

The Influence of Surface Conditioning of Ceramic Restorations before Metal Bracket Bonding

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ABSTRACT

The aim of this study was to compare the shear bond strength and Adhesive Remnant Index of four different veneering ceramic materials to metal brackets. Additionally, it should be examined whether it is possible to overcome the etching method using hydrofluoric acid which is noxious. Instead of this treatment, air particle abrasion with 25 um aluminium trioxide, silane coupling application and etching with 37.0 per cent orthophosphoric acid as pre-treatment procedures of the veneering ceramics before bonding was investigated. Two surface conditioning methods of four ceramic materials before bonding brackets were examined: in Group 1 an air particle abrasion with 25 µm aluminium trioxide (4 seconds at a pressure of 2.5 bars) and subsequently a silane coupling agent (Espe Sil, 3M Unitek, Monrovia, USA) was applicated on one side of each ceramic specimen (10 per group). In Group 2 one side of each sample (10 per group) was etched with 37.0 per cent orthophosphoric acid for two minutes and was followed by a silane application (Espe Sil, 3M Unitek, Monrovia, USA). After this procedure the self-ligating metal brackets SmartClip (3M Unitek, Monrovia, USA) brackets were bonded to the ceramic blocks and a thermocycling process started (5°C - 55°C, 6000 cycles). Then, shear bond strength and Adhesive Remnant Index (ARI) were measured. To determine statistical differences Oneway-ANOVA and Tukey Post-hoc test were performed. The level of significance was set at $\alpha = 0.05$. On the basis of the results of the current study, it could be concluded that sandblasting with 25 µm aluminium trioxide and the use of orthophosphoric acid (37.0 per cent) seem to prepare the surface of the ceramic restoration sufficiently before bracket bonding. The found level of shear bond strength values seem be sufficient for bracket bonding. Hydrofluoric acid seems not to be justifiable anymore for preparing the surface of dental ceramic restorations before bracket bonding.

Keywords: Ceramic Restorations; Orthodontic Brackets; Aluminium Trioxide; Orthophosphoric Acid

1. Introduction

As a result of the basic investigations of Buonocore (1955) the direct bonding technique has revolutionized bonding brackets to teeth [1]. Over the years a lot of attention has been paid for improving the acid-etching technique, primers and adhesives.

However, the treatment of adult patients is becoming more and more vital in orthodontics at the present time. The operator is often faced with the problem of ceramic restorations, especially in the anterior region, of elderly adult patients. Most of the veneering ceramic materials available on the market are feldspatic with dispersed crystalline phase in the glass matrix. The structure of veneering ceramic has been described as an amorphous and glassy matrix that consists of a random network of crosslinked silica in a tetrahedral arrangement, which is embedded in varying amounts of undissolved feldspatic and leucite crystals [2]. Nevertheless, hydrothermal ceramics,

so called glass ceramics, with innovative chemical and physical properties become more and more important. In this material the quartz lattice, which forms the vitreous phase, is modified by adding alkali oxides, which lower the melting temperature, increases the coefficient of expansion [3]. For ceramic surface treatment, the acid can react with the glassy matrix, which is selectively removed and the crystalline structure is exposed. This leads to rougher surface of the veneering ceramic which means more micromechanical retention [3].

Ceramic restorations, such as ceramic crowns or veneers, which are adhesively bonded to teeth, can be nowadays more often found in orthodontic patients because of an increasing number of adult patients who ask for a treatment. Therefore, the question arises which procedure should be applied for bonding brackets to ceramic restorations. It has been suggested by several authors [4-6] to utilize hydrofluoric acid for preparing the ceramic surface. Hydrofluoric acid is best known for its ability to

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dissolve glass by reacting with SiO₂, the major component of most glass, to form silicon tetrafluoride gas and hexafluorosilicic acid. This property has been known since the 17th century, even before hydrofluoric acid had been prepared in large quantities by Carl Wilhelm Scheele in 1771 [3]. It is also unique in its ability to dissolve many metal and semimetal oxides [6]. The danger in handling hydrofluoric acid is extreme, as skin saturation with the acid in areas of only 25 square inches (160 cm²) may be relatively painless, yet ultimately fatal. High concentrations of hydrofluoric acid and hydrogen fluoride gas will also quickly destroy the corneas of the eyes [7].

Consequently, the purpose of this study was to compare the shear bond strength and Adhesive Remnant Index of four different veneering ceramic materials to metal brackets.

