

Design and Application of a MCU-based Smart Contactor System

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ABSTRACT

This paper aims to design a MCU-based smart contactor system, which will realize functions of real time surveillance of contactors' work status and data exchange with host computer, thus instantly reflect different status of the system. In case of abnormal status such as over-current or under-voltage, the contactor will be able to automatically cut off power supply to protect electrical load and the circuit. Through ARINC485 bus, system computer will collect and record contactor parameters, including contact voltage, contact current, supply frequency, contact temperature and contact status to provide critical data to the examination and repair of contactors.

Keywords: Aerial Contactor; MCU; Testing; ARINC485

1. Introduction

Aerial contactors have many applications in aircrafts and play an important role in power supply for on-board equipments and instruments. A malfunctioned contactor would cause the destruction of electric load and, even worse, an on-board electrical fire. Hence, the performance of contactors has direct impact on power supply quality for on-board system devices and has a close relation with flight safety. If it is possible to carry out real time surveillance and recording of contactors during a flight, then arising fault would be instantly detected and relative electrical load be disconnected to ensure the normal functioning of other electrical loads and power circuits. By this way, accident caused by breakdowns such as short circuit will be avoided and flight safety would be greatly improved. Meanwhile, maintenance interval will be greatly shortened and operation cost be saved as maintenance personnel are directed to targets based on system information, such as recorded contactor status.

2. System Design

First, we select Micro Controller Unit (MCU) as the system's main control chip to realize functions of surveillance and communications. Second, make sure the device is able to perform real time measuring of three phase voltage and current as signal excursion may appear. To enable an accurate measurement, we need to synchronize the sampling frequency of MCU A/D with signal frequency and phase position, which calls for three-phase AC signal measuring. What's more, enable the direct

control of contactor through the driving of contactor coil via I/O signal and the receiving of external control level. At last, make sure the Full-duplex communication by way of two groups of half-duplex operation RS485. The system structure framework is shown in **Figure 1**.

2.1. Hardware Design

The system controller adopts MSP430F149 [1] MCU, an ultra-low power consumption unit produced by TI.The MCU is especially suitable for battery applications or handheld devices. Besides, the integration of a large amount of peripheral modules into the controller unit enables the MCU a perfect option for the design of SoC; and abundant alternative components with various types also enrich its flexibility for designers. As a 16 bit simplified instruction architecture, the MCU has plenty of working registers and data storage units, including

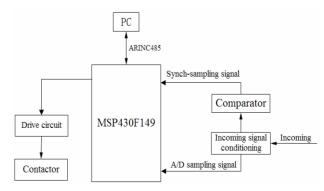


Figure 1. System structure framework.

calculation enabled RAM units. Except for the selection of controller, it also satisfies the design of voltage and current transducers.

2.1.1. Design of Voltage Transducer

Adopt an isolation transformer voltage drop method. Take Model HPT205NB voltage transformer as the isolation transformer. See its parameters as follows: Incoming current: 0 - 2 mA, Output current: 0 - 2 mA, Precision: 0.1%, Linearity: 0.07%, Phase shifting: $\leq 11'$, Isolation withstand voltage: 2700 Vac, Internal resistance: 105Ω . Its main advantages are shown in the schematic diagram of circuit (see **Figure 2**), including high signal isolation, strong anti-jamming capability and conformity to requirements for industrial anti-jamming system design.

2.1.2. Design of Current Transducer

Adopt A1302 linear Hall sensor [2] produced by Allegro. A1302 is a successive type proportional linear Hall Effect sensor, which is able to provide precise proportionable voltage output values with the applied magnetic field. It has a static output voltage which equals with 50% of supply voltage. Its output sensitivity is 1.3 mV/G. See its application circuit diagram in **Figure 3**.

In **Figure 3**, power source of the transducer is provided by a DC/DC uncontrolled rectifier, which goes through two levels II type filtering and a voltage regulator tube. This enables the stability and precision of signal measurement. After capacitor filtering and voltage partial pressure, output signal from transducer will be sent to MCU A/D for processing.

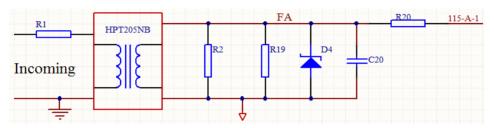


Figure 2. Step-down circuit of isolating transformer.

