" and 1/32" at different concentrations (0 wt% - 20 wt%) were used to reinforce rigid PVC foams; the PVC foam-glass fiber (PVC-GF) composites were extruded using a single screw profile extruder. The extruded PVC-GF composites were characterized for their dimensional stability, structural, thermal, and mechanical properties. Experimental results show that the dimensional stability, heat resistance, and storage modulus were enhanced without compromising the tensile and flexural strengths of the composites. Thermal shrinkage decreased by almost 55% in composites reinforced with 1/32" GF and by 60% in composites reinforced with 1/16" GFs, with visible improvements to the shape distortion. Overall, foam composites which were prepared with longer (1/16") glass fibers exhibited better mechanical and thermal properties than those prepared with shorter (1/32") glass fibers. Microstructural observations suggest that this is due to better interlocking between the long fibers and the foam cells, which result in better load distribution in the matrix.

## Keywords

Polyvinyl Chloride, PVC Foam, PVC Composites, Polymer Composites, Glass Fiber Composites, Reinforced Polymers

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## 1. Introduction

Polymer foams are a unique class of materials that are widely used due to their light weight, low cost, and good formability along with load bearing and insulation capabilities. The cellular structure of the foam determines its

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mechanical and physical properties, and hence its performance and applications [1] [2]. Rigid Polyvinyl Chloride (PVC) foam and their composites have been used as an excellent replacement for wood in the building materials industry in the form of profiles, sheets, and pipes due to their low cost, low density, fire retardancy, and high insulation and damping properties. However, rigid PVC foams lack adequate dimensional stability when they are exposed to high and/or low temperatures. Certain applications of PVC foam products require excellent dimensional stability; such as in exterior moldings, siding, decking and railing applications. Solid fillers, such as calcium carbonate, talc, glass fibers (GF), carbon fibers, and wood fibers have been reported as effective PVC reinforcement additives in many publications [3]-[5]. The selection process of an effective reinforcement filler depends on its compatibility with the polymer matrix and the governing relationship between structure, property, and performance of the composite.

The use of GF as a reinforcement filler for improved dimensional stability in non-foam polymer composites has been studied and reported extensively. Raj *et al.* [6] studied the effect of heat exposure on the mechanical and thermal properties of glass fiber, mica and wood fiber reinforced low density polyethylene (LDPE); they reported that tensile strength and dimensional stability of the GF reinforced LDPE increased with increasing GF content. Canova *et al.* [7] studied GF (3.2 mm) and mica filled Polypropylene (PP) composites; they reported high dimensional stability and shrinkage reduction in GF-PP composites with higher filler contents. Jang *et al.* [8] prepared poly (butylene terephthalate) (PBT) filled GF composites using extrusion process. They reported enhancement in mechanical properties only when using sufficient coupling agents in order to improve the interfacial interaction between GF and the polymer matrix. They also claimed that the loading amount and length of GF, as well as the extrusion conditions determine the final mechanical properties of PBT-GF composites. Hassan *et al.* [9] prepared PP reinforced GF using maleic anhydride polypropylene (MAPP) as a coupling agent in extrusion and injection molding. They reported modest increase in the melting temperature of the composites with increasing GF and MAPP contents. Dynamic mechanical analysis (DMA) showed an improvement in the viscoelastic properties of the composite with low GF loadings in the presence of the coupling agent.

Although short GF are known to yield lower enhancement in their composites when compared to their longer counterparts, they are still widely used in polymer composites due to their processing advantages [10]. Ozkoc *et al.* [11] studied the effect of content and extrusion conditions of surface treated short GF on the mechanical properties of acrylonitrile-butadiene-styrene (ABS). In their work, polyamide-6 (PA6) was used at different levels to improve the interaction between GF and the matrix. They reported that the tensile strength, tensile modulus, flexural modulus, and impact strength of the composites are lower when using shorter glass fibers. However, mechanical properties improved slightly when using higher amounts of short GF and PA6. Thomason *et al.* [12] studied the effect of the length, diameter, and content of GF on the impact properties of polyamide 6, 6 reinforced with GF using notched and un-notched impact samples. They reported that the impact properties of the notched samples were more sensitive to the fiber length and content; while the fiber diameter and content were the main parameters affecting the impact strength of the un-notched samples. Jiang [13] studied the influence of short (0.8 mm) and long (6.4 mm) GF on the impact strength of PVC/wood flour/ GF at a constant loading level of 5%. It was reported that the long GF improved the impact strength while maintaining flexural properties, whereas the short GF did not show any significant improvements. In addition, it has been reported elsewhere that glass fibers improve dimensional stability and mechanical strength in PVC composites [14] [15].