As ceramic materials Vita Omega 900 (VITA Zahnfabrik, Bad Säckingen, Germany), Symbio Ceram (DeguDent, Haunau, Germany), Imagine Reflex (Wieland, Pforzheim, Germany), Hera Ceram Sun (Heraeus Kulzer; Hanau, Germany), Ducera Gold (DeguDent, Haunau, Germany) were chosen. Additionally, a further aim of this study was to overcome the etching using hydrofluoric acid which is noxious and could hardly damage the corneas of the eyes. Instead of that air particle abrasion with 25 μm aluminium trioxide, silane coupling application and etching with 37.0 per cent orthophosphoric acid as pre-treatment procedures of the veneering ceramics before bonding was investigated.

2. Material and Methods

A total of 100 ceramic blocks with the dimensions of $10 \times 10 \times 10$ mm were manufactured. The following sintered ceramics were investigated (20 per group):

Vita Omega 900 (VITA Zahnfabrik, Bad Säckingen, Germany)

Symbio Ceram (DeguDent, Haunau, Germany)

Imagine Reflex (Wieland, Pforzheim, Germany)

Hera Ceram Sun (Heraeus Kulzer; Hanau, Germany)

Ducera Gold (DeguDent, Haunau, Germany)

The exact temperatures of each sintered ceramics during the manufacturing process are shown in **Table 1**. The ceramic blocks were cleaned and polished with burnish-

Table 1. Manufacturing parameters of the sintered ceramic groups.

Ceramic brand	Preheating temperature [°C]	Burning temperature [°C]	Holding time [s]
Vita Omega 900	600	930	60
Symbio Ceram	575	820	60
Imagine Reflex	575	900	120
Hera Ceram Sun	600	860	60
Ducera Gold	450	785	60

ers to attain a high gloss.

Two surface conditioning methods of the ceramic blocks before bonding brackets were investigated: in Group 1 an air particle abrasion with 25 μ m aluminium trioxide (4 seconds at a pressure of 2.5 bars) and subsequently a silane coupling agent (Espe Sil, 3M Unitek, Monrovia, USA) was applicated on one side of each ceramic specimen (10 per group). In Group 2 one side of each sample (10 per group) was etched with 37.0 per cent orthophosphoric acid for two minutes and was followed by a silane application (Espe Sil, 3M Unitek, Monrovia, USA).

After this procedure the brackets were bonded to the ceramic blocks as follows: the conventional primer Transbond XT Primer (3M Unitek, Monrovia, USA) was applied, gently thinned with air and light-cured for 20 seconds (Ortholux LED, 3M Unitek). After this procedure the self-ligating metal brackets SmartClip (3M Unitek, Monrovia, USA) were bonded to the ceramic specimens using the adhesive Transbond XT (3M Unitek, Monrovia, USA). All brackets were placed centrally on the prepared surfaces of the samples. The excess resin was carefully removed from the tooth using a dental probe. The samples were then light-cured with a light emitting diode (LED) curing device (Ortholux LED, 3M Unitek) for 20 seconds. All brackets were bonded by the same operator.

To simulate the moisture and temperature changes in the oral environment all samples were exposed to thermocycling 24 hours after preparation. All groups were alternatively flooded every 2 min. with warm (55°C) and cold (5°C) distilled water for 6000 cycles in a mastication device [8].

Shear bond strength (SBS) was performed using the universal testing machine Zwick 1446 (**Figure 1**, Zwick, Ulm, Germany) at a cross-head speed of 1 mm·min⁻¹. The embedded ceramic block and the adhesively fixed bracket were positioned in the testing machine so that the bracket slot was placed horizontally. A knife-edge shearing rod was used to deliver the shear force at the bracket base-enamel interface. All brackets were shear tested to failure. The SBS was determined using the formula $\sigma_{\text{shear}} = F_{\text{max}}/A_{\text{bracket base surface}}$ (MPa). The surface area of the bracket bases was determined by measuring length and width and computing the mean area.

Additionally, the Adhesive Remnant Index (ARI) was determined. The classification of the ARI-index was as follows:

"0": no composite remained on the enamel.

"1": less than 50% of the composite remained on the enamel.

"2": more than 50% of the composite remained on the enamel

"3": all composite remained on the enamel.

To determine statistical differences Kruskal-Wallis test



Figure 1. Shear bond strength testing device (Zwick universal testing machine 1446, Zwick, Ulm, Germany).

and Mann-Whitney U-test were performed. Means and standard deviations were calculated. The level of significance was set at $\alpha=0.05$.

