

# Simulation of the Thermal and Mechanical Effects of a Planar Rectangular High Intensity Ultrasound Transducer to Be Used for Destroying Atherosclerotic Plaque

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## ABSTRACT

The aim of this study is to perform a simulation study of the thermal and mechanical effects of a flat rectangular ( $3 \times 10 \text{ mm}^2$ ), MRI compatible transducer operating at 5 MHz for the purpose of destroying atherosclerotic plaque. The simulation study focuses on measuring the plaque destruction (due to the thermal or mechanical mode of ultrasound) as a function of power, time, frequency, duty factor and pulse duration. The main goal is to keep the artery temperature at a safe level. The simulation study shows that with the thermal mode the temperature in the artery cannot be kept at a safe level.

**Keywords:** Ultrasound; Atherosclerotic; Plaque; MRI

## 1. Introduction

Atherosclerosis also known as arteriosclerotic vascular disease (ASVD) is a condition in which fatty material collects along the walls of arteries. This fatty material thickens, hardens (forms calcium deposits), and may eventually block the arteries [1]. Calcium is a critical component of atherosclerotic plaque. The absence of calcification is strong evidence against the presence of active disease even with significant luminal stenosis. Calcification is reversible and may contribute to the formation of an atheroma by adding the byproducts of resorption to the necrotic core. The sequence of events in plaque development following injury is inflammation, followed by calcification of the damaged tissue, ending ultimately in the formation of a necrotic core [2-4].

Lifestyle changes, such as following a healthy diet and exercising, are often the best treatment for atherosclerosis. But sometimes, medication or surgical procedures may be recommended as well [5]. Over the years, researchers have been involved in Clinical research to develop medication treatments and approaches in order to reduce the risk of heart attack and other medical problems caused by atherosclerosis (for example Angiotensin II receptor blockers (ARBs) [5], Angiotensin-converting enzyme (ACE)[6], Cholesterol Medications[7], Diuretics[8]).

In advanced cases, atherosclerosis treatment may require special surgical procedures such as Balloon Angioplasty [9-12], Balloon Angioplasty and Stenting [13-15], Cutting Balloon [16-21], Atherectomy [22,23], Surgical Bypass [24,25] and Endarterectomy [26,27] to open an artery and improve blood flow.

Another treatment option could be the application of mechanical waves such as ultrasound. With ultrasound either the thermal or mechanical properties can be utilized. Our group uses MRI to monitor ultrasonic protocols and therefore, the ultrasonic transducer has to be MRI compatible. In this paper a simulation study of the thermal and mechanical effects of flat rectangular ( $3 \times 10 \text{ mm}^2$ ), MRI compatible ultrasonic transducer operating at 5 MHz for destroying atherosclerotic plaque is included. The simulation study focuses on measuring the plaque destruction (thermal or mechanical) as a function of power, time, frequency, duty factor and pulse duration. The main goal is to keep the artery temperature at a safe level. This paper includes the design of the MRI compatible transducer.

## 2. Materials and Methods

### 2.1. Simulation Model

The power field was estimated using the KZK model [28]. The temperature vs. time history was obtained by

solving the bio-heat equation proposed by Pennes (1948) numerically [29]. The explicit form of this equation is given by:

$$\rho_t c_t \frac{\partial T}{\partial t} = k \nabla^2 T + w_b c_b (T - T_a) + Q_p \quad (1)$$

where  $\rho_t$  is the density of the tissue,  $c_t$  is the specific heat of the tissue,  $T$  is the temperature of the tissue,  $t$  is the time,  $w_b$  is the blood perfusion rate,  $c_b$  is the specific heat of the blood,  $T_a$  is the arterial blood temperature,  $k$  is the thermal conductivity of the tissue, and  $Q_p$  is the ultrasonic power deposition rate.

### 2.2. Estimation of Thermal Dose

The effect of hyperthermia depends on the temperature and the duration of the heating. If a constant temperature could be maintained, then the duration of heating would be a reasonable way of expressing thermal dose, with units of time. In reality, however, a constant temperature is not maintained, so it is necessary to find a method of relating a treatment to an equivalent time at a specified reference temperature. A mathematical relation between time and temperature was described by Dewey [30] and given by:

$$t_2 = t_1 R^{(T_2 - T_1)}, \quad (2)$$

where  $T_1, T_2$  are temperatures at times  $t_1$  and  $t_2$  respectively, and  $R$  is a constant.

