

Numerical Solution to Boundary Layer Problems over Moving Flat Plate in Non-Newtonian Media

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ABSTRACT

Our aim is to investigate the solutions to the boundary layer problem of a power-law non-Newtonian fluid along an impermeable sheet moving with a constant velocity in an otherwise quiescent fluid environment. In the absence of an exact solution in closed form, numerical solutions for the velocity distribution in the boundary layer for different power exponents will be presented. Our goal is to give an iterative transformation method for the determination of the skin friction parameter and the boundary layer thickness for different parameter values and the dependence of the skin friction parameter and the boundary layer thickness on the power exponent are examined.

KEYWORDS

Boundary Layer Problem; Non-Newtonian Fluid; Skin Friction Parameter; Iterative Transformation Method

1. Introduction

The study of flow generated by a moving surface in an otherwise quiescent fluid plays a significant role in many material processing applications such as hot rolling, metal forming and continuous casting (see e.g., [1-3]).

Boundary layer flow induced by the uniform motion of a continuous plate in a Newtonian fluid has been analytically studied by Sakiadis [4] and experimentally applied by Tsou *et al.* [5]. A polymer sheet extruded continuously from a die traveling between a feed roll and a wind-up roll was investigated by Sakiadis [4,6]. He pointed out that the known solutions for the boundary layer on surfaces of finite length are not applicable to the boundary layer on continuous surfaces. In the case of a moving sheet of finite length, the boundary layer grows in a direction opposite to the direction of motion of the sheet.

Tsou *et al.* [5] showed in their analytical and experimental study that the obtained analytical results for the laminar velocity field are in excellent agreement with the measured data, therefore it validates that the mathematical model for boundary layer on a continuous moving surface describes a physically realizable flow.

The problems of the boundary layer over a continuous surface moving in an otherwise quiescent fluid environment have attracted considerable attention (e.g., [1-3,5,7,8]). In this paper we use the power-law rheological model for the flow of a fluid over a sheet. In the absence of an exact solution in closed form, numerical solutions for the velocity distribution in the boundary layer for different power exponents will be presented, and the dependence of the skin friction parameter and the boundary layer thickness on the power exponent n are examined.

2. Mathematical Model

2.1. Boundary Layer Equations

Consider the two-dimensional steady flow of a non-Newtonian fluid of density ρ modeled by a power law fluid due to Ostwald-de Waele over a flat plate moving continuously with a constant velocity U_w in an otherwise quiescent fluid medium [5]. The governing equations of motion and heat transfer for non-Newtonian flow neglecting pressure gradient, body forces can be described by the following equations [5]:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, \qquad (1)$$

and

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \frac{1}{\rho} \frac{\partial \tau_{xy}}{\partial y}, \qquad (2)$$

where u, v are the velocity components along x and y coordinates, respectively, T is the temperature of the fluid in the boundary layer. Furthermore, we apply power-law relation $\tau_{xy} = K \left| \frac{\partial u}{\partial y} \right|^{n-1} \frac{\partial u}{\partial y}$ between the

shear stress and the shear rate, where $\mu_c \left| \frac{\partial u}{\partial y} \right|^{n-1}$ denotes the kinematic viscosity, *K* the consistency index for

non-Newtonian viscosity and $\mu_c = \frac{K}{\rho}$. Here, *n* is called power-law index, that is n < 1 for pseudoplastic, n = 1 for Newtonian, and n > 1 for dilatant fluids. Then, differential Equation (2) becomes [9]

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$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \frac{\partial}{\partial y} \left(\mu_c \left| \frac{\partial u}{\partial y} \right|^{n-1} \frac{\partial u}{\partial y} \right).$$
(3)

The boundary conditions of the flow can be expressed as

 $u(x,0) = U_w, v(x,0) = 0, \lim_{x \to \infty} u(x,y) = 0.$

If a flat plate in surroundings at rest is moved with constant velocity U_w , the no-slip condition means that boundary layer exists close to the wall (see Figure 1). The moving plate emerges from the wall. This fixes the origin of the coordinate system and has an analog to the leading edge of a flat plate at zero incidence in a flow. Both permit only then a steady solution in a spatially fixed coordinate system.