3. Results

Results of shear bond strength measurements are depicted in Figure 2. In Table 2 ARI scores of the different ceramic groups are listed. The statistical analysis of the data obtained in our study reveals that there is no significant enhancement of shear bond strength using sandblasting with 25 µm aluminium in comparison to using orthophosphoric acid (37.0 per cent) as surface conditioning method of ceramic restorations (p > 0.05, Table 3). Almost the same result could be observed when ARI scores are compared: No statistical different between the two surface conditioning methods could be measured (p > 0.05, **Table 3**). Median values of shear bond strength are shown in **Table 4**. The ceramic restoration Image Reflex revealed the lowest shear bond values of all groups after sandblasting (130.0 MPa, Table 4). The highest shear bond values could be observed using the ceramic groups

Table 2. ARI (Adhesive Remnant Index) of different ceramic groups.

ARI score:	0	1	2	3
Vita Omega 900 sandblasted	5	2	0	3
Vita Omega 900 etched*	6	0	0	4
Symbio Ceram sandblasted	1	3	0	6
Symbio Ceram etched*	10	0	0	0
Imagine Reflex sandblasted	6	0	0	4
Imagine Reflex etched*	8	0	0	2
Hera Ceram Sun sandblasted	2	0	0	8
Hera Ceram Sun etched*	6	0	0	4
Ducera Gold sandblasted	5	2	0	3
Ducera Gold etched*	7	0	0	3

Etched*: etched with 37.0 per cent orthophosphoric acid for 1 minute. ARI scores: "0", no composite remained on the enamel; "1", less than 50% of the composite remained on the enamel; "2", more than 50% of the composite remained on the enamel; "3", all composite remained on the enamel.

Table 3. Statistical analysis.

	SBS	ARI index
Vita Omega 900 sandblasted vs etched*	n.s.	n.s.
Symbio Ceram sandblasted vs etched*	n.s.	n.s.
Imagine Reflex sandblasted vs etched*	n.s.	n.s.
Hera Ceram Sun sandblasted vs etched*	n.s.	n.s.
Ducera Gold sandblasted vs etched*	n.s.	n.s.

Statistical analysis (Kruskal-Wallis test, Mann-Whitney U-test) of shear bond strength (SBS) and adhesive remnant index (ARI); n.s.: not significant; Level of significance: p=0.05; etched*: etched with 37.0 per cent orthophosphoric acid for 1 minute; No significant difference (p>0.05) between sandblasted and etched ceramics within a material group and between the groups were measured.

Table 4. Median-values of different ceramic groups. Shear bond strength: SBS.

Ceramic groups :	SBS [MPa]		
Vita Omega 900 sandblasted	172.5		
Vita Omega 900 etched	196.5		
Symbio Ceram sandblasted	169.5		
Symbio Ceram etched	217.5		
Imagine Reflex sandblasted	130.0		
Imagine Reflex etched	141.5		
Hera Ceram Sun sandblasted	166.5		
Hera Ceram Sun etched	195.0		
Ducera Gold sandblasted	170.5		
Ducera Gold etched	168.0		

are listed. The statistical analysis of the data obtained in our study reveals that there is no significant enhancement of shear bond strength using sandblasting with 25 μ m aluminium in comparison to using orthophosphoric acid (37.0 per cent) as surface conditioning method of ceramic restorations (p > 0.05, **Table 3**). Almost the same result could be observed when ARI scores are compared: No statistical different between the two surface condition-

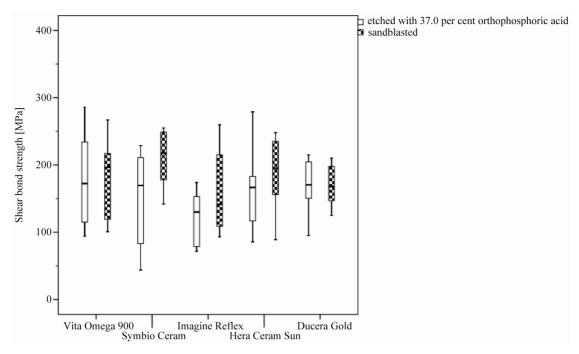


Figure 2. Shear bond strength [MPa] of different ceramic groups etched with 37.0 per cent orthophosphoric acid or sand-blasted before bracket bonding.

ing methods could be measured (p > 0.05, **Table 3**). Median values of shear bond strength are shown in **Table 4**. The ceramic restoration Image Reflex revealed the lowest shear bond values of all groups after sandblasting (130.0 MPa, **Table 4**). The highest shear bond values could be observed using the ceramic Symbio Ceram after etching with orthophosphoric acid (37.0 per cent) as surface conditioning method (217.5 MPa, **Table 4**).