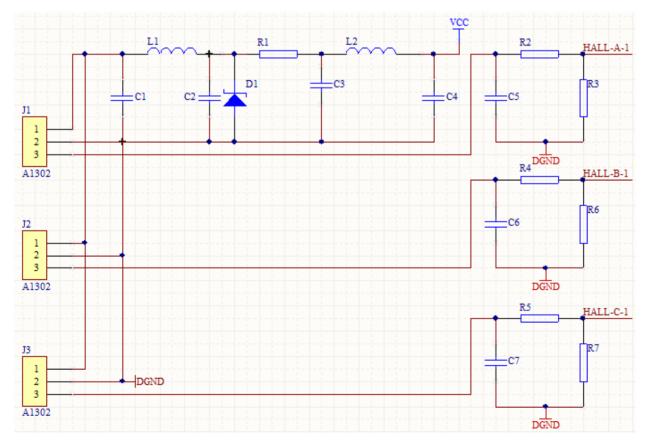


Figure 3. Circuit diagram of hall current signal conditioning.

2.2. Software Design

Considering the frequency jitter of tested signal is not large and will not result in serious wave distortion, we use input capture terminal to trigger the sampling, and then continuously take samples at numerous points (within the range of 1 – 1.5 circle) and then take down results. Calculate the digital value of these signals' amplitude, and then determine proportional relation of effective values through fitting method in experiments to obtain effective value of the signals. Such a solution of sampling and calculation not only saves hardware resources, reduces the size of circuit board, but also saves precious RAM resource in MSP430F149, thus enhancing the utilization of stack and acquiring a qualified speed for real time surveillance. The controller software flow path

is shown in Figure 4.

3. System Testing

3.1. System Testing Platform

A testing platform is required for a comprehensive testing of system functions and system performance. The platform consists of power source, electrical load, protection device, standard measuring equipments and etc. See block diagram of the platform in **Figure 5**.

3.2. Analysis of Experimental Data

Use fitting method to obtain proportional relation of measured signals' virtual values and then determine the final virtual values.

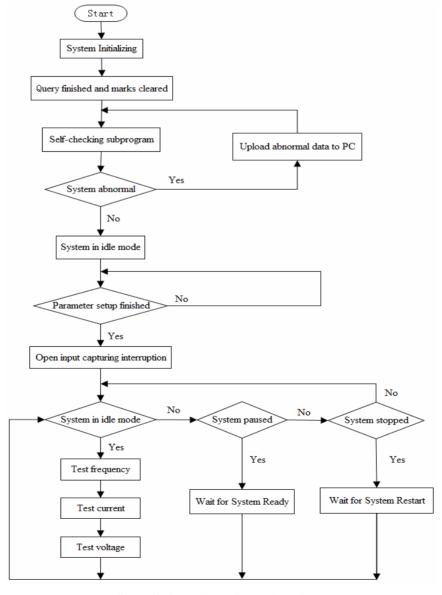


Figure 4. Controller software flow chart.

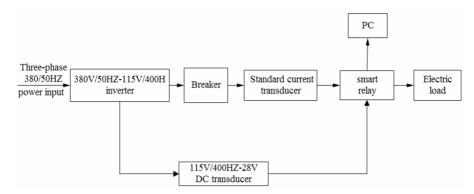


Figure 5. Block diagram of system testing platform.

3.2.1. Analysis of Current Data

Given a polynomial as equation (1), then a corresponding normal equation is obtained as equation (2).

$$\psi(x) = a_0 + a_1 x + a_2 x^2. \tag{1}$$

$$\begin{bmatrix} 26 & \sum x_i & \sum x_i^2 \\ \sum x_i & \sum x_i^2 & \sum x_i^3 \\ \sum x_i^2 & \sum x_i^3 & \sum x_i^4 \end{bmatrix} \begin{bmatrix} X_0 \\ X_1 \\ X_2 \end{bmatrix} = \begin{bmatrix} \sum y_i \\ \sum x_i y_i \\ \sum x_i^2 y_i \end{bmatrix}$$
(2)

Calculate with the help of MATLAB to get fitting polynomials of phase A, B and C as equation (3).

$$\begin{cases} \psi_A(x) = 11.1562 + (-0.0018)x + (2.6088e - 006)x^2 \\ \psi_B(x) = 10.3004 + (-0.0013)x + (2.2989e - 006)x^2 \\ \psi_C(x) = 10.5804 + (-1.9585e-004)x + (9.1916e - 007)x^2 \end{cases}$$

Conduct fitting process on each point's electrical current scaling factor to get a proportionality coefficient curve. Together with the proportionality coefficient of each point obtained through experimental data, it is shown in **Figure 6**.

Based on proportional coefficient of each point obtained through fitting, determine corresponding nominal current value and display the contrast relation with actual current values in Figure 7.

Final experimental results indicated that the deviation between obtained three-phase experimental current value and the actual current value is about 0.1%, which is able to meet engineering design requirements.

3.2.2. Analysis of Voltage Data

Given a polynomial as equation (4), then a corresponding normal equation is obtained as equation (5).

$$\psi(x) = a_0 + a_1 x. \tag{4}$$

$$\begin{bmatrix} 12 & \sum x_i \\ \sum x_i & \sum x_i^2 \end{bmatrix} \begin{bmatrix} X_0 \\ X_1 \end{bmatrix} = \begin{bmatrix} \sum y_i \\ \sum x_i y_i \end{bmatrix}$$
 (5)



Calculate with the help of MATLAB to get fitting

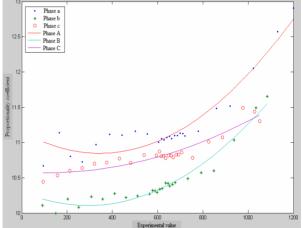


Figure 6. Proportional coefficient curve obtained through fitting of currents.

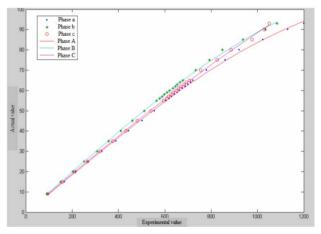


Figure 7. Contrast of experimental current value and virtual current value obtained through fitting.

polynomials of phase A, B and C as equation (6).

$$\begin{cases} \psi_A(x) = -0.0025x + 24.397 \\ \psi_B(x) = -0.0025x + 24.4434 \\ \psi_C(x) = -0.0027x + 24.2588 \end{cases}$$
 (6)

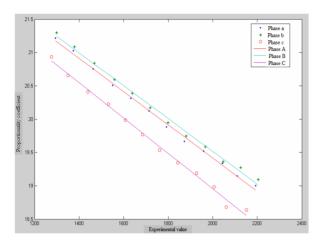


Figure 8. Proportional coefficient curve obtained through fitting of voltage.

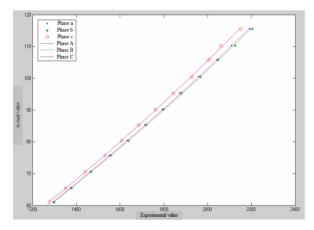


Figure 9. Contrast of experimental voltage value and virtual voltage value obtained through fitting.

Conduct fitting process on each point's voltage scaling factor to get a proportionality coefficient curve. Together with the proportionality coefficient of each point obtained through experimental data, it is shown in **Figure 8**.

Based on proportional coefficient of each point through fitting, determine corresponding voltage value and display the contrast relation with actual voltage values in **Figure 9**.

Final experimental results indicated that the deviation between obtained three-phase experimental voltage value and the actual voltage value is about 0.3%, which is able to meet engineering design requirements.

4. Conclusions

As experiments and analyses showed, this innovative smart contactor is featured by the realization of the onoff control of three-phase 115 V/400 Hz AC power supply, the real time adjustment of contactor status as per bus command and the real time surveillance of three-phase load voltage within the safety range of 60 - 150 V and the AC within the safety range of 10 - 60 A as per bus command, as well as the surveillance of contactor's ambient temperature fluctuating within $\pm 1^{\circ}$ C under the scope of -40° C $-+150^{\circ}$ C. The contactor is also able to perform real time uploading of present working parameters as per requirement of data processing devices to realize remote control.

REFERENCES

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