2.2. Similarity Transformation Method

The continuity Equation (1) is satisfied by introducing a stream function ψ such that

$$u = \frac{\partial \psi}{\partial y} \quad , v = -\frac{\partial \psi}{\partial x} \,. \tag{4}$$

The momentum equation can be transformed into the corresponding ordinary differential equation by the following transformations

$$\psi(x,y) = \mu_c^{\frac{1}{n+1}} \left(U_w \right)^{\frac{2n-1}{n+1}} x^{\frac{1}{n+1}} f(\eta), \quad \eta = \mu_c^{-\frac{1}{n+1}} \left(U_w \right)^{\frac{2-n}{n+1}} \frac{y}{x^{\frac{1}{n+1}}},$$

where η is the similarity variable and $f(\eta)$ is the dimensionless stream function. Equation (3) with the transformed boundary conditions can be written as



Figure 1. The physical model of the boundary layer on a continuously moving surface.

$$\left(\left|f''\right|^{n-1}f''\right)' + \frac{1}{n+1}ff'' = 0,$$
(5)

$$f'(0) = 1, \ f(0) = 0, \ f'(\infty) = \lim_{\eta \to \infty} f'(\eta) = 0,$$
 (6)

where the prime denotes the differentiation with respect to the similarity variable η . Equation (5) is called the generalized Sakiadis equation. The dimensionless velocity components have the form: u(x,y) = U - f'(y)

$$w(x, y) = \frac{U_w}{n+1} R e_x^{\frac{n}{n+1}} \left(\eta f'(\eta) - f(\eta) \right),$$

and $\eta = Re_x^{\frac{1}{n+1}} y / x$, where $Re_x = \rho U_{\infty}^{2-n} x^n / K$ is the local Reynolds number.

Since the pioneering work by Acrivos [10], different approaches have been investigated for f''(0) in the case of non-Newtonian fluids. It has a physical meaning: *drag force* or force due to *skin friction*. It is a fluid dynamic resistive force which is a consequence of the fluid and the pressure distribution on the surface of the object. The *skin friction parameter* f''(0) originates from the non-dimensional *drag coefficient*

$$C_{D} = (n+1)^{\frac{1}{n+1}} R e^{\frac{-n}{n+1}} \left| f''(0) \right|^{n-1} f''(0),$$

and it is involved in the wall shear stress

$$\tau_{w}(x) = \left[\frac{\rho^{n} K U_{w}^{3n}}{x^{n}}\right]^{\frac{1}{n+1}} \left|f''(0)\right|^{n-1} f''(0).$$

The boundary value problem (5), (6) is defined on a semi-infinite interval [11]. For Newtonian fluids (n = 1), Equation (5) is the well-known Blasius equation:

$$f''' + \frac{1}{2}f f'' = 0.$$
⁽⁷⁾

Blasius [12] solved Equation (7) subject to boundary conditions

$$f'(0) = 0, \ f(0) = 0, \ f'(\infty) = \lim_{\eta \to \infty} f'(\eta) = 1$$
 (8)

by patching a power series to an approximation at some finite value of η . An iterative transformation method was introduced for (7), (8) by Töpfer for the determination of f''(0) (see [13]).

Equation (5) with (8) is called the generalized Blasius problem [12]. For non-Newtonian fluids on steady surfaces, the boundary value problem (5), (6) has been investigated in [14,15] and for Newtonian fluid in [16,17].

The aim of this paper is to give a method for the determination of the skin friction parameter f''(0) and the boundary layer thickness for different parameter values *n*.

3. Iterative Transformation Method

In this section an iterative transformation method (ITM) is developed to solve the boundary value problem (5), (6). Solving this problem, we have to deal with a practically unsuited condition at infinity. To tackle this computational difficulty, we apply the so-called scaling concept. Non-iterative and iterative transformation methods for boundary value problems have been introduced by Fazio [18].

The idea behind the present method is to consider the "partial" invariance of (5), (6) with respect to a scaling transformation in the sense that the differential equation and one of the boundary conditions at 0 are invariant, while the other two boundary conditions are not invariant. Therefore, we modify the problem by introducing a numerical parameter *h*. Now, Equation (5) is to be solved with boundary conditions

$$f(0) = 0, \quad f'(0) = h^p, \quad f'(\infty) = \lim f'(\eta) = 1 - h^p,$$

where we involve *h*, to ensure the invariance of the extended scaling group.