4. Discussion

Dental ceramics are nowadays often used as restorative material as veneers, crowns and bridges because of their aesthetic appearance, their outstanding mechanical properties and their biocompatibility. The increased demand by adults for orthodontic treatment results in the necessity for orthodontics to attach brackets and tubes on ceramic restorations. However, the difficulty of orthodontic bracket bonding is its semipermanent nature. Bond strength should be high enough to resist accidental debonding during treatment but also low enough to remove the bracket from the ceramic without generating excessive force which might damage the peridontium of the tooth or the restoration [9]. Several methods have been suggested to strengthen the bond strength between ceramics and brackets: it was described to roughen the porcelain with diamond burs, green stones or abrasive disks [7]. Others described for getting more retention to cut a retention cavity in the ceramic surface [6]. Nevertheless, all these procedures damage the glazed surface of restoration. Another method of roughening the ceramic surface is to apply acids or sandblasting [5]. The use of strong acids to roughen the ceramic surface was suggested by Calamia [10]. As acids hydrofluoric acid and orthophosphoric acid have been suggested. 9.6 per cent hydrofluoric acid is able to create a series of surface pits by preferential dissolution of the glass phase from the ceramic matrix [5]. Nevertheless, it is described as an acid which is extremely dangerous because of its corrosive character and the danger of causing severe trauma to soft tissues and tooth substance [11]. For that reason we decided to use in this study orthophosphoric acid instead of hydrofluoric acid with the aim to demonstrate that hydrofluoric acid is not necessary for bonding brackets to ceramic restoration. It was demonstrated that orthophosphoric acid with a concentration of 37.0 per cent is not able to etch a ceramic surface and, consequently, does not produce physical or topographical changes on porcelain. On the other hand, orthophosphoric acid has the ability to neutralize the alkalinity of the absorbed water layer, which is present on all ceramic restorations in the mouth and, thereby, improve the chemical activity of any silane primer when subsequently applied [11]. Silane molecules, after being hydrolyzed to silanol, is able to form a polysiloxane network or hydroxyl groups to cover the silica surface. Monomeric ends of silane molecules react with the methacrylate groups of the adhesive resins by free radical polymerization [12,13].

The aim of this study was to compare the shear bond strength and Adhesive Remnant Index of four different

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veneering ceramic materials to metal brackets and to examine whether it is possible to overcome the etching using hydrofluoric acid which is noxious. Instead of this treatment, air particle abrasion with 25 μm aluminium trioxide, silane coupling application and etching with 37.0 per cent orthophosphoric acid as pre-treatment procedures of the veneering ceramics before bonding was investigated.

The results of the present study show that there is no significant enhancement of shear bond strength and ARI scores using sandblasting with 25 μm aluminium in comparison to using orthophosphoric acid (37.0 per cent) as surface conditioning method of ceramic restorations.

Therefore, the method of sandblasting with 25 um aluminium trioxide the surface of the ceramic restoration could be rejected because the method of using only orthophosphoric acid (37.0 per cent) revealed comparable results and is much easier to apply. The ARI scores measured in this study confirm this conclusion. Additionally, the use of hydrofluoric acid seems not to be justifiable anymore for preparing the surface of dental ceramic restorations before bracket bonding. The danger in handling hydrofluoric acid is extreme, because skin and corneas of the eyes could be severely damaged by contact. The results of the present study show that median values of 130.0 - 217.5 MPa could be reached using only orthophosphoric acid (37.0 per cent). This level of shear bond strength is described to be sufficient for bracket bonding and to avoid accidental bracket debonding [4-6]. Nevertheless, it needs to be remembered that this is an in-vitro study, and care should be taken in interpreting the results to those that might be obtained in the oral cavity.

5. Conclusion

On the basis of the results of the current study, it could be concluded that sandblasting with 25 μ m aluminium trioxide and the use of orthophosphoric acid (37.0 per cent) seem to prepare the surface of ceramic restoration sufficiently before bracket bonding. The found level of shear bond strength values seem be sufficient for bracket bonding. Hydrofluoric acid seems not to be justifiable anymore for preparing the surface of dental ceramic restorations before bracket bonding.

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