

# Effects of Thermal Conditions in the Phase Formation of Undoped and Doped $\text{Pb}(\text{Zr}_{1-x}\text{Ti}_x)\text{O}_3$ Solid Solutions

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## ABSTRACT

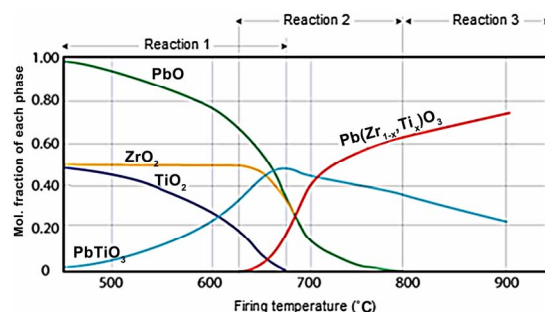
The purpose of this research is to study the effect of thermal conditions such as temperature ramp rate and isothermal times in the phase formation of  $\text{Pb}(\text{Zr}_{1-x}\text{Ti}_x)\text{O}_3$  solid solutions with composition near the morphotropic phase boundary (MPB) by using the conventional ceramic method. The perovskite phase formation and morphology of undoped  $\text{Pb}(\text{Zr}_{0.52}\text{Ti}_{0.48})\text{O}_3$  (abbreviated PZT) and doped new material  $\text{Pb}_{0.98}\text{Gd}_{0.02}[(\text{Zr}_{0.52}\text{Ti}_{0.48})_{0.98}(\text{Mg}_{1/3}\text{Nb}_{2/3})_{0.01}(\text{Ni}_{1/3}\text{Sb}_{2/3})_{0.01}]\text{O}_3$  (abbreviated PZT-PGMNNS) specimens calcined between 700°C and 900°C have been examined by powder X-ray diffraction (XRD), scanning electron microscopy (SEM) and Fourier Transform Infrared (FTIR) while the thermal evolution of the initial precursor was followed by TG-DTA. So the results of these studies have been discussed.

**Keywords:**  $\text{Pb}(\text{Zr}_{1-x}\text{Ti}_x)\text{O}_3$ ; Morphotropic Phase Boundary; Conventional Ceramic Method; Perovskite Phase

## 1. Introduction

The solid solution of  $\text{Pb}(\text{Zr}_{1-x}\text{Ti}_x)\text{O}_3$ , known as lead zirconate titanate (PZT), is one of the most studied ferroelectric materials in the past 40 years, especially because of its excellent dielectric, ferroelectric and piezoelectric properties [1-4]. The highest piezoelectric coefficients of PZT are found for compositions near the morphotropic phase boundary (MPB) between the tetragonal and rhombohedral regions of the composition-temperature phase diagram [5,6]. Generally, the material of PZT is fabricated by a solid-state reaction among  $\text{PbO}$ ,  $\text{TiO}_2$  and  $\text{ZrO}_2$  (ordinary dry method) by which the sequences of this reaction are today well known and several studies describe them very well [7-13]. Most authors agree that the solid state reaction usually begins by the formation of a highly tetragonal lead titanate solid solution, which the remaining  $\text{PbO}$  and  $\text{ZrO}_2$  react to form  $\text{Pb}(\text{Zr}_{1-x}\text{Ti}_x)\text{O}_3$ . One version of the course of reaction is shown in **Figure 1**. [14], which shows the different phases present depending on the temperature.

The transformations undergone by the initial mixture oxides during its heat treatment can be simple or complex depending on the nature and the reactivity of the



**Figure 1.** Phases in the system  $\text{PbO}:\text{TiO}_2\text{-PbO}:\text{ZrO}_2$  as a function of firing temperature [14].

starting oxides (purity, structure, grain size, etc...) which choice of the composition of the reaction mixture, the addition of various dopants and the thermal conditions (heating/cooling rates and isothermal times) [15-18] that seem to have a great effect on the progress of the reaction including the formation of the desired final phase (PZT).

To define the thermal conditions that govern the reaction mechanism, it is necessary to use several techniques to determine unambiguously the final product formed. Therefore, the study is attempted to describe and to explain the thermal conditions which govern the phase formation of undoped and doped  $\text{Pb}(\text{Zr}_{1-x}\text{Ti}_x)\text{O}_3$  solutions,

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prepared by a conventional mixed-oxide method at various processing conditions like; calcination temperature; temperature ramp rates and isothermal times using different analysis techniques such as X-ray diffraction and thermal analysis techniques that are very often complete each other.