We introduce the following transformations to convert the boundary value problem to an initial value problem,

where the following scaling transformation is applied and $f''(0) = -\sigma$ is denoted:

$$g = \lambda^{\alpha} f, \eta^* = \lambda^{\beta} \eta, h^* = \lambda^{\gamma} h.$$

Equation (5) is scaling invariant if

$$(2-n)\alpha = (1-2n)\beta.$$
⁽⁹⁾

Then, one gets

$$\left(\left|g''\right|^{n-1}g''\right)' + \frac{1}{n+1}gg'' = 0.$$
⁽¹⁰⁾

The appropriate boundary conditions can be determined from the proper derivatives of f:

$$f(0) = \sigma^{-\alpha} g(0) = 0 \tag{11}$$

$$f'(0) = h^{p} \Longrightarrow \lambda^{\beta - \alpha} g'(0) = \left(\lambda^{-\gamma} h^{*}\right)^{p}$$
(12)

$$f'(\infty) = 1 - h^{p} \Longrightarrow \lambda^{\beta - \alpha} g'(\infty) = 1 - \left(\lambda^{-\gamma} h^{*}\right)^{p}$$
(13)

$$g''(0) = \lambda^{\alpha - 2\beta} f''(0).$$
⁽¹⁴⁾

We can observe from Equation (11) that the first boundary condition in (6) is scaling invariant. The other two boundary conditions are not invariant.

Now, let $\lambda = \sigma$ and g''(0) = -1. From (9), (12) and (14) we get the following expressions for the scaling parameters:

$$\alpha = \frac{1-2n}{3}, \quad \beta = \frac{2-n}{3}, \quad \gamma = -\frac{1}{p}\frac{1+n}{3}.$$
(15)

Utilizing the boundary condition prescribed at infinity, from (13) we gain a formula for the sought value of $\sigma = -f''(0)$:

$$\sigma = \left(g'(\infty) + h^{*p}\right)^{-\frac{3}{n+1}} \tag{16}$$

During the calculating process, *p* is freely chosen.

Now, we can write the initial values in their final forms:

$$g(0) = 0, g'(0) = h^{*p}, g''(0) = -1.$$
 (17)

The initial value problem (10), (17) is solved with the so-called iterative transformation method. Its steps are enumerated below:

1) A numerical parameter h is applied so that two boundary conditions remain invariant.

2) By starting with a suitable value of h^* , a root finder algorithm is used to define a sequence h_i^* for $j = 0, 1, \cdots$. After each iteration the group parameter λ is obtained by solving the IVP numerically. The sequence is defined by $\Gamma(h^*) = h - 1 = 0$.

3) An adequate termination criteria must be used to verify whether $\Gamma(h_i^*) \to 0$ as $i \to \infty$.

4) The solution of the original problem can be received by rescaling to h = 1.

4. Results

The nonlinear ordinary differential Equation (10) with the boundary conditions in (17) was solved for some values of the power-law index *n* by MATLAB. The built-in ode113, a variable order Adams-Bashforth-Moulton solver was used with default accuracy and adaptivity parameters and η_{max} was determined when the local error was less than 10^{-6} . As for the root finder algorithm, we programmed the bisection method because of safety considerations.

We may remark that if f' is demanded to decrease monotonically, then f'' is negative for every possible η . Therefore choosing a positive number for g''(0), h never reaches 1 which is the case for n=1 [19]. Numerical results for function values f''(0) are shown below in Table 1.

For n = 1 we reproduced the result achieved by Fazio. Figure 2 illustrates the $f'(\eta)$ function, which is

0.96 0.97 0.98 0.99 1 1.1 1.2 n f"(0) -0.443438 -0.443438-0.443286 -0.443193 -0.443726-0.436611-0.4098341.3 1.4 1.42 1.45 1.48 1.49 1.5 n f"(0) -0.361843 -0.282487-0.259809-0.217169 -0.154069-0.123517 -0.081410





Figure 2. Similarity velocity profiles for power-law non-Newtonian fluid.

proportional to the non-dimensional velocity component, for different power law indices n.

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