The calculation of the thermal dose for changing temperature exposure was done by using the technique suggested by Sapareto and Dewey [31]. The technique uses numerical integration to calculate the time that would give an equivalent thermal dose at a reference temperature under different temperature profiles. The reference temperature of 43°C has been chosen since this is the standard temperature used as a reference [21]. For any temperature profile the dose can be found by

$$t_{43} = \sum_0^{t_{final}} R^{(43 - T_t)} \Delta t, \quad (3)$$

where  $t_{43}$  is the equivalent time at 43°C,  $T_t$  is the average temperature during  $\Delta t$ . The default value of  $R$  equal to 0.25 was chosen for temperatures smaller than 43°C and a value equal to 0.5 for temperatures higher than 43°C [31]. The temperature after the power turn OFF was also considered since during the decay part thermal dose is contributed.

### 2.3. Estimation of Lesion Size

The prediction of lesion size requires the knowledge of the thermal dose threshold that causes 90% - 100% necrosis. Previous studies [32,33] show that the threshold thermal dosage reference at 43°C for soft tissue is be-

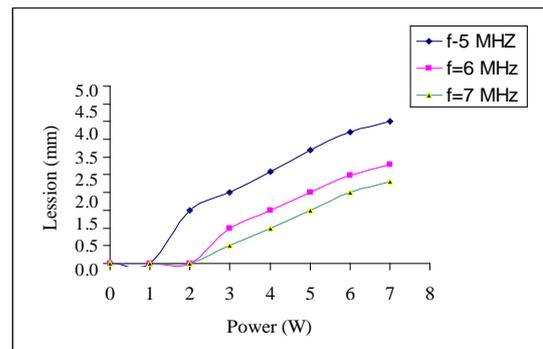
tween 50 min and 240 min. Therefore, the extreme threshold of dose necrosis of 240 min at 43°C was considered.

### 3. Results

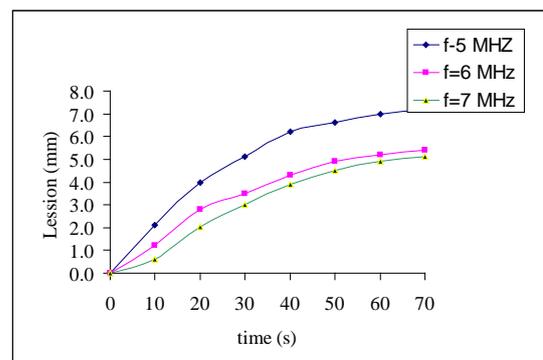
**Figure 1** shows the graph of thermal lesion vs. power for a 20 s sonication at the frequency of 5, 6, 7 MHz. Therefore with 5 MHz and 3 W a plaque of 2 mm is destroyed. With 7 MHz a power of 6 W must be used in order to destroy 2 mm. **Figure 2** shows the thermal lesion vs. time for a power of 7 W at the frequency of 5, 6, 7 MHz. Therefore with 5 MHz and 20 s a 4 mm plaque is destroyed. With 7 MHz and 20 s a plaque of 2 mm is destroyed. The temperature in the artery for both **Figure 1** and **Figure 2** exceeded the safe level. **Figure 3** shows the graph of plaque removal vs. power for PRF = 1 Hz, DF = 10% and frequency 5, 6, 7 MHz (total time = 30 mins). Therefore with 5 MHz and 60 W a plaque of 2 mm is removed. With 7 MHz and 60 W a 1 mm plaque is removed. The temperature in the artery for the results of **Figure 3** never exceeded the safe level.

### 4. Conclusions

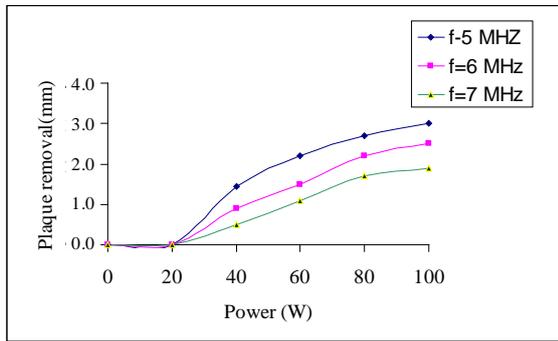
The aim of this paper was to conduct a simulation study



**Figure 1.** Thermal lesion vs. power for a 20 s sonication at the frequency of 5, 6, 7 MHz.



**Figure 2.** Thermal lesion vs. time for a power of 7 W at the frequency of 5, 6, 7 MHz.



**Figure 3. Plaque removal vs. power for PRF = 1 Hz, DF = 10% and frequency 5, 6, 7 MHz (total time = 30 min).**

of the thermal and mechanical effects of a flat rectangular ( $3 \times 10 \text{ mm}^2$ ) MRI compatible transducer operating at 5 MHz for destroying atherosclerotic plaque. The main goal was to keep the artery temperature at a safe level. The simulation study shows that with the thermal mode the temperature in the artery cannot be kept at a safe level. Using mechanical mode ultrasound yields no severe temperature elevation in the arteries. This paper provides useful information regarding the size of the plaque removal as power, time, frequency, duty factor and pulse duration.

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