## 2. Experimental Procedure

The compositions that used in this study are  $\text{Pb}(\text{Zr}_{0.52}\text{Ti}_{0.48})\text{O}_3$  (undoped PZT) and  $\text{Pb}_{0.98}\text{Gd}_{0.02}[(\text{Zr}_{0.52}\text{Ti}_{0.48})_{0.98}(\text{Mg}_{1/3}\text{Nb}_{2/3})_{0.01}(\text{Ni}_{1/3}\text{Sb}_{2/3})_{0.01}]\text{O}_3$  (doped PZT-PGMNNS) close to the morphotropic phase boundary (MPB). These systems were prepared by the conventional ceramic method. The starting raw materials in oxide form of high purity used were  $\text{PbO}$  (massicot, 99.0% purity, Biochem),  $\text{ZrO}_2$  (baddeleyite, 99.0% purity, Biochem),  $\text{TiO}_2$  (60.2% rutile and 39.8% anatase, 99.0% purity, Biochem),  $\text{Gd}_2\text{O}_3$  (99.99% purity, Alfa Aesar),  $\text{MgO}$  (99.6% purity, Alfa Aesar),  $\text{Nb}_2\text{O}_5$  (99.95% purity, Alfa Aesar),  $\text{NiO}$  (99.6% purity, Alfa Aesar) and  $\text{Sb}_2\text{O}_3$  (>99.0% purity, Biochem).

For the preparation of PZT and PZT-PGMNNS precursors, the starting powders were weighted in the required stoichiometric ratio and then mixed in acetone medium for 24 h through a magnetic stirrer to achieve homogenization. After drying process, the mixed powders were crushed for 6 h in a mortar with a pestle. To ease the reactions in solid, the powders were pressed into 13 mm in diameter and 2 mm thick pellets under uni-axial pressure of 750 MPa. The resultant specimens were calcined on alumina plates at temperatures between 700 and 900°C. The chosen conditions of temperature ramp rates and duration (isothermal time) were varied from 2 to 10°C min<sup>-1</sup> and from 2 to 6 h, respectively.

After calcinations, the fired product was analyzed by X-ray diffraction (XRD: BRUKER-AXE, D8) using  $\text{CuK}\alpha$  radiation. The results, *i.e.* peak positions; were compared with the information from the JCPDS database to identify the presence of the perovskite structure and phases present. The general morphology of the calcined specimens were observed by scanning electron microscopy (SEM: JEOL JSM-6390LV) at room temperature. Complementary analysis which confirm the formation temperature of the perovskite phase, such as thermal analyses (TG/DTA: L70/2171 Thyristor-Power Supply) from 25°C to 900°C at a heating rate of 10°C min<sup>-1</sup> and infrared analysis (FTIR: FTR-8400S SHIMADZU) in the 4000 - 400 rang using the KBr pellet technique (about 1 mg of sample and 200 mg of KBr were used for the preparation of the pellets) were performed.

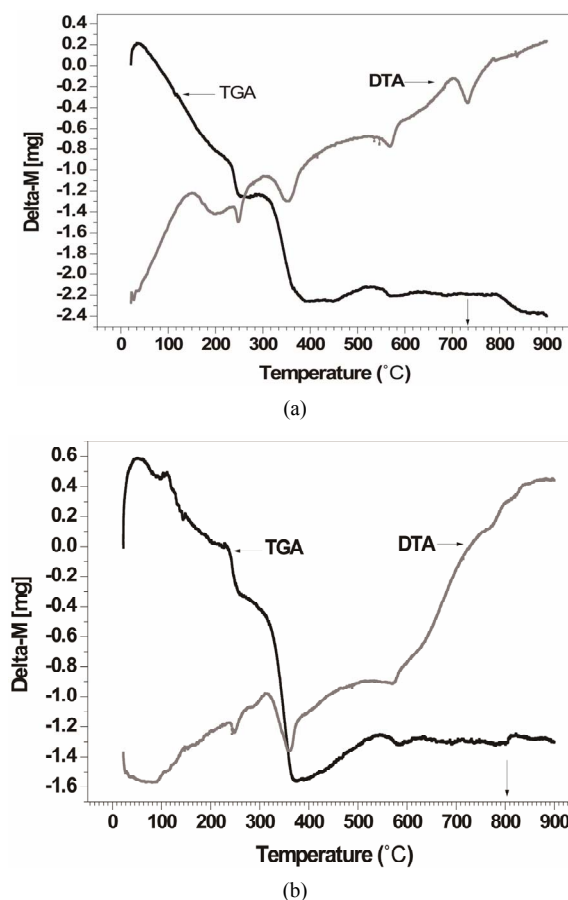
## 3. Results and Discussion

The thermal analyses (TG/DTA) provides additional information on the synthesis and the thermal conditions of