Deanin *et al.* [16] investigated the effect of adding GF on the dimensional stability of PBT foam composites. They reported enhancement in the dimensional stability when using coupling agents and surface treatments to enhance the interaction between the GF and polymer matrix. Similarly, Laurent *et al.* [17] studied the effect of surface treatment on the mechanical properties of foamed and un-foamed PVC reinforced with wood fibers. They observed a reduction in tensile modulus and tensile strength of the composites at higher GF loading, which was attributed to higher void fraction in the composites structure and weak interaction between the matrix and GF. Mengeloglu *et al.* [18] studied the mechanical properties of extruded foam PVC/wood-flour composites and reported similar results to Laurent *et al.* [17]. Tungjitpornkull *et al.* [19] prepared E-chopped GF filled wood/PVC composites at different GF loadings, 10, 20 and 30 phr, with various fiber lengths 3, 6 and 12 mm. They concluded that the most critical parameter in determining the tensile and flexural properties of the composites is the GF loading in the composite.

Based on our literature review, there is no published work on the effect of GF on the dimensional stability of PVC foams. In this study, the effect of GF content and length on the dimensional stability, as well as the mechanical, microstructural, and thermal properties of PVC foam composites, are investigated.

## 2. Experimental

### 2.1. Materials

Rigid PVC resin was purchased from Shintech, USA; it had an inherent viscosity of 0.74 (ASTM D1243); bulk density of 36.3 lb/ft<sup>3</sup> (ASTM D 1895), and maximum volatiles of 0.12% (ASTM D3030). A commercially available thermal stabilizer, Thermolite T-137, and processing aids, Plastistrength P530 and P770, were provided by Arkema, USA. Other ingredients used in preparing the samples are Lubricants Loxiol 2986 and 2987 produced by Oleochemicals; paraffin wax Petrac 215 produced by Ferro Corp.; Calcium Stearate COAD 10 produced by Norac Corp.; chemical blowing agents Azodicarbonamide (ADC) produced by Season Corp.; and Sodium Hydrogen Carbonate (FICEL SBH) produced by Hughes Polymer Additives Corporation. The specific content of each ingredient is considered proprietary; however the amount of each ingredient follows a common formulation used in making rigid PVC foams. Two types of milled and saline treated E-glass fibers, with lengths of 1/16" and 1/32" and diameter of 16 microns, were purchased from Fiber Glast Developments Corporation.

### 2.2. Sample Preparation

PVC foam compounds were prepared using a high shear mixer (Gunther Pepenmeier, Machinen-u. Detmoid, Type: TSHK). Initially, the PVC resin was added to the mixer at room temperature. Then, the stabilizer was added at 52°C, glass fibers and processing aids were added at 58°C. Finally, the lubricants and the blowing agents were added at 66°C.

When the temperature reached 100°C, the compound was collected from the mixer and allowed to cool down to room temperature before extrusion. The compounds were extruded using a 1.25 inch, 20:1 (L/D) single screw extruder (Thermoplast Extrusion Machine<sup>®</sup> from New England Wire Machinery Co.) at a screw speed of 60 rpm. The heating zones temperatures were in the range of 158°C to 175°C. A rectangular profile die was used to extrude the samples. The extruded stream was air cooled prior to feeding through an aluminum sizer (1" × 0.28") placed in a vacuum chilled water tank. Finally, the extruded stream is cut into 12" pieces using an automated cutter. The composites formulations are listed in [Table 1](#).

### 2.3. Thermal Properties

Thermal properties of the foam composites were analyzed using: 1) TA Instrument SDT 2960 thermo-gravimetric analysis equipment (TGA) in the temperature range of 25°C to 800°C at a heating rate of 10°C/min under argon atmosphere; and 2) Differential Scanning Calorimetry (DSC) measurements using TA Q2000 analyzer (TA Instruments, US). Foam composite samples weighing 5 to 10 mg were heated in standard aluminum pans in the temperature range of 25°C to 260°C at a heating rate of 10°C/min.

Dynamic Mechanical Analysis (DMA) was performed on TA Instrument Q800 to evaluate the viscoelastic properties (storage modulus, loss modulus, and  $\tan\delta$ ) of composites in the solid state. A three-point bending mode was used at a test temperature range of 25°C to 120°C and a constant heating rate of 3°C/min at 1 Hz frequency of dynamic force.

**Table 1.** PVC foam composites formulation.

Sample Number	Glass Fiber	PVC Resin	Stabilizer	Blowing Agents	Lubricants	Processing Aid
GF0	0	92.5				
GF5	5	87.5				
GF10	1/16"	10				
GF15		15				
GF20		20	0.85	0.5	0.6	6
GF5	5	87.5				
GF10	1/32"	10				
GF15		15				
GF20		20	72.5			

The dimensional stability of the foam composites was analyzed using AAMA (American Architectural Manufacturers Association) standards. Extruded samples were heated in an oven at 82°C for 30 minutes. The original dimensions of the foam composites were 12" × 1" × 0.28". The change in length was measured after 4 hours and reported as a shrinkage percentage according to Equation (1), where  $l_o$  and  $l_f$  are the initial and final lengths; respectively:

$$\% \text{ Shrinkage} = \frac{l_o - l_f}{l_o} \times 100 \quad (1)$$

Heat resistance of the composites were analyzed according to AAMA standards. Extruded samples were heated in an oven at 141°C for 30 minutes. The original dimensions of the foam composites were 12" × 1" × 0.28". Visual inspection on the samples was done to determine the presence of any flaws or distortion after cooling down for four hours on a dry and clean surfaces.

## 2.4. Mechanical Properties

Tensile properties were determined using an Instron 3365 universal testing machine on rectangular specimens measuring 12" × 1" × 0.28" at a crosshead speed of 0.5 in/min. Flexural properties were determined using Instron 3365 with a three-point bending test set-up on rectangular specimens measuring 8" × 1" × 0.28" at a crosshead speed of 0.5 in/min. The span length was kept at 4 inches. The flexural stress and strains were calculated using Equations (2) and (3):

$$\sigma_f = \frac{3PL}{2bd^2} \quad (2)$$

$$\varepsilon_f = \frac{6Dd}{L^2} \quad (3)$$

where,  $\sigma_f$  and  $\varepsilon_f$  are the respective flexural stress and strain at the midpoint, and  $P$ ,  $L$ ,  $b$ ,  $d$ ,  $D$  are the load, span length, specimen width, specimen thickness and midpoint deflection; respectively. The flexural strength was determined using the maximum stress value recorded before sample fracture and flexural modulus was determined by the slope of the initial linear region of the stress-strain curve.

Charpy impact properties were determined using Tinus Olsen impact testing machine (model IT 504) according to ASTM D 6110. Four samples of each composite were tested. The dimensions of the impact testing samples were 5" × 0.5" × 0.28" with a 45° notch at the middle.

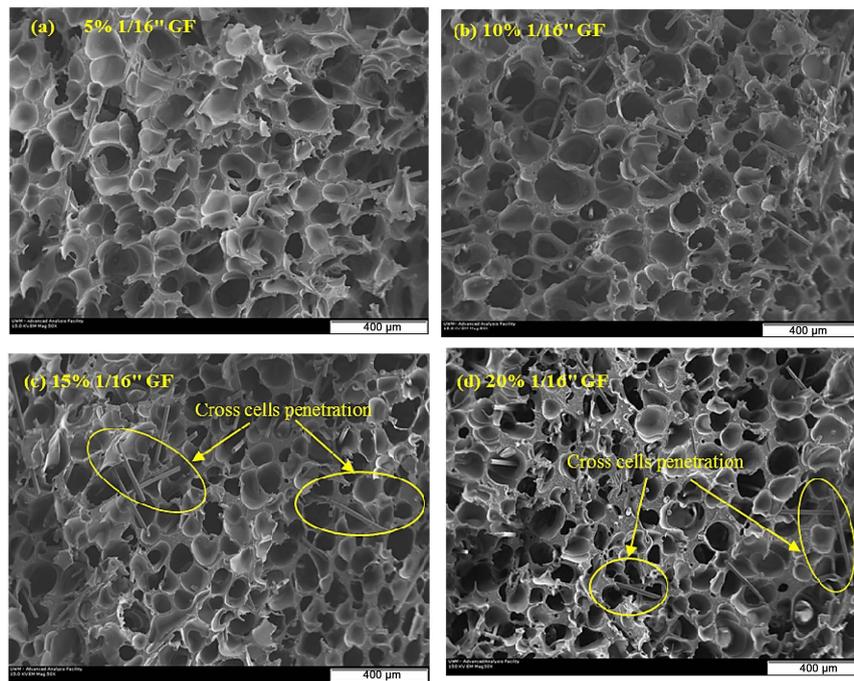
## 2.5. Scanning Electron Microscopy (SEM)

Topcon SM-300 SEM was used for imaging and microstructural analysis of the extruded PVC-GF foam composites. The specimens were fractured in liquid nitrogen and coated using a sputter coater to minimize the charging effect and to improve the conductivity of the samples prior to analysis.

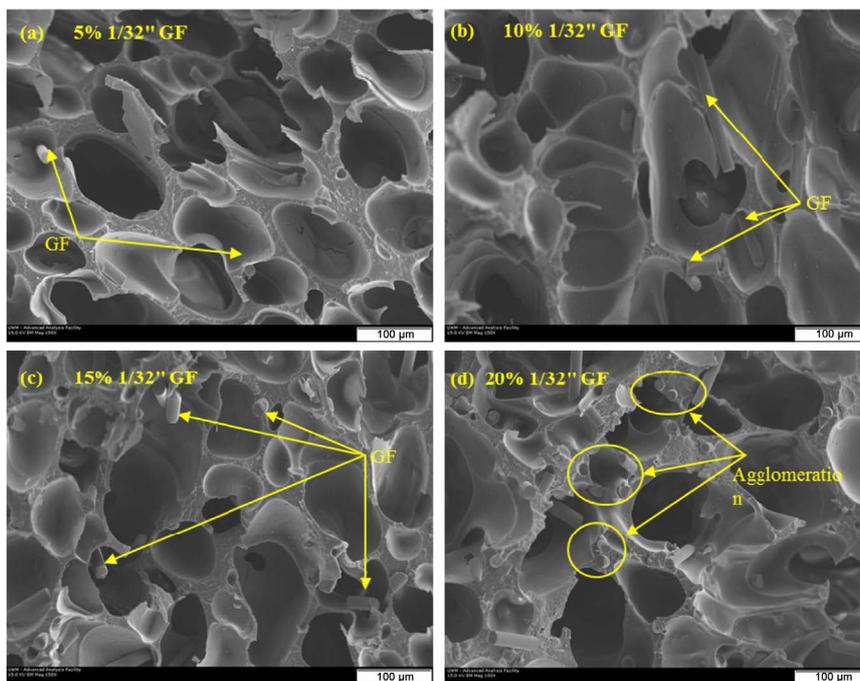
## 3. Results and Discussion

### 3.1. Microstructure and Morphology

The dispersion and surface bonding of the solid phase with the host polymer matrix affects many important characteristics; such as mechanical properties and dimensional stability [16] [17]. Therefore, it is important to study the fiber-matrix interface in order to explain the characteristics and behavior of these composites. **Figures 1(a)-(d)** shows the dispersion of 1/16" GFs in the PVC foam matrix at 50x magnification; whereas **Figures 2(a)-(d)** shows the dispersion of 1/32" GFs in the PVC foam matrix at 150x magnification. One can observe in both sets of micrographs the random orientation and dispersion of GF in the matrix, and the penetration of the long fibers through the closed cell walls. In the case of 1/16" GFs, the penetration is across multiple cell walls, as shown in **Figure 1(c)**; whereas the penetration in the case of 1/32" GFs is mostly limited to individual cell walls, as shown in **Figure 2(c)**. Fiber dispersion is a function of the fiber lengths; shorter fibers tend to agglomerate more than the longer fibers during processing due to the liquid additives used in the compounding process.

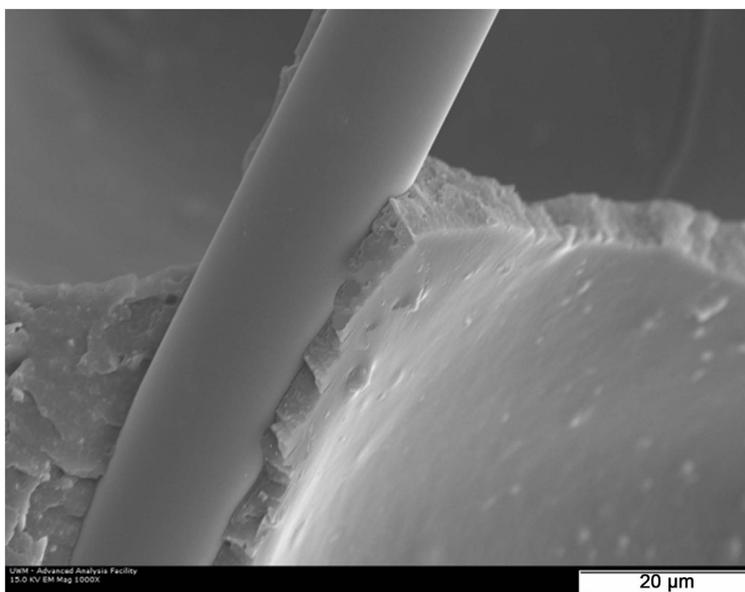


**Figure 1.** SEM micrographs at 50× of 1/16" GF-PVC (a) 5% (b) 10% (c) 15% (d) 20%.



**Figure 2.** SEM micrographs at 150× of 1/32" GF-PVC (a) 5%; (b) 10%; (c) 15%; (d) 20%.

**Figure 3** shows a close up image of a fiber-matrix interface at 1000× magnification. The orientation of this particular fiber is along the fracture surface, whereas the majority of fibers which are present in the foam matrix are across the fracture surfaces. However, the fracture surface shown in **Figure 3** seems to be clean, which indicates poor bonding between the two surfaces. In addition, the diameter of the GF seems to be close to the thickness of the cell wall, or higher at some locations. Both these observations may be significant to the effect of GF on the mechanical and thermal performance of the composite matrix.



**Figure 3.** SEM micrograph at 1000 $\times$  of a glass fiber interface with PVC foam.

### 3.2. Thermal Properties

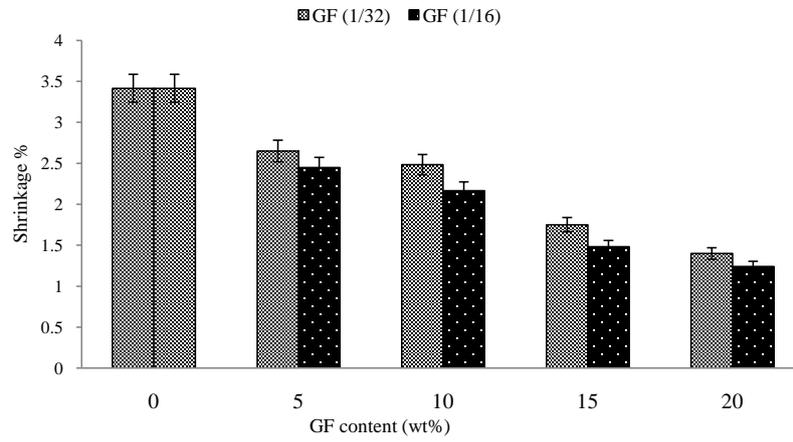
Dimensional stability of the foam composites was measured as a percentage of shrinkage; the effect of GF lengths and loading is presented in **Figure 4**. The percentage of shrinkage decreased by 22.5% and 28.4% when adding 5% of 1/32" and 1/16" GFs; respectively, compared with pristine samples. It is evident that dimensional stability increases significantly with increasing the GF content in the composites. This is due to the higher solid content in the polymer matrix, which has higher resistance to thermal expansion and/or contraction. A comparison between the samples made with the same filler content at different GF lengths reveals that the composites containing longer GF (1/16") exhibit higher dimensional stability improvement than those with shorter GF. This may be attributed to a higher interlocking and bonding between longer GF and the foam matrix along the fiber length. Since GF has lower coefficient of thermal expansion than the polymer matrix, higher interaction between the fibers and the matrix improves dimensional stability of the composites.

Heat resistance was evaluated qualitatively by visual inspection for surface flaws and shape distortion of the extruded samples after subjection to heating and cooling cycles. Although, the test samples did not show any flakes or cracks on the surface, some distortion was observed on the sides. It was also observed that the addition of GF reduced the amount of swelling. In addition, the composites containing 1/16" GFs exhibited higher heat resistance when compared with those containing shorter GF lengths. Meanwhile, the addition of GF does not seem to affect the glass transition temperature ( $T_g$ ) of the PVC foam composites, around 82°C, as shown in **Table 2**. Similar conclusions were presented by Hassan *et al.* [9].

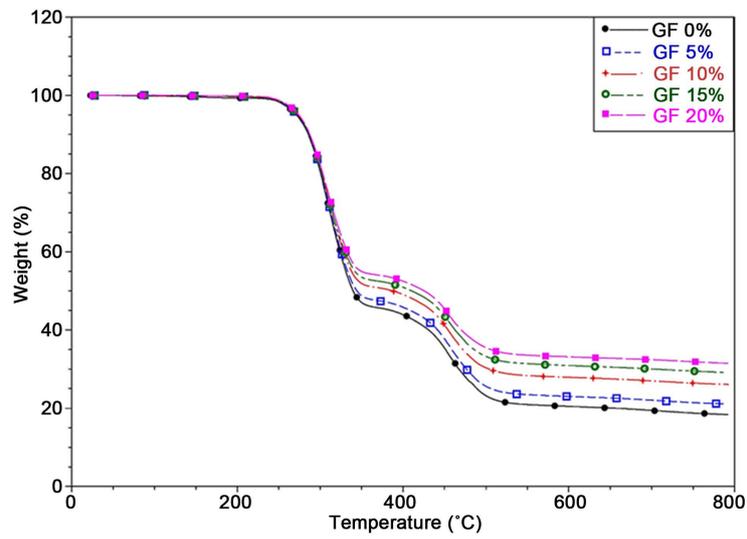
The results from TGA analysis of PVC-GF foam composites are presented in **Figure 5**. The average Primary Degradation Temperature (PDT) of the foam composites begins around 277°C, while the average Secondary Degradation Temperature (SDT) is around 440°C.

Increasing GF content increases the secondary decomposition temperature of the composites, as shown in **Table 3**, which means that it takes more energy to break the hydrocarbon backbone of the polymer matrix [20] [21]. On the other hand, the PDT of the composites, which indicates the start of the separation process of chlorine from the polymer chains, decreases slightly by increasing the GF content. This can be attributed to the higher thermal conductivity of GF, which results in faster heat transfer into the PVC matrix and thermal degradation starting at lower temperatures [21]. The residual weight at 800°C is found to increase with increasing GF content due to the higher content of inorganic filler in the matrix.

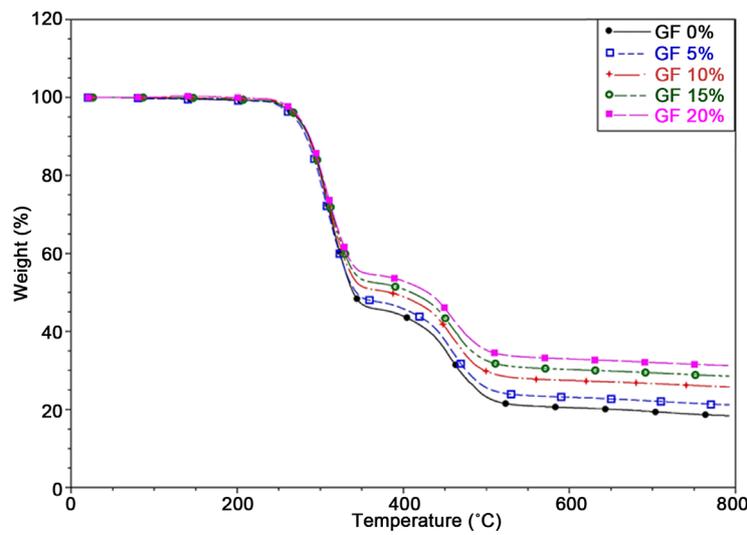
Thermo mechanical properties of the PVC-GF composites were determined by DMA analysis. Variations in the storage modulus ( $E'$ ), which represents the elastic behavior, and the loss modulus ( $E''$ ), which represents the viscous behavior, with temperature, are shown in **Figure 6** and **Figure 7**; respectively. The storage modulus and the peak intensity of the loss modulus increased with the addition of GFs and were the highest at 15% GF, for both



**Figure 4.** Dimensional stability of PVC-GF foam composites.

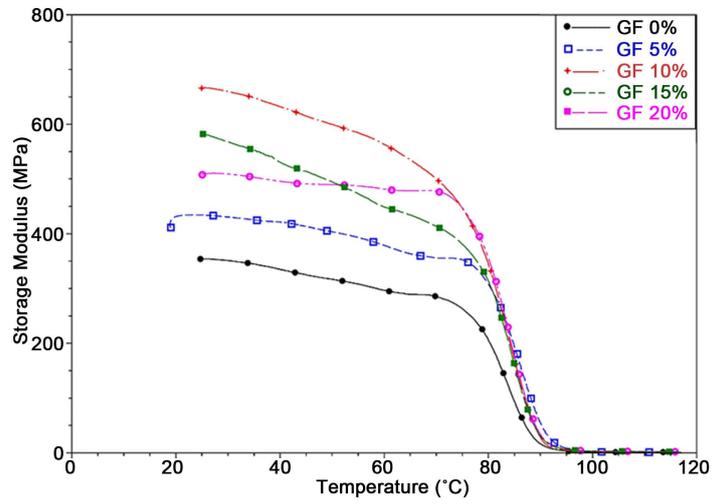


(a)

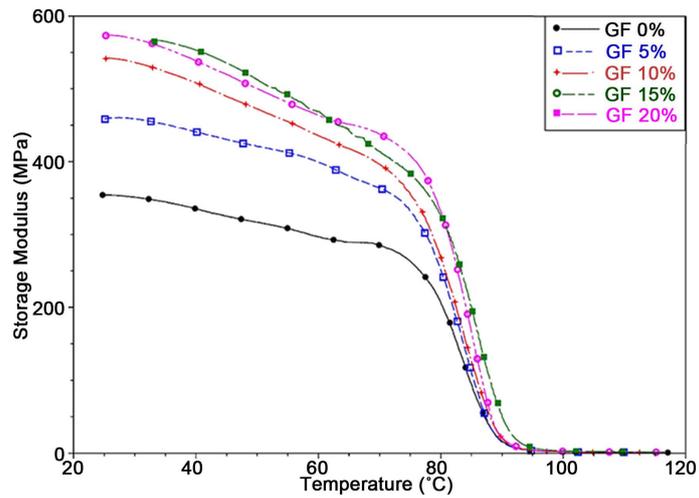


(b)

**Figure 5.** TGA analysis for PVC-GF composites (a) 1/16"; (b) 1/32".

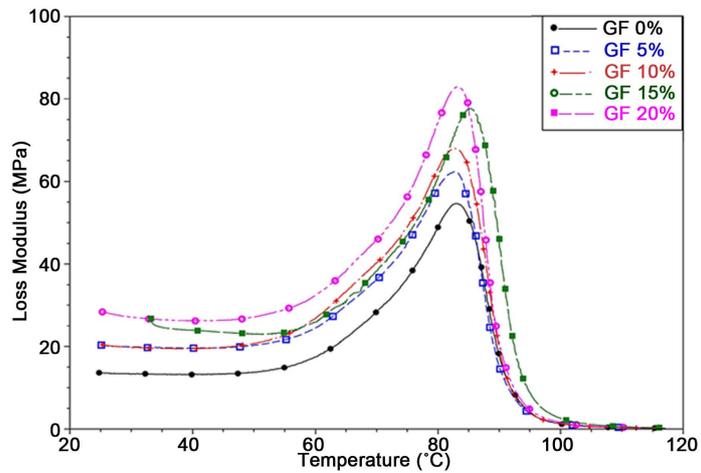


(a)

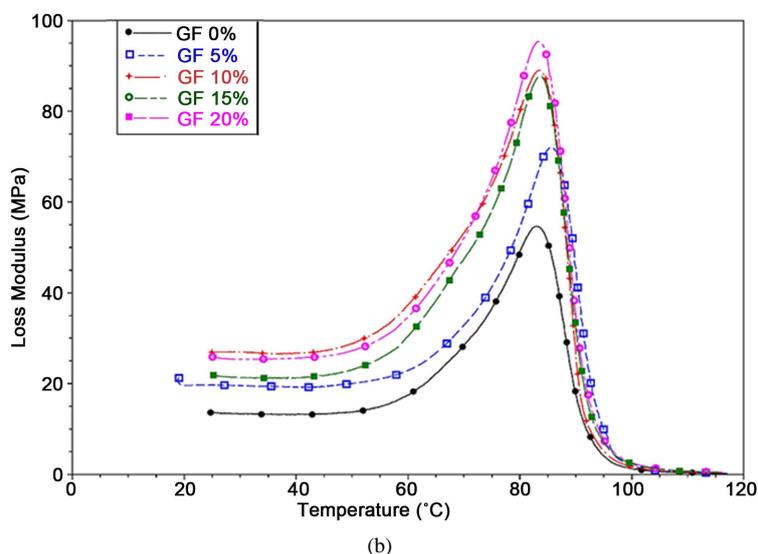


(b)

**Figure 6.** Storage Modulus ( $E'$ ) of PVC-GF composites (a) 1/16"; (b) 1/32". The curves are labeled with respect to the value of storage modulus from top to bottom.



(a)



**Figure 7.** Loss Modulus ( $E''$ ) of PVC-GF composites (a) 1/16"; (b) 1/32". The curves are labeled with respect to the value of loss modulus from top to bottom.

**Table 2.** Glass transition temperatures of the GF-PVC composites measured by DSC.

GF wt%	0%	5%	10%	15%	20%
<b>Fiber Length</b>	N/A	1/16"	1/32"	1/16"	1/32"
<b>T<sub>g</sub> (°C)</b>	82.21	82.47	81.93	82.97	83.8

**Table 3.** Primary and secondary decomposition temperature of PVC-GF composites.

Sample	Glass Fiber	PDT (°C)	SDT (°C)
GF0	0%	279.39	442.25
GF5	5%	278.21	439.36
GF10	10%	278.57	441.78
GF15	15%	276.73	440.63
GF20	20%	277.31	439.04
GF5	5%	276.66	436.23
GF10	10%	277.15	437.73
GF15	15%	277.23	437.85
GF20	20%	277.27	443.67

GF lengths. This is attributed to the enhancement in the energy dissipation ability in the presence of solid fillers in the polymer matrix and the increase in the polymer-filler and filler-filler slippages at T<sub>g</sub> [21] [22].

However, at 20 wt% GF concentration, the magnitude of  $E'$  and  $E''$  decrease due to the agglomeration of GFs at higher concentrations, as was shown earlier by SEM analysis (Figure 2(d)). The agglomeration of GFs leads to higher friction between the fibers and less interaction between the reinforcing phase and the host matrix. Consequently, the energy dissipation in the reinforced polymer matrix is reduced [17]. Similarly, the composites with 1/16" GFs exhibit higher storage and loss moduli compared to the 1/32" GFs. The storage modulus increased from 350 MPa to 650 MPa with the addition of 10% 1/16" GFs; whereas it increased only to 550 MPa with the addition of 10% 1/32" GFs. The loss modulus ( $E''$ ) peak increased to from 53 MPa to 95 MPa and 83 MPa in the case of 15%-1/16" and 15%-1/32" GFs; respectively. This is also attributed to the higher energy dissi-

pation in the presence of longer glass fibers due to higher interaction between the fibers and the polymer matrix.

### 3.3. Mechanical Properties

The mechanical properties of polymer GF composites highly depend on the geometry of the reinforcement phase; such as the length and diameter of the GF [12]. **Table 4** summarizes the effect of GF length and content on the mechanical properties of PVC-GF composites. Since the bonding between GFs and the polymer foam occurs only through the cell walls, the enhancement in the foam strength is limited and is greatly affected by the bonding strength between the two surfaces. However, longer fibers are likely to have more bonding sites due to higher penetration through the walls of the closed cell foams. The ultimate tensile strength (UTS) of the composite foams seems to maintain its value at different loadings of GF. Meanwhile, the composites made with longer glass fibers (1/16") seem to have slightly higher UTS at all loading levels. A similar effect of the glass fibers length on the UTS is also visible with the flexural strength measurements shown in **Table 4**.

The ductility of the PVC-GF composites, measured by the extension at break, was noticed to decrease in the presence of glass fibers. Higher amounts of GFs in the polymer matrix render the composite more brittle and prone to brittle fracture as they are dispersed in the matrix with no specific orientation. Longer GF (1/16") exhibit higher reduction in ductility compared to the shorter fibers; this is also attributed to the higher penetration of the longer fibers in the walls of the closed cell foams which increases the stiffness of the structure.

The impact strength of the PVC-GF composites decreases with the addition of GFs irrespective of their lengths. In the case of 1/16" GFs, the impact strength decreased from 33 J/m<sup>2</sup> at 5%GF to 25 J/m<sup>2</sup> at 20% GF, which is a 24% reduction. However, the reduction in impact strength in the case of 1/32" GFs was higher and at 29%, *i.e.*, 31 J/m<sup>2</sup> at 5%GF and 22 J/m<sup>2</sup> at 20%GF. The longer fibers tend to strengthen the composite matrix as they are able to penetrate across multiple cell walls and thus interlocking the matrix between the fibers themselves, which leads to better load distribution [13].

## 4. Conclusions

Dimensional stability of PVC-GF foam composites measured by thermal shrinkage and heat resistance was improved significantly with the addition of GF to the foam composites. Thermal shrinkage decreased by almost 60%, with visible improvements to the shape distortion. Longer GF yielded better improvement than shorter fibers due to their higher interaction with the foam cells. SEM images of the foam cells confirmed the random distribution and orientation of the GF in the polymer matrix; the connections between the GFs and the matrix are only through the walls of the foam-matrix. Also, SEM images confirmed that longer GFs exhibit higher crossings through the composite walls, and more interlocking between the fibers themselves.

Mechanical properties of the PVC-GF composites have mixed reactions. Whereas the tensile and flexural strengths seem to be marginally affected by the addition of GFs, the ductility and impact strengths decreased significantly with higher GF loadings. However, longer GFs scored better than their shorter counterparts due to

**Table 4.** Mechanical properties of PVC-GF composites.

Sample	Glass Fiber	UTS (MPa)	Ductility (mm)	Flexural Strength (MPa)	Impact Strength (J/m <sup>2</sup> )	
GF0	0%	8.17	43.43	17.26	30.13	
GF5	5%	8.91	38.08	17.92	33.08	
GF10	1/16"	10%	8.56	16.68	29.81	
GF15		15%	8.69	16.13	28.89	
GF20		20%	8.55	18.58	25.47	
GF5		5%	8.68	37.80	16.59	30.92
GF10	1/32"	10%	8.28	15.70	29.06	
GF15		15%	8.44	17.00	23.75	
GF20		20%	8.31	30.83	16.19	21.58

higher interlocking between the fibers and the foam cells, which results in better load distribution in the matrix. The viscoelastic properties of the PVC-GF composites measured by storage and loss moduli were enhanced by the addition of GFs with better improvements in the case of longer GFs.

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