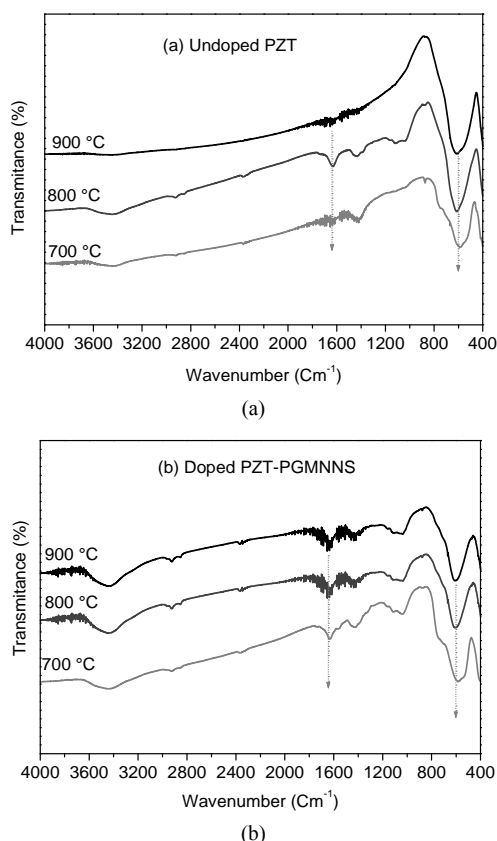
the phase formation. **Figure 2** displays the TG/DTA curves performed over the undoped and doped powder mixture compositions selected for this study.

These results confirm our good choice of the temperature range (between 700°C and 900°C) for samples calcinations. From these figures we deduce observe that the temperature of the perovskite phase formation is estimated between 700°C and 750°C, in correlation with an endothermic peak centered at ca. 730°C (**Figure 2(a)**) which corresponds mainly to an oxygen loss resulting from the formation of the final perovskite phase for the undoped powder. While it is estimated at a higher temperature (750°C to 850°C (**Figure 2(b)**) in correlation with an endothermic peak centered at ca. 800°C) for the doped powder which indicates that doping affects the temperature of the phase formation. These results are in agreement with FTIR and XRD results discussed below.

With FTIR analysis, it was possible to track the formation, as a function of calcination temperatures, of PZT's  $\text{ABO}_3$  structure. **Figure 3** presents the IR spectra, in the zone between 4000 and 400 cm<sup>-1</sup> for all phases of undoped PZT and doped PZT-PGMNNS samples.



**Figure 2.** TG/DTA curves for the powder mixture compositions: (a) undoped powder; (b) doped powder.

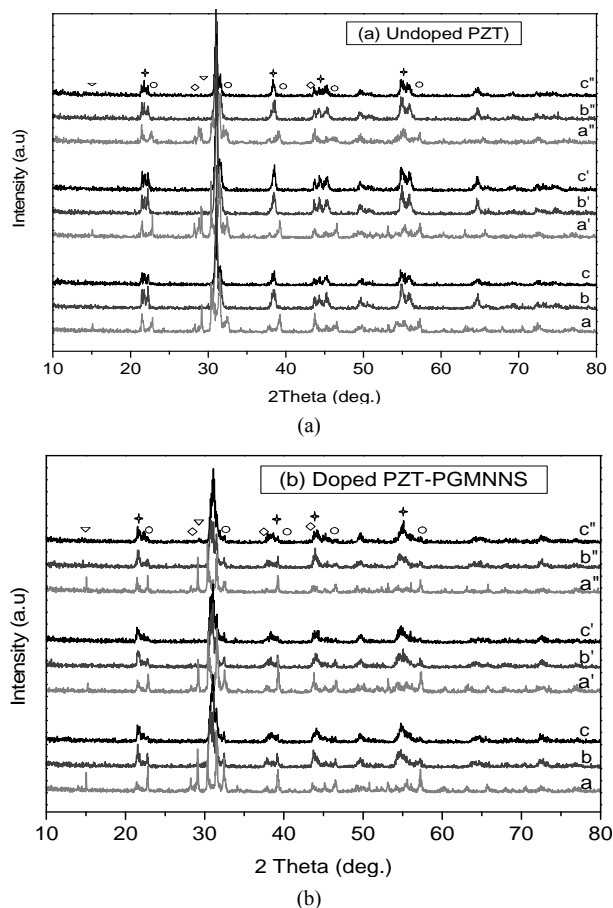


**Figure 3.** FTIR spectra of the samples calcined at the indicated temperatures using a temperature ramp rate of 2 °C/min for 2 h: (a) undoped PZT; (b) doped PZT-PGMNNS.

In **Figures 3(a)** and **b**, the most important band, that extends from 800 to 400  $\text{cm}^{-1}$ , of the perovskites structure, is observed with a maximum absorption at  $\sim 600 \text{ cm}^{-1}$ , which is the characteristic band of oxides with perovskite-type structure [19,20]. This bands exhibit a significant increase for the samples calcined at a higher temperature (800 °C and 900 °C). Noting that a small band at about  $\sim 1600 \text{ cm}^{-1}$  which is probably typical of the presence of some water in the KBr employed to dilute the samples into the pellets and chemisorbed from the atmosphere onto the samples is also observed in some of the spectra.

With DRX analysis it was possible to ensure of the phase purity and identify the crystalline phases of the calcined powders at different thermal conditions. **Figure 4** shows the XRD patterns of undoped PZT and doped PZT-PGMNNS powders at various calcination temperatures (750 °C, 800 °C and 900 °C), temperature ramp rates (2 °C/min and 10 °C/min) and periods of time (2 and 6 h). Similar trends were also observed for PZT produced by using other thermal conditions [21].

From these figures it was found that PZT perovskite phase with co-existence of both tetragonal and rhombohedral phases matching with the JCPDS file no. 33-0784



**Figure 4.** XRD patterns of powders calcined at different temperatures and for different isothermal times and temperature ramp rates for undoped PZT and doped PZT-PGMNNS: a, b, c) 10 °C/min until 700 °C, 800 °C, 900 °C for 2 h, a', b', c' and a'', b'', c'') 2 °C/min until 700 °C, 800 °C, 900 °C for 2 h and 6 h respectively. In this figure, (P) stands for PbO ( $\nabla$ ); (PT) for  $\text{PbTiO}_3$  ( $\circ$ ); (PZ) for  $\text{PbZrO}_3$ ; ( $\diamond$ ) for PZT ( $\star$ ).

and 73-2022, respectively and without any trace of pyrochlore phase normally forms was observed in all the samples. In the XRD patterns of the undoped and doped powders that were reacted at 700 °C using a ramp rate of 2 and 10 °C/min for 2 and 6 h (**Figures 4(a)** and **b**) additional peaks at approximately 15°, 29° 2 $\theta$  and were detected. These can be attributed to the presence of unreacted PbO. Peaks of PT (JCPDS no. 06-0452), and PZ (JCPDS no. 035-0739) were also observed in the XRD patterns which is believed to originate from the uncompleted reaction during powder calcination at these thermal conditions.

When the reaction temperature was increased to 800 °C with changing the heating profile (2 to 6 h and 10 to 2 °C/min), no PT and PZ peaks were observed in the XRD patterns. This means that a reaction had occurred. All the

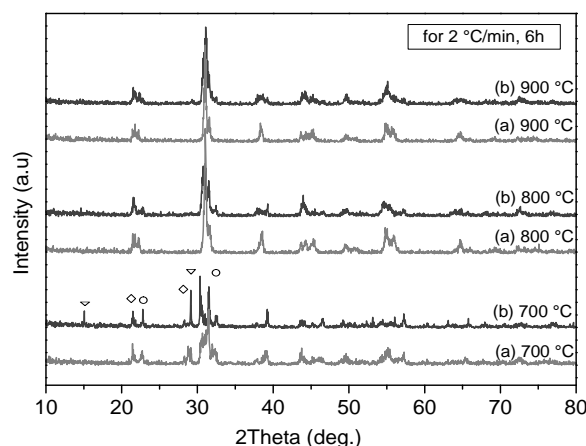
samples calcined at 900°C exhibit almost the same XRD spectrum. The stoichiometric composition diffraction patterns calcination between 700°C and 900°C using a ramp rate of 2°C/min for 6 h, which are considering as optimal thermal parameters for this study is shown in **Figure 5** and compared with doped simple composition.

It is possible to observe that the number of PbO peaks is less compared with doped sample calcined under the same conditions. This result could well indicate that the perovskite phase formation is not complete for doped compositions. When the calcination temperature is increased, the reaction is observed to be almost complete and the perovskite structure is dominated in XRD for all compositions. Notice that a heating profile also influences the final particle size and size distribution of phase formation.

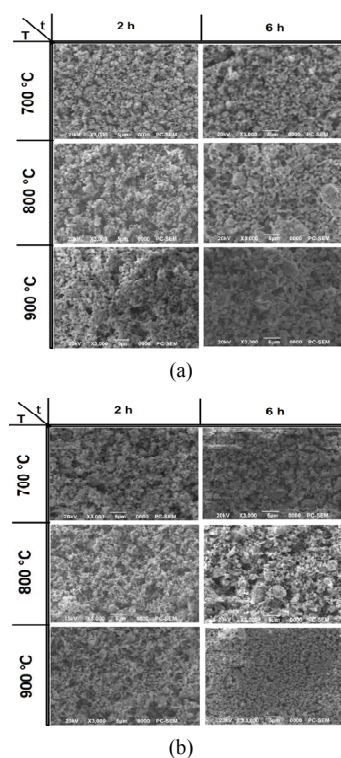
In **Figure 6**, the particle morphology of the powders is compared. It can be noted that the increasing of reaction temperature (top to bottom) or time (left to right) led to increase in the particle size. This is more evident for powders synthesized with isothermal time of 6 h. The shape gradually became more regular with the increasing of isothermal time (left to right). Both the phenomena were also observed at lower heating ramp rates (**Figures 6(a)** and **(b)**).

At the lowest processing temperature and time (700°C, 2 h) the synthesized PZT powder had a distinctive spherical shape (**Figure 7(a)**) which became less pronounced with the increasing process parameters the final particle size and size distribution of it was instead observed that a change in the particle shape occurred with particles becoming more regular with decreasing ramp rates (at constant isothermal time and temperature).

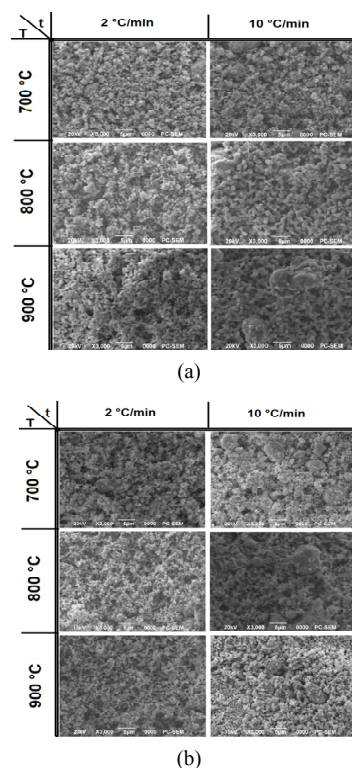
Moreover an increment in the heating rate led to a larger particle size distribution with the presence of big particles in the final PZT powder. This correlates with the observed results by others [22].



**Figure 5.** XRD patterns of PZT and PZT-PGMNNS powders at different temperatures with a temperature ramp rate of 2°C/min for 6 h.



**Figure 6.** SEM micrographs of powders calcined at different temperatures and for 2 and 6 h of isothermal times (a) undoped PZT; (b) doped PZT-PGMNNS.



**Figure 7.** SEM micrographs of powders calcined at different temperatures and with temperature ramp rates of 2 and 10°C/min for: (a) undoped PZT; (b) doped PZT-PGMNNS.

#### 4. Conclusion

The effect of thermal process parameters such as calcination temperature, reaction time and temperature ramp rate on the perovskite phase formation and general particle size morphology of undoped and doped PZT compositions was investigated by solid-state route. Thus, the results obtained in this study allowed us to suggest a standardized thermal profile that can be used to synthesize new materials using the same state route. For samples calcined at 700°C with higher temperature ramp rate (10°C/min), the reaction between the starting materials was not complete. Residual PbO and intermediate solid solutions (PT and PZ) were found within the product. A single perovskite phase type was observed as calcination temperature increased at 800°C. At temperature higher 900°C there is no notable change which allows us to consider that 800°C as the optimum temperature of calcination samples using the ramp rate of 2°C/min and 6 h of during time. The particles obtained at 700°C and at fast heating rates were less spherical than the same powder treated at higher temperatures for the same isothermal time. At high temperatures and long reaction times an excessive particle growth was observed. The regular particles were obtained by heating the raw materials at 800°C for 2 h using a slow temperature ramp rate (2°C/min<sup>-1</sup